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VOLUME NEVADA-UT, VERIFICATION STUDIES, FY GEOTECHNICAL DAT WHITE RIVER NORTH, CDP, NEVAL

PREPARED F
SPACE AND MISSILE SYSTEMS ORGANIZATION (SAM
NORTON AIR FORCE BASE, CALIFORE



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GEOTECHNICAL EVALUATION
VOLUME V, NEVADA-UTAH
VERIFICATION STUDIES, FY 79
GEOTECHNICAL DATA
WHITE RIVER NORTH CDP, NEVADA

Prepared for:

U. S. Department of the Air Force Space and Missile Systems Organization (SAMSO) Norton Air Force Base, California 92409

Prepared by:

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24 August 1979

VOLUME V GEOTECHNICAL DATA, WHITE RIVER NORTH CDP

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FOREWORD

This report was prepared for the Department of the Air Force, Space and Missile Systems Organization (SAMSO), in compliance with Contract No. F04704-78-C-0027, CDRL Item 005A2. It presents geological, geophysical, and geotechnical data and evaluates the suitability of portions of Nevada and Utah for siting the MX Land Mobile Advanced ICBM System.

This report is the first of several Verification reports which will be prepared. The objectives are to verify sufficient suitable area for deployment of the MX System and to provide preliminary physical and engineering characteristics of the soils. The Verification Studies are the final phase of a site-selection process which was begun in 1977. Previous studies have been termed Screening, Characterization, and Ranking. In preparing this report, it has been assumed that the reader is familiar with these previous studies.

Results of the FY 79 Verification studies are contained in 11 volumes as follows:

Geotechnical Results

Volume 1A - Sections 1.0, 2.0, and 3.0 contain Introduction, Results and Conclusions, and Recommendations for Future Studies. Sections 4.0 through 6.0 contain summary geotechnical data for Whirlwind, Snake East, and Hamlin CDP's.

Volume 1B - Sections 7.0 through 10.0 contain summary geotechnical data for White River North, Garden-Coal, Reveille-Railroad and Big Smoky CDP's.

Geotechnical Data Volumes

Volume II - Whirlwind CDP Volume III - Snake East CDP

Volume IV - Hamlin CDP

* Volume V - White River North CDP

Volume VI - Garden-Coal CDP

Volume VII - Reveille-Railroad CDP

Volume VIII - Big Smoky CDP Volume IX - Dry Lake CDP Volume X - Ralston CDP

* This volume is presented herein.

SECTION 1.0
GEOLOGIC STATION DATA

EXPLANATIONS OF GEOLOGIC STATION DATA

Geologic stations were established at selected locations throughout the CDP at which detailed descriptions of surficial basin-fill deposits or rock were recorded. Locations of all geologic stations are shown in Drawing 1, Activity Location Map. All data taken on surficial basin-fill units at these stations are listed in Table 1-1 and an explanation of the column headings in the table is given below. At stations where rock descriptions were made, only geologic unit designations are listed. A general explanation of all geologic unit symbols used in Verification Studies is included at the end of this section.

Column Heading	
Table 1-1	

Explanation

Station Number	Geologic stations are numbered sequentially.
	Where more than one geologic field team worked
	in a CDP, stations made by each team are dif-
	ferentiated with a letter (A, B, or C) follow-
	lan the state of a membrane

ing the station number.

Geologic Unit	Generic geologic unit only, i.e. the grain-size designation (f, s, g, c) is omitted from surficial basin-fill units. The letter B in the
	unit designation indicates a buried deposit not exposed at the surface.

MPS MM Average maximum particle size in millimeters.

Grain Size

(%B, %C, %G,

Wnified Soil Classification System. Percentages of boulders (%B) and cobbles (%C) are based on the entire deposit, whereas percentages of gravel (%G), sand (%S) and fines (%F) are taken only on the fraction composed of particles less than 3 inches (76 mm) in diameter.

USCS Soil class according to the Unified Soil Class-ification System.

Munsell Color Soil color based on Munsell Soil Color Chart.

Source Rock
Types(s)

Rock types of coarse clasts listed in order of abundance.

* Physical Properties

Data listed in columns 6 through 15 address specific soil properties. These are listed below in parentheses following the column heading number and are also listed at the bottom of Table 1-1. Data are coded with each numerical entry referring to a specific soil condition as listed below.

- 6 (Grain Shape) 1) Angular, 2) Subangular, 3) Subrounded,
 - 4) Rounded, 5) Well rounded
- 7 (Moisture 1) Dry, 2) Moist, 3) Wet Content)
- 8 (Plasticity 1) None, 2) Low, 3) Medium, 4) High of Fines)
- 9 (Consistency) Coarse grained: 1) Very Loose, 2) Loose, 3) Medium Dense, 4) Dense, 5) Very Dense,

Fine grained: 1)Soft, 2) Firm, 3) Stiff,
4) Hard

- 10 (Structure)

 1) Stratified Tabular, 2) Stratified Other (lensed, cross bedded, discontinuous beds),
 3) Nonstratified
- 11 (Cementation 1) None, 2) Weak, 3) Moderate, 4) Strong
 Induration) .
- 12 (Depth to Depth to layer (in centimeters) exhibiting cemented cementation induration described in Column 11 (above)
- 13 (Weathering 1) Fresh, 2) Slight, 3) Moderate, 4) Very of clasts)
- 14 (Soil 1) None (A-C profile), 2) Poor (incipient B-horizon), 3) Well (prominant B-horizon) Development)
- 15 (Caliche 1) Stage I, 2) Stage II, 3) Stage III, Development) 4) Stage IV, 5) None

Drainage

DP	(M)	Average	depth	of	drainages	(in	meters)
WD	(M)	Average	width	of	drainages	(in	meters)

Average slope of ground surface (in percent grade) Slope (%)

Sample Number of samples taken

GENERALIZED GEOLOGIC UNITS

Explanation

Surficial Basin-fill Units

- Al Younger Fluvial Deposits Major modern stream channel and flood-plain deposits.
- A2 Older Fluvial Deposits Older incised stream channel and flood-plain deposits in elevated terraces bordering major modern drainages.
- A3 Eolian Deposits Wind-blown deposits of sand occurring as either thin sheets (A3s) or dunes (A3d).
- A4 Playa and Lacustrine Deposits Deposits occurring in modern, active playas (A4) or in either inactive playas or older lake beds and abandoned shorelines associated with extinct lakes (A40).
- A5 Alluvial Fan Deposits Alluvial deposits consisting of debris flow and water-laid alluvium near mountain fronts, grading into predominantly water-laid alluvium deposited in shifting distributary channels near the basin center. Younger (A5y), intermediate (A5i), and older (A5o) alluvial fans are differentiated by surface soil development, terrain conditions, and present depositional/erosional environment.

Grain sizes of these deposits (except A3 deposits, which are exclusively sandy) are indicated by a single letter (f, s, g, or c) following the geologic unit symbol. These letters indicate the predominant grain size and range of soil types according to the Unified Soil Classification System:

- f fine-grained (ML, CL, MH, CH)
- s sands (SP, SW, SM, SC)
- g gravels (GP, GW, GM, GC)
- c coarse grained with greater than 30 percent boulders and cobbles (generally GP, GW, GM, GC)

ROCK UNITS

- I Igneous (undifferentiated). Rocks formed by solidification of a molten or partially molten mass.
 - Il Intrusive Plutonic rocks formed by solidification of molten material beneath the surface (e.g., granite, granodiorite, diorite, gabbro).
 - I2 Extrusive (intermediate and acidic) Volcanic rocks of intermediate and acidic compositon formed by solidification of molten material at or near the surface, (e.g., rhyolite, latite, dacite, andesite).
 - I3 Extrusive (basic) Volcanic rocks of basic composition, generally formed by solidification of molten materials at or near the surface (e.g., basalt).
 - I4 Extrusive (pyroclistic) Rocks formed by accumulation
 of volcanic ejecta (e.g., ash, tuff, welded tuff,
 agglomerate).
- S Sedimentary (undifferentiated) Rocks formed by accumulation of clastic solids, organic solids and/or chemically precipitated minerals.
 - Sl Arenaceous and/or Siliceous Rocks Composed of sand size particles (e.g., sandstone, orthoquartzite) or of cryptocrystalline silica (e.g., opal, chert).
 - S2 Carbonate Rocks Composed predominantly of calcium carbonate detritus or chemical precipitates (e.g., limestone, dolomite, chalk).
 - S3 Argillaceous Rocks Composed of clay and silt-sized particles (e.g., siltstone, shale, claystone).
 - S4 Evaporite Rocks Precipitated from solution as a result of evaporation (e.g., halite, gypsum, anhydrite, sylvite).
 - S5 Coarse Clastic Rocks Composed of gravel sized or larger clasts (e.g., conglomerate, breccia).
- M Metamorphic (undifferentiated) Rocks formed through recrystallization in the solid state of preexisting rocks by heat and pressure (e.g., gneiss, schist, nornfels, metaguartzite).

		SOIL DESCRIPTION		TERRAIN
STATION MISSNUP	GEOL MPS GRAIN SIZE UNIT WH TO BC IG IS TR	FUSCS COLOR ROCK TYPE(S)	*PHTSICAL PROPERTIES 5 7 8 9 10 11 12 15 14 15	SHAINAGE SUCHE SHEED LOOK SAMPLE
-	451 170 00 08 45 032 025		2 1 1 2 3 2 02C 2 2 3	3.0 202 6 2
448G024	A51 090 00 02 25 370 005		1 2 1 2 3 1	1.5 310 32 3 1.0 362 3E
44RG02P 44RG03A	55 458 070 00 00 02 086 012	* **-** A7 FWAR/4 17		••
N48603A	ASY 720 00 62 65 025 610	1 GP-G* 10.0Y45/6 12		•5 003 Ge
###604F	AST 155 00 73 50 035 015		7 7 2 4 3 3 1 1 5 1 5 2 2 1 7 2 2 03A 7 2 2 2	2.5 075 CC 0
9436646	ASY 015 00 00 37 2P6 105	SP-SH 10.0784/4 52 [2	2 4 1 2 3 2 1 5	
448604P 448605A	A2P 030 00 40 60 040 301 A5Y 120 00 31 55 650 013		2 2 1 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	•e 302 21 1
448G558 448G161	41 300 00 30 30 305 395 440 004 00 00 00 305 595		2 3 2 3 1 1 5	.1 000 22 1
MWRSJER	ASI 270 GG C1 35 053 C15	5 54 05.0745/6 52	7 2 1 3 2 1 032 3 7 2	1+5 32* 33 5
1486074 1486075	A40 025 00 30 01 075 125 A51 400 31 35 50 046 036		1 2 1 1 3 2 040 2 1 1	1.5 300 CC 7
44FG064	457 175 00 CO 35 045 020	S SP C7.5YP5/4 52	2 2 1 2 2 1 300 2 2 1	45 007 34 2
4486046	457 702 00 00 JT 590 610		7 2 1 7 3 1 2 5	: u :
4486094	ASI 120 00 01 30 040 030	C SM 10.0486/4 32 12	7 7 1 2 3 2 340 2 2 2 2 2 2 2 3 1 032 2 2 2 2	1.0 003 34 0
4686348 4686364	ASI 335 00 00 25 070 005		? Z 1 Z 3 1 032 Z 2 ? 3 Z 1 3 2 Z 034 ? ? 2	1.0 100 10 2
MWRG108	ASC 001 00 00 00 005 095 AST 050 00 00 30 005 025		2 2 4 3 3 1 000 2 2 1	1.0 001 4
4486118	451 085 00 02 45 646 567	7 <4-5P 07.5YR4/4 52 12	5 2 1 2 3 1 2 2 2	341 175 17 1
4486124 4486128	457 110 00 02 45 030 925 451 075 30 04 60 020 020		2 2 2 2 2 1 2 1 5 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	45 203 24 2 340 270 21 0
WHRG 134	451 240 OT 30 25 CEO 325	5 SC	2 2 3 3 3 1 3 2 1	2+5 093 25 2
4446138 4486144	451 0+0 30 07 15 C48 005 457 135 30 02 15 045 325		2 2 2 2 3 2 247 5 1 3	1.0 001 37 .
448614F	45: 820 00 CT 16 375 315	SP 10.3747/4 S2	2 2 1 2 3 2 367 2 1 2	
144615B	440 001 00 00 30 015 085 451 040 00 05 75 J23 302	2 GB 52	7 2 1 2 2 2 355 2 1 1	1.5 010 35 .
NURG168	ASI 345 08 30 15 060 325 ASI 349 00 05 50 040 310		2 3 1 2 3 2 04 7 2 2 3 2 2 1 4 3 2 230 2 1 2	2.0 104 04 0 1.0 425 07 0
NURG174	457 575 00 00 15 065 J20	SM 07.5485/6 S2	721331 215	45 301 DU D
96178	451 180 00 10 50 045 003 451 060 00 20 20 060 023	5 GP+G* 10.0YR7/4 52 12 5* 2 5* 10.0YR5/4 52	2 2 1 4 3 4 942 2 1 4	1.0 000 11 1 .7 100 02 1
448 G 1 88	ASY 078 00 02 60 028 012	2 CP+GM 07.5YP5/4 52 12	1 2 2 2 3 1 2 1 1	.f 203 37 -
4486138 4486138	A40 361 66 68 86 867 136 A51 340 37 27 25 878 884		2 2 1 5 3 4 030 7 3 4	145 300 75 7
NW#627A NW#6278	457 025 08 30 07 340 550 451 398 08 10 50 455 115		1 2 1 3 3 1 1 1 1 5	.5 302 02 0
NWRG214	AST 130 00 G2 30 C55 '15	5 SM 10.0746/6 12		ted ond le d
4486218 4486224	457 105 07 01 40 040 020	97.5784/4 8 SP+GP 10.0764/4 12 52	5 2 1 2 3 1 2 2 3	2.5 002 02 0
4WF 62 28	ASY 015 00 00 07 098 002	SP 07.5144/6 12 EL	2 2 1 2 3 1 055 1 5	1.0 3.5 3. [
NURG234 NuRG235	ASI 160 31 15 65 333 003		3 2 1 4 2 4 245 2 1 4	10.0 100 27 2
44F6244	451 170 CO 02 60 020 020 451 080 00 15 45 073 002		1 2 2 3 1 3 627 2 1 1 1 1 2 1 4 3 3 628 7 7 7	1.5 30/ 28 1
NuR6254	457 001 00 00 00 007 10	J =L 10-0785/4	2 2 3 3 1 1 1 5	001 20
NWAG258 NWAG264	ASI 060 08 90 02 098 10		7 2 1 2 2 2 340 2 1 3	4.6 636 3
NUF 6268	451 060 00 00 05 055 00	2 SP 07.5Y#4/6 12	2 2 2 2 3 3 1 2 1 5	.2 505 07
448 G 2 7 5 448 G 2 7 2	457 346 98 98 91 069 039 451 200 08 30 50 045 009	0 SP	2 2 2 3 3 1 7 1 5 3 2 1 2 3 1 7 7 1	1-5 000 01
44RG244	457 150 00 C0 60 015 025 457 130 00 C3 60 039 010		7 2 7 2 3 1 2 7 1 7 2 1 2 5	1.6 103 /6 3
462674 4646364	ASY 380 CO 01 40 C40 121	0 SH#GP 07.5Y#4/6 52	5 2 2 7 2 2 437 2 2 1	*C 790 11 7
NURS31A NURS32A	AST 045 00 70 15 055 030 AST 065 08 01 35 050 01		2 2 1 3 3 3 030 2 2 2 3	48 305 04 1 43 001 14 3
448613A	ASY COL 00 00 00 786 10	0 ML 10.67##/6		.0 000 23 3
MURG34A Murg35A	ASI 363 00 00 30 350 029 ASI 105 00 01 65 327 300		2 2 1 3 3 7 505 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	1.0 106 (+ 1 2.0 105 (F)
4446364	451 060 08 00 15 065 520		3 7 1 1 3 2 654 2 2 2	** 361 52 1

7 - CONSISTENCY 12 - DEPTH TO CEMENTED LATERIONS 15 - CALIDME DEVILOPMENT 10 - STRUCTURE 13 - MEATHERING OF CLASTS 11 - DEMENTATION-INCURATION 14 - SCIL PROFILE DEVELOPMENT

GEOLOGIC STATION DATA
VERIFICATION SITE, WHITE RIVER, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE

EPARTMENT OF THE AIR FORCE - SANSO

**PHYSICAL PROPERTIES : 6 - GRAIN SMAPE 7 - MOISTUPE CONTENT P - PLASTICITY FINES SECTION 2.0
GROUND-WATER DATA

EXPLANATIONS OF GROUND-WATER DATA

Existing ground-water data were collected from all available sources. These data were updated where possible from measurements taken during Fugro field operations, and all data are shown on Table 2-1. Locations of water wells and boreholes in which water-level measurements were available are shown in Drawing 1. Well numbers listed in Column 1 (Table 2-1) refer to well locations in Drawing 1. Actual well numbers giving location according to the Bureau of Land Management Land Survey System are shown in Column 2.

Water levels generally refer to the static ground-water table in the unconfined basin-fill aquifer. Perched conditions or levels in artesian aquifers are noted where known.

1		ELEVATION		WATER LEVEL			
WELL NO.	WELL LOCATION NUMBER*	OF GROUND SURFACE - FEET (METERS) ABOVE M.S.L.	DEPTH OF WELL - FEET (METERS)	DEPTH BELOW GROUND SURFACE - FEET (METERS)	DATE MEASURED	ELEVATION - FEET (METERS) ABOVE M.S.L.	REFERENCES** REMARKS
Wl	12N/62E-29B	5553	112	26	1947	5527	2
W2	12N/62E-30B	(1709) 5558 (1710)	(34)	(8) 37 (11)	1947	(1701) 5521 (1699)	2
ωз	12N/62E-30C	5530 (1702)	50 (15)	22 (7)	1947	5508 (1695)	2
W4	12N/62E-33A	5594 (1721)	48 (15)	40 (12)	1947	5554 (1709)	2
W 5	12N/62E-33D	5531 (1702)	_	24 (7)	1947	5507 (1694)	2
W6	11N/61E-16D	5470 (1683)	82 (25)	28 (9)	1948	5442 (1674)	2
W7	11N/61E-25B	5440 (1674)	-	15 (5)	1978	5425 (1669)	1
W8	11N/61E-27A	5440 (1674)	-	(3)	1978	5429 (1670)	1
W9 W10	11N/61E-32B 11N/61E-35D	5431 (1702) 5417	48 (15)	43 (13) 15	1978	5388 (1658) 5402	1
W10	11N/61E-35D	(1667) 5412	- 171	(5) 14	1978	(1662) 5398	2
W12	11N/62E-4B	(1665) 5531	(53)	(4)	1943	(1661) 5488	2
W13	11N/62E-5D	(1702) 5520	(17) 30	(13)	1948	(1689) 5517	2
W14	11N/62E-6A	(1698) 5503	(9) 10	(1) 5	1947	(1698) 5498	2
W15	11N/62E-7B	(1693) 5480	(3)	(2) 18	1947	(1692) 5462	2
W16	11N/62E-17C	(1686) 5460 (1680)	- 15 (5)	(6) 7 (2)	1948	(1681) 5453 (1678)	2

^{*} Mt. Diablo Baseline and Meridian

GROUND-WATER DATA
VERIFICATION SITE
WHITE RIVER NORTH CDP, NEVADA

NOTE: All wells tap unconfined alluvial aquifers except where noted. Where published data are lacking or inaccurate, ground surface elevations are taken from topographic maps.

MX SITING INVESTIGATION PABLE
DEPARTMENT OF THE AIR FORCE - SAMSO 2-1

^{**} References:

⁽¹⁾ Fugro field measurements (1978)

⁽²⁾ U.S. Geological Survey (1978)

WELL NO.	WELL LOCATION NUMBER*	OF GROUND SURFACE - FEET	DEPTH OF WELL -	DEPTH			1
		(METERS) ABOVE M.S.L.	FEET (METERS)	BELOW GROUND SURFACE - FEET (METERS)	DATE MEASURED	ELEVATION ~ FEET (METERS) ABOVE M.S.L.	REFERENCES**/ REMARKS
W17	lln/62E-19C	5442		7		5435	2
- }		(1674)	-	(2)	-	(1672)	}
W18	11N/62E-28A	5639	}	43	1978	5596	1
- [(1735)	_	(13)	1978	(1722)	j
W19	11N/62E-33D	5661	130	7		5654	2
1		(1742)	(40)	(2)	-	(1740)	}
W20	10N/60E-13C	5390		50	1948	5340	2
- {		(1658)	-	(15)	{ }	(1643)	{
W21	10N/60E-24D	5374	}	41	1948	5333	2
}		(1653)) -	(13)	1	(1641))
W22	10N/60E-36B	5356	į	50	1978	5306	1
- 1		(1648)	} -	(15)		(1633)	}
W23	10N/61E-11D	5376	į	5	1947	5371	2
1		(1654)	-	(2)		(1653)	1
W24	10N/61E-20A	5366	1	22	1978	5344	1
ļ		(1651)	-	(7)] [(1644)	1
W25	10N/61E-26B	5344	l	9	1947	5335	2
}		(1644)	} -	(3)]	(1642)	}
W26	10N/61E-34A	5334	1	6	1947	5328	2
}		(1641)	-	(2)	}	(1639)	
W27	10N/62E-17A	5762	}	259	1978	5503]]
}		(1773)	-	(80)		(1693)	
W28	10N/62E-19A	5630	}	149	1978	5481	1
{		(1732)	-	(46)	1	(1686)	1
W29 {	9N/59E-5D	5885	44	39	1957	5846	2
{		(1810)	(14)	(12)		(1799)	}
W30	9N/60E-1A	5346	40	50	1978	5296	{1
1		(1645)	(12)	(15)	}	(1630)	{
W31	9N/60E-15D	5505	[195	1978	5310	1
1		(1694)	-	(60)	}	(1634)	1
W32	9N/61E-78	5341	43	31	1948	5310	2
i		(1643)	(13)	(10		(1634)	1
į		1	1	ł			

- Mt. Diablo Baseline
- References:
 - (1) Fugro field measurements (1978)(2) U.S. Geological Survey (1978)

GROUND-WATER DATA VERIFICATION SITE WHITE RIVER NORTH COP, NEVADA

NOTE: All wells tap unconfined alluvial aquiters except where noted. Where published data are lacking or inaccurate, ground surface elevations are taken from topographic maps.

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SANSO

TABLE 2-1 2 0f 3

UGRO NATIONAL INC.

		ELEVATION		WATER LEVEL			
WELL NO.	WELL LOCATION Number*	OF GROUND SURFACE - FEET (METERS) ABOVE M.S.L.	OEPTH OF WELL - FEET (METERS)	DEPTH BELOW GROUND SURFACE - FEET (METERS)	DATE MEASURED	ELEVATION - FEET (METERS) ABOVE M.S.L.	REFERENCES**/ REMARKS
W33	8N/59E-3C	6660 (2049)	100	85 (26)	1967	6575 (2023)	2
W34	8N/60E-21A	5490 (1689)	-	500+	1978	(2023) (4990 ((1535)	2
W35	8N/60E-24D	5261 (1613)		35 (11)	1978	5226 (1608)	2
W36	8N/60E-27D	5480 (1686)	142 (44)	116 (36)	1948	5364 (1650)	2
W37	8N/60E-28A	5340 (1643)	_	117 (36)	1978	5223 (1607)	1
W38	8N/61E-33A	5250 (1615)	-	36 (11)	1978	5214 (1604	1
W39	7N/61E-4D	5245 (1614)	-	39 (12)	1978	5206 (1602)	1
W40	6N/60E-21A	5240 (1612)	-	89 (27)	1978	5151 (1585)	1
W41	4N/61E-16D	5094 (1567)	-	84 (26)	1963	5010 (1542)	2
W42	4N/61E-36A	5040 (1551)	-	90 (28)	_	4950 (1523)	2
		Ì			}		
							<u> </u>

- * Mt. Diablo Baseline and Meridian
- ** References:
 - 1. Fugro field measurements (1978)
 - 2. U.S. Geological Survey (1978)

GROUND-WATER DATA
VERIFICATION SITE
WHITE RIVER NORTH CDP, NEVADA

NGTE: Ail wells tap unconfined alluvial aquifers except where noted. Where published data are lacking or inaccurate, ground surface elevations are taken from topographic maps.

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SECTION 3.0 SEISMIC REFRACTION DATA

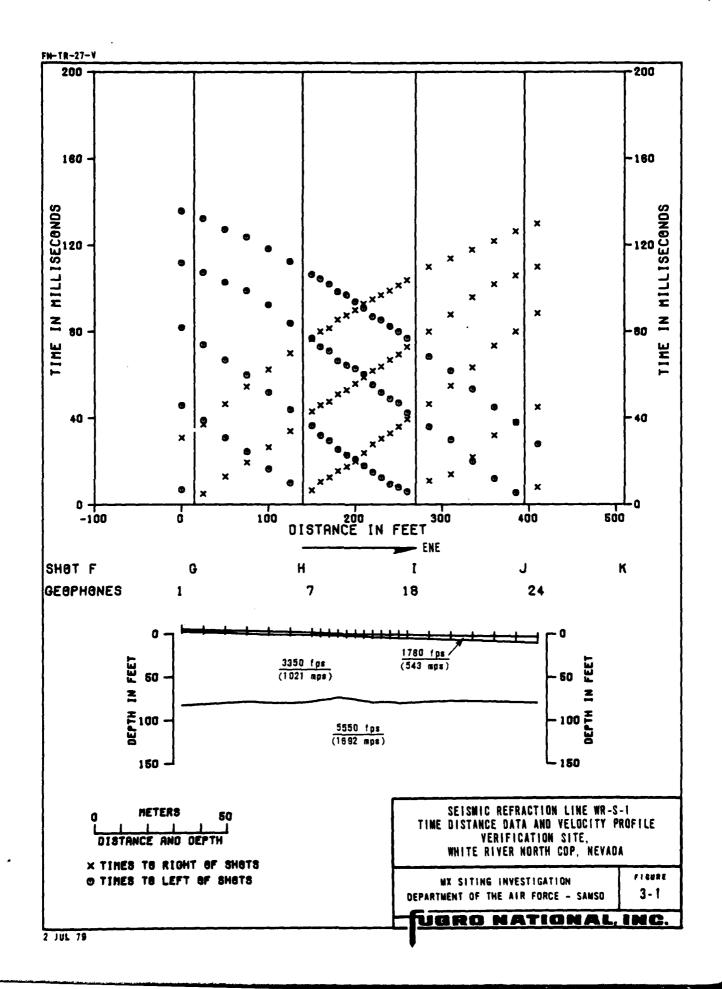
EXPLANATIONS OF SEISMIC REFRACTION DATA

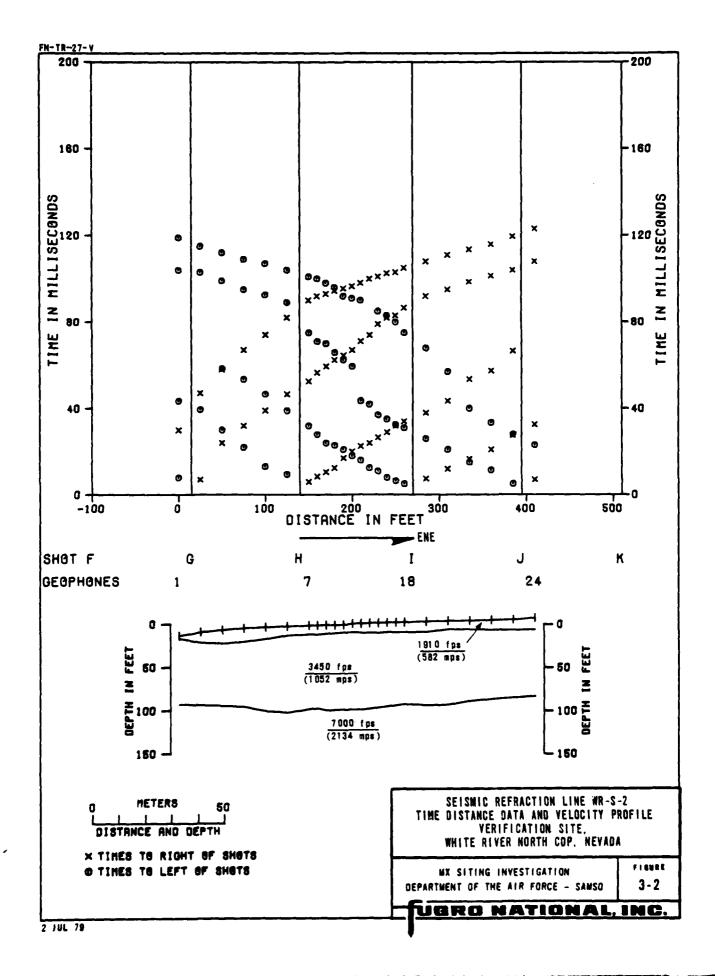
Each figure shows seismic wave travel times plotted versus surface distance between the energy source (shot) and the detector (geophone) for a single seismic line. Distances are measured along the line from geophone number 1 which is designated as zero distance. Distances to the right (on the paper) of geophone 1 are positive. The direction arrow gives the approximate direction of the geophone array from geophone 1 to geophone 24.

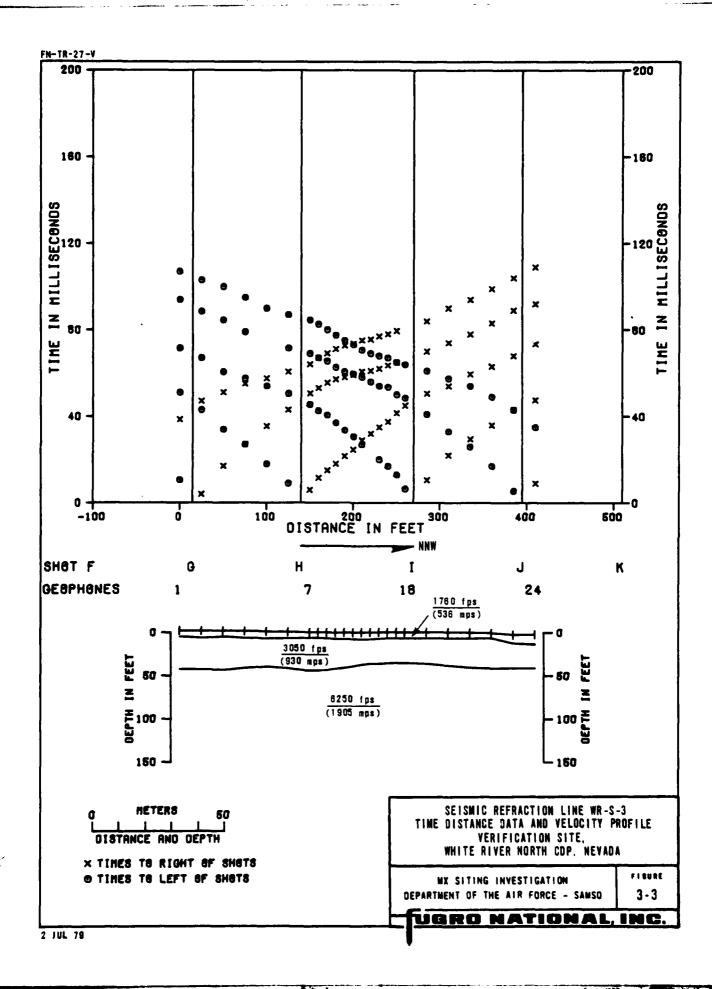
Travel Time Versus Distance Graph (Upper Half of Figure)
This is a travel time versus distance graph. The abscissa
represents distance; the ordinate, time. The six vertical
lines represent the locations of shots (designated as F, G, H,
I, J, and K). The symbol, X, denotes travel times at geophones
that were located to the right of a shot. The symbol, 0,
denotes travel times that were located to the left of shots.

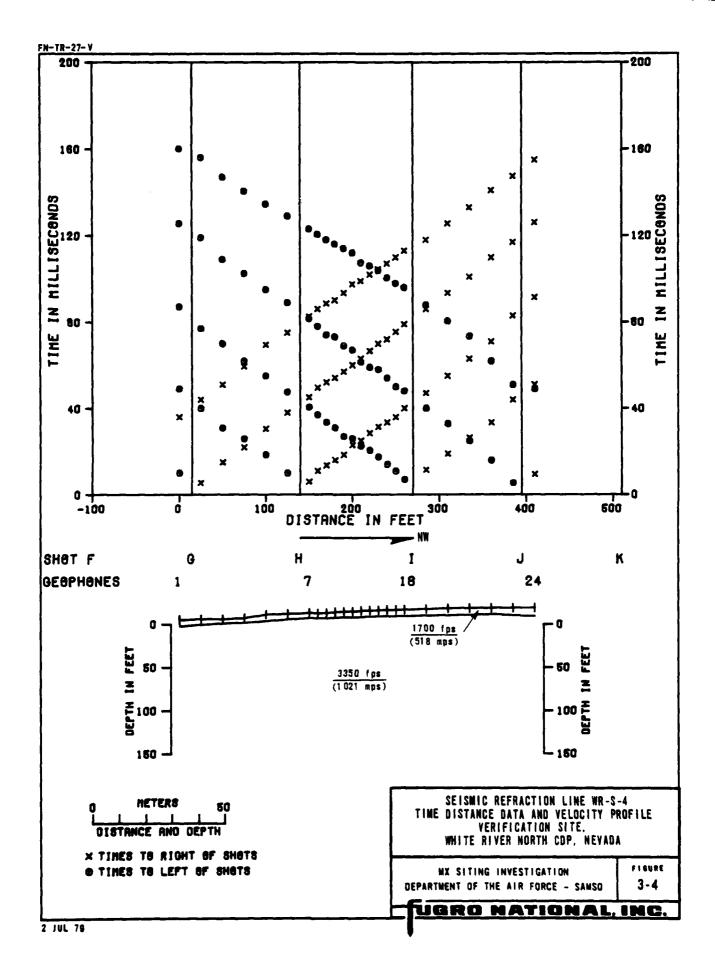
Velocity Cross Section (Lower Half of Figure)

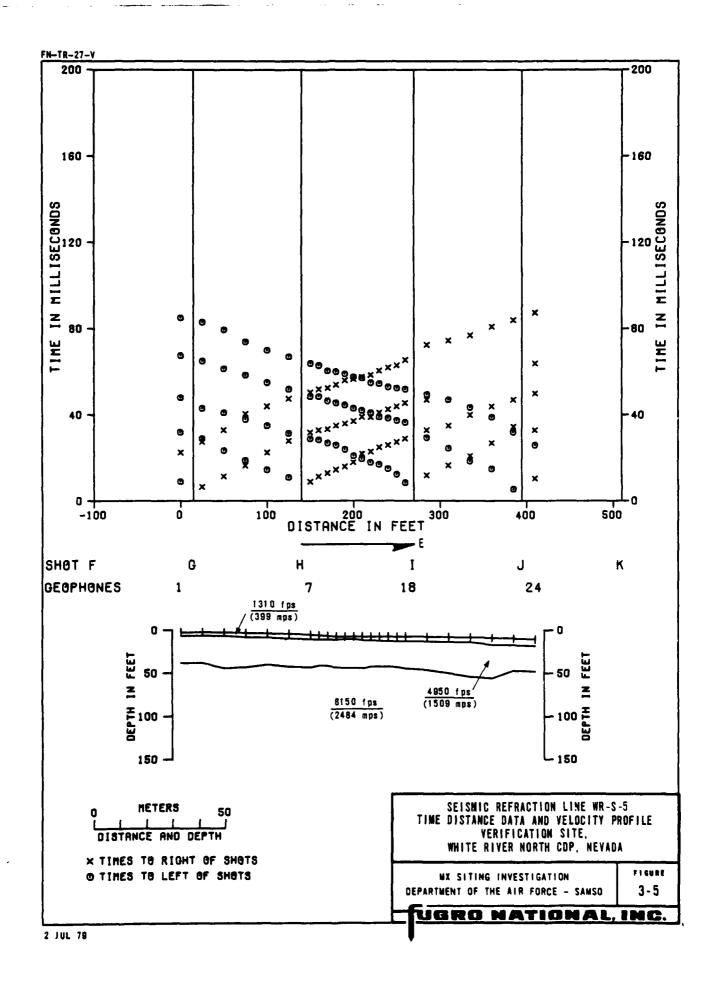
This is an interpreted velocity cross section beneath the seismic line. The top line represents the ground-surface profile. The short vertical lines crossing the top line mark the geophone positions. The depth scale is plotted relative to a point on the line which was arbitrarily chosen as "zero elevation" at the time the line was surveyed. The additional lines across the cross section represent the interpreted boundaries between layers of material with different compressional wave velocities. These boundaries are commonly called "refractors". The velocity interpreted to be representative of each layer is shown.

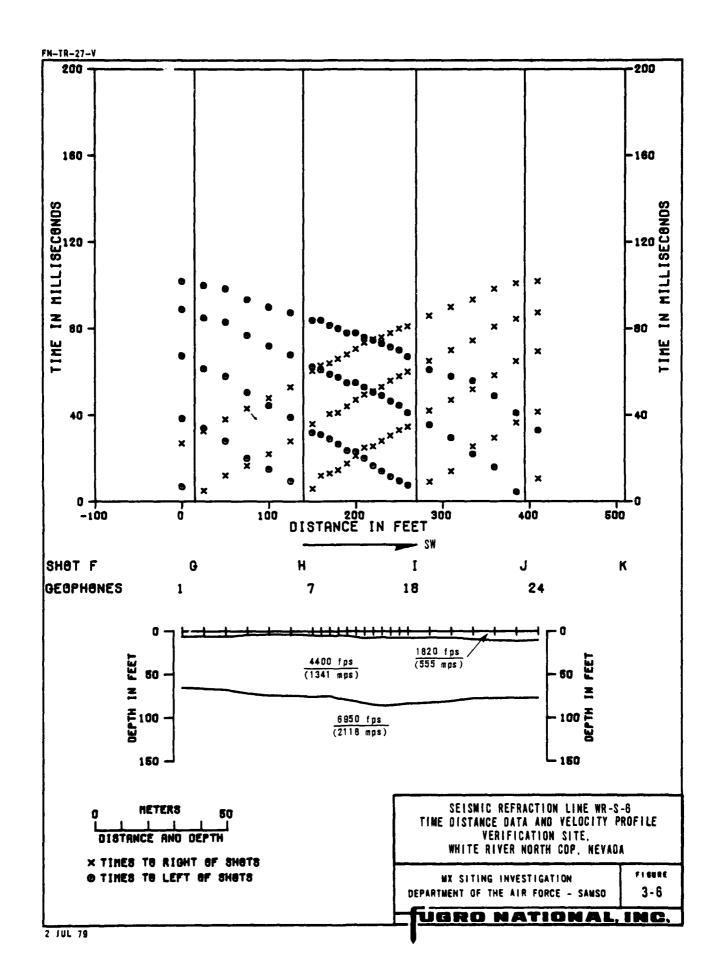


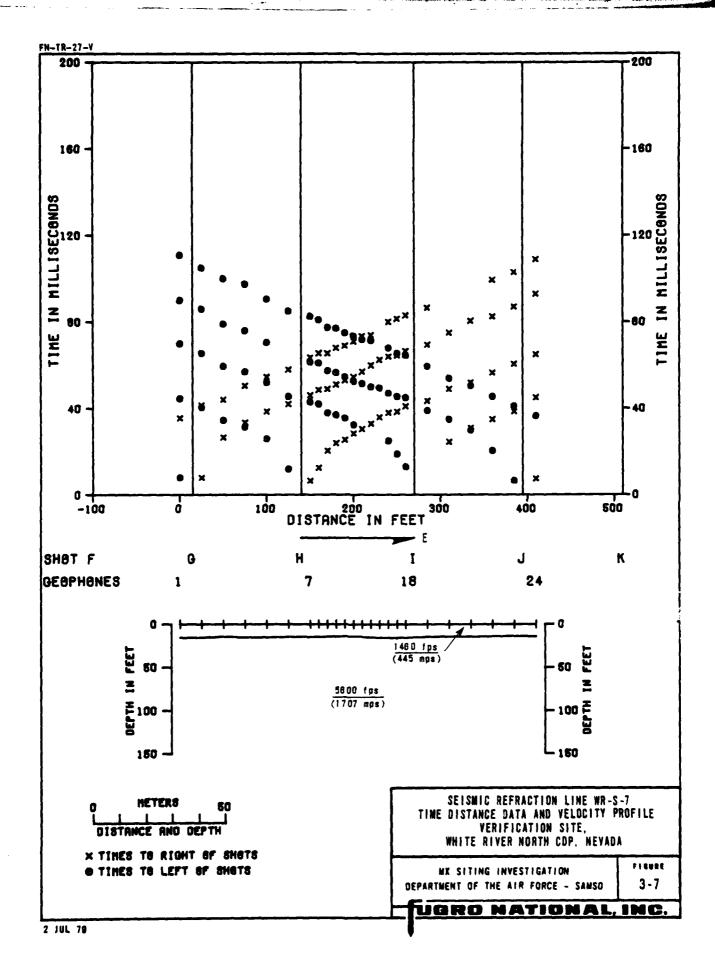


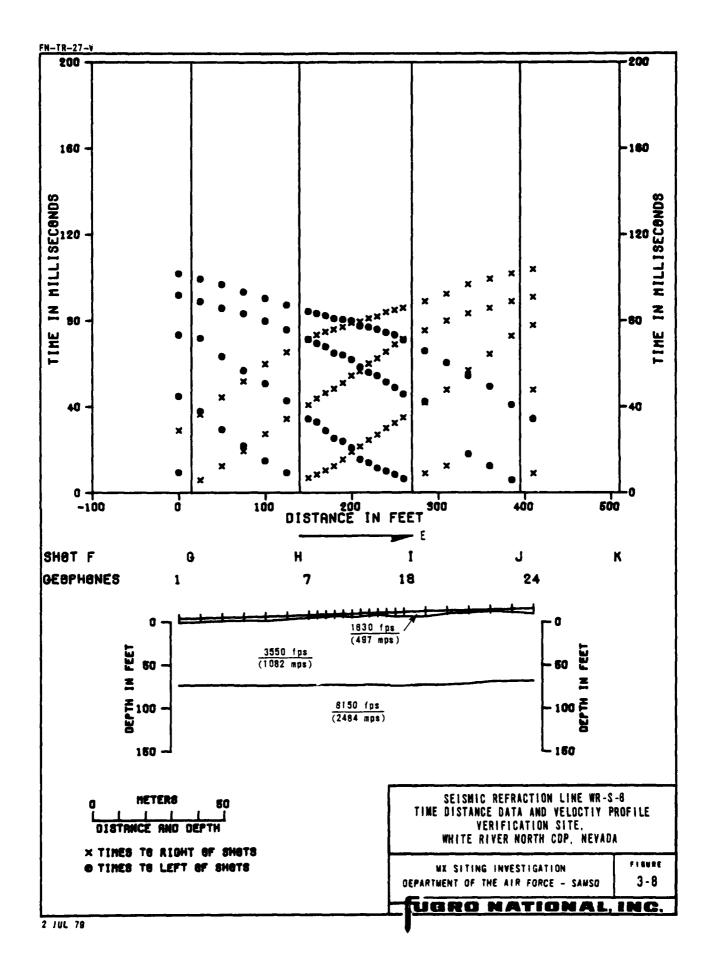


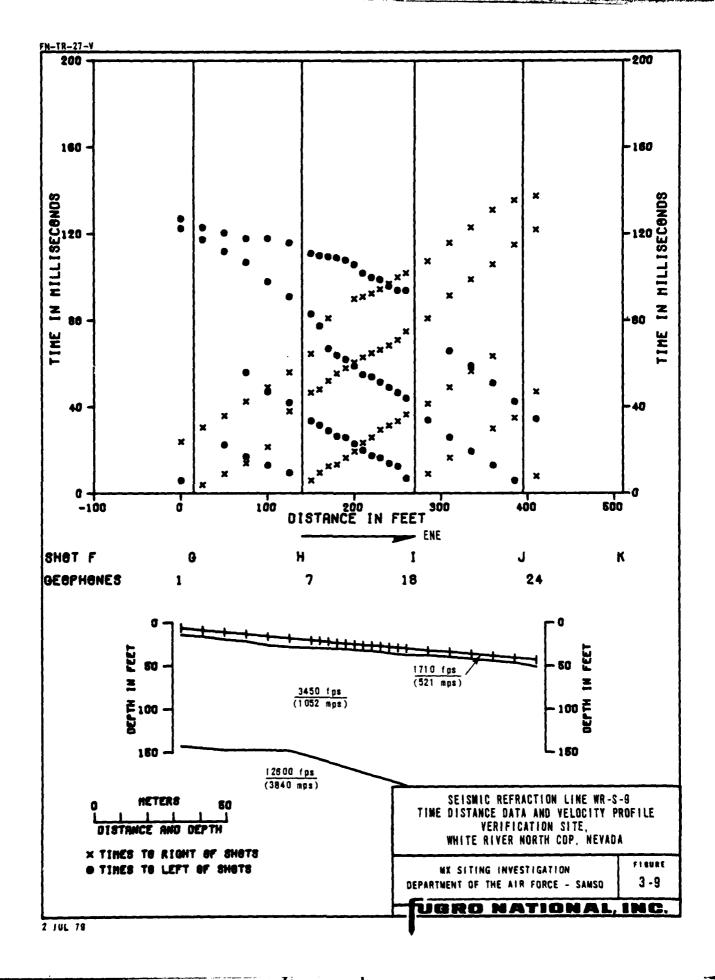


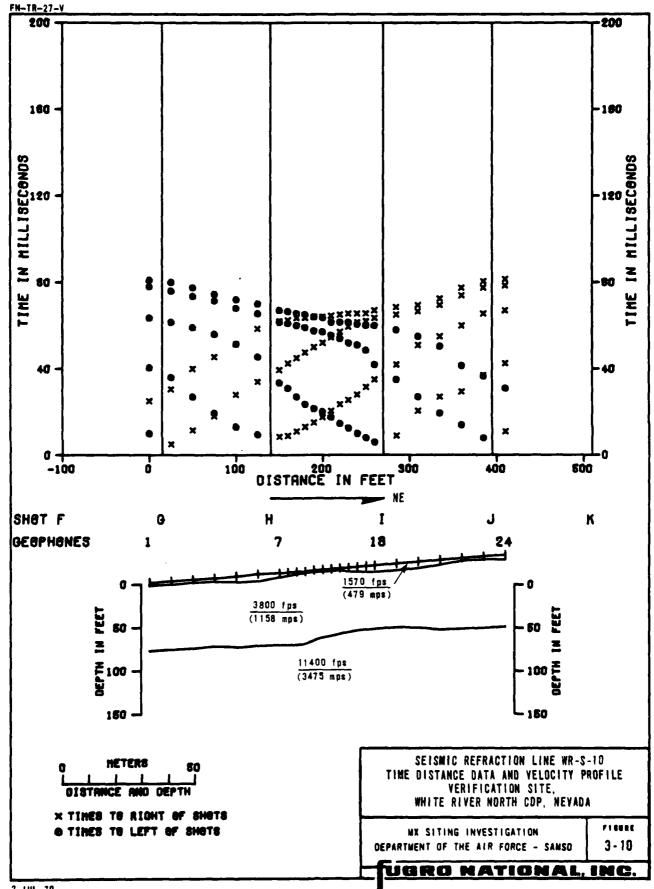


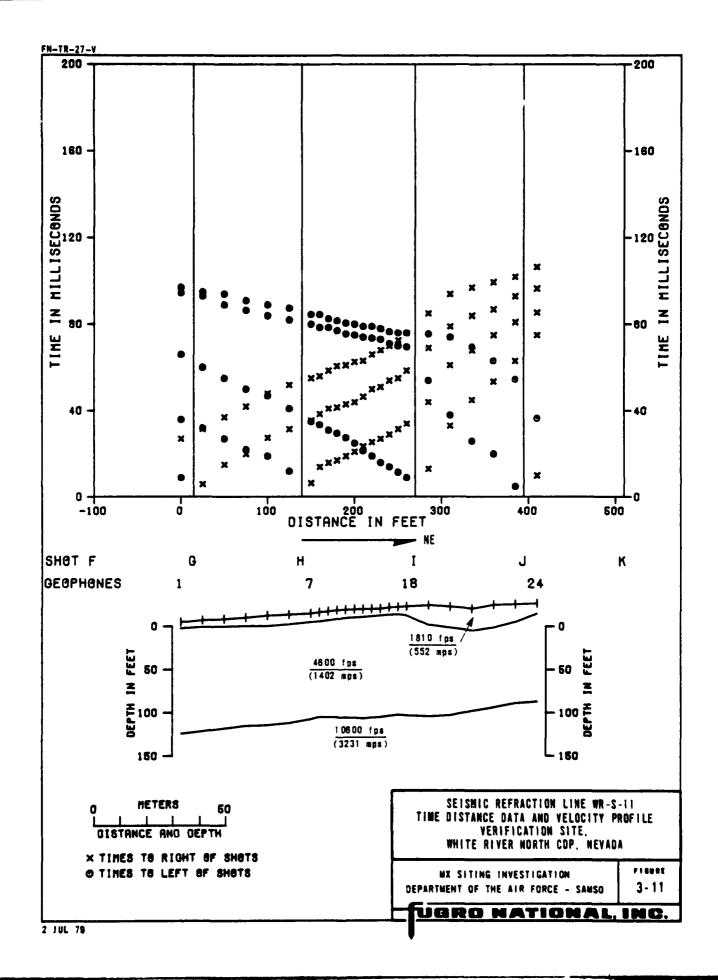


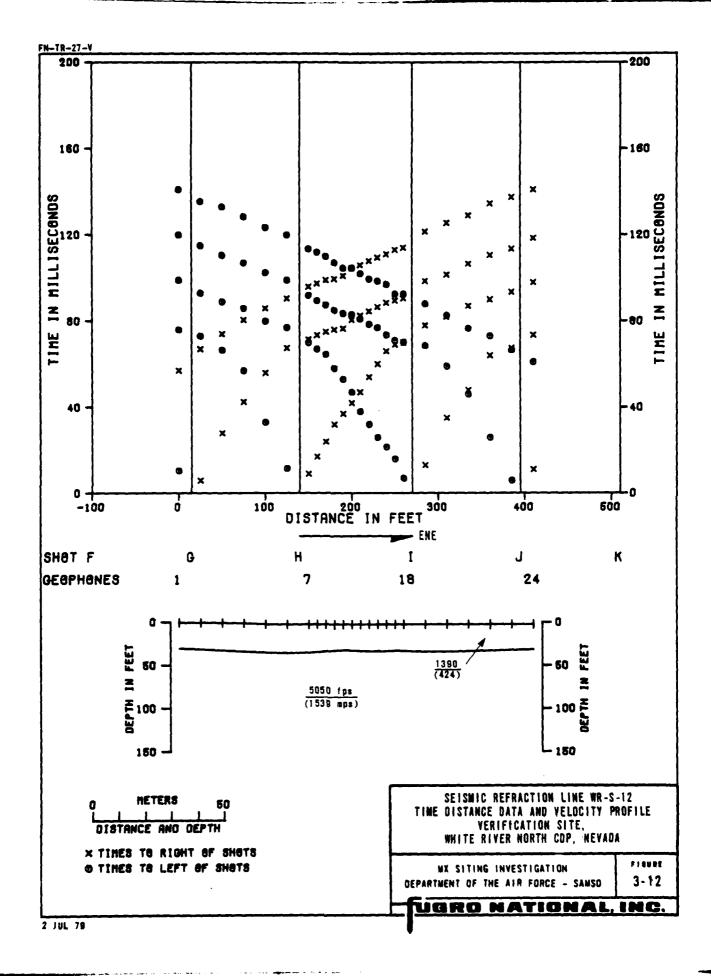


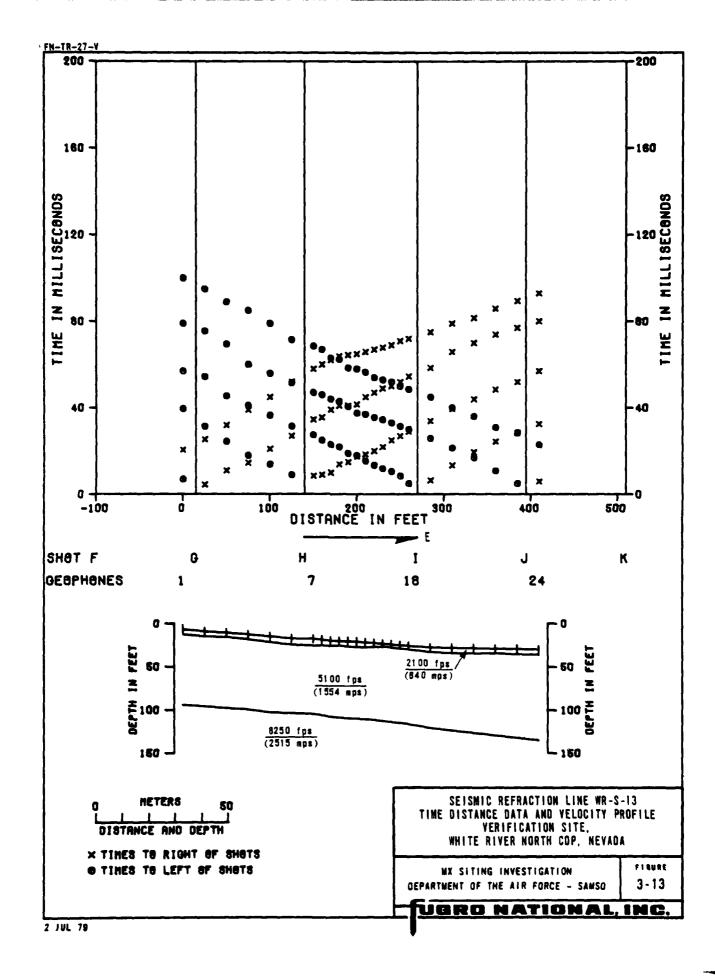


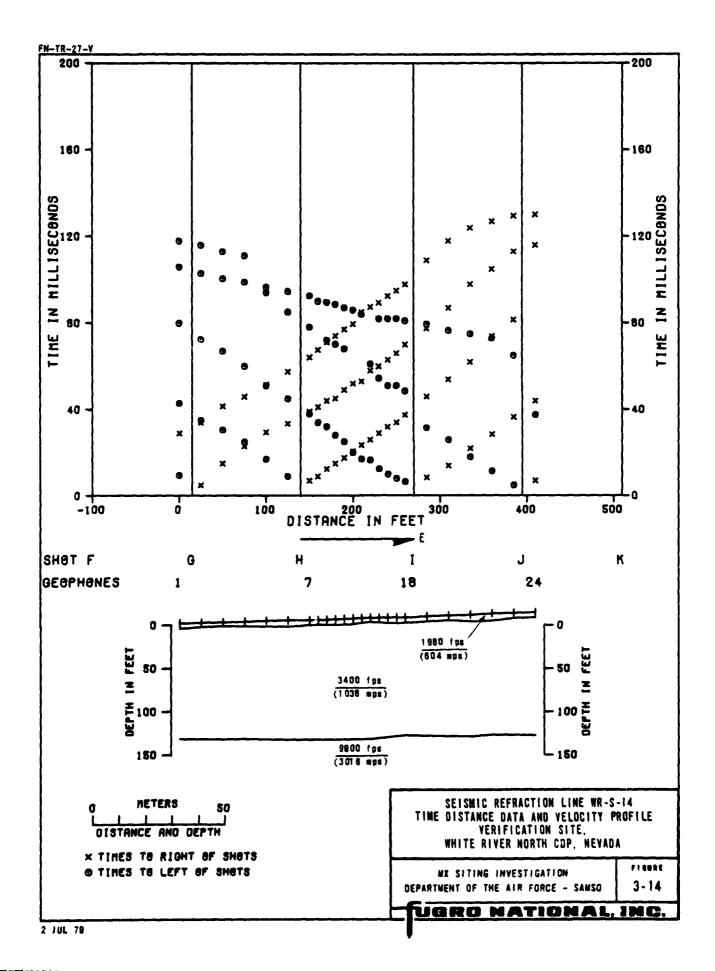


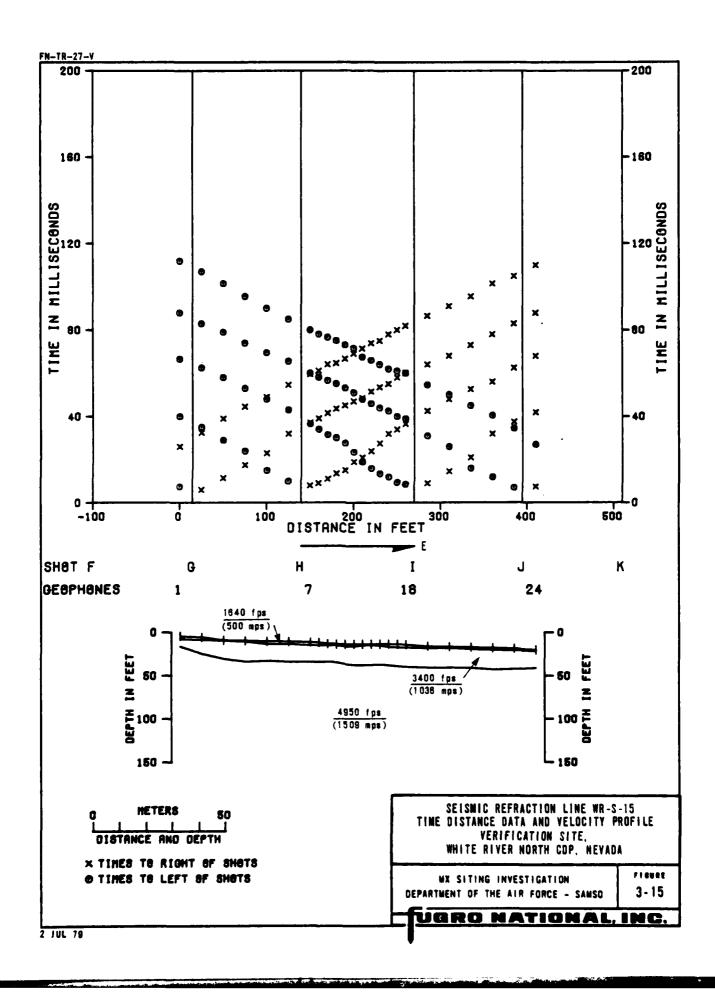


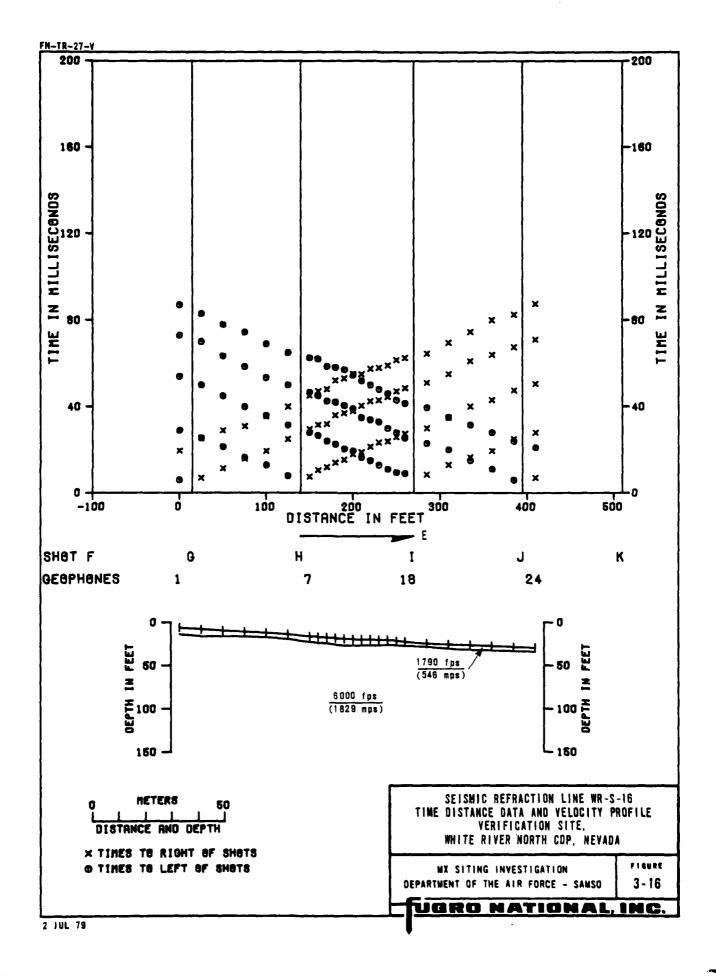


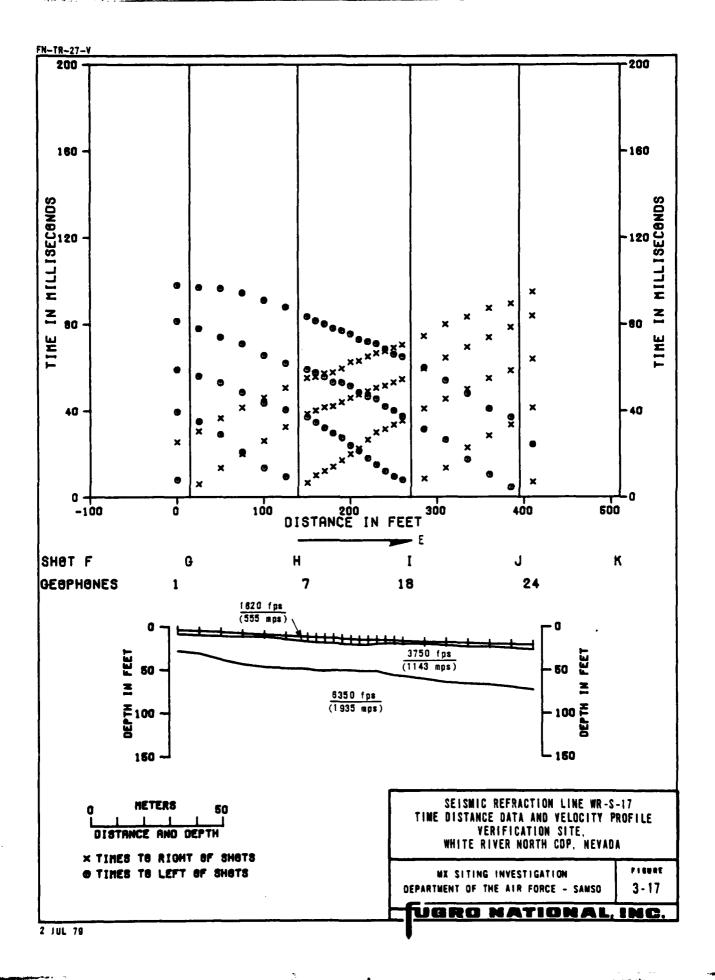


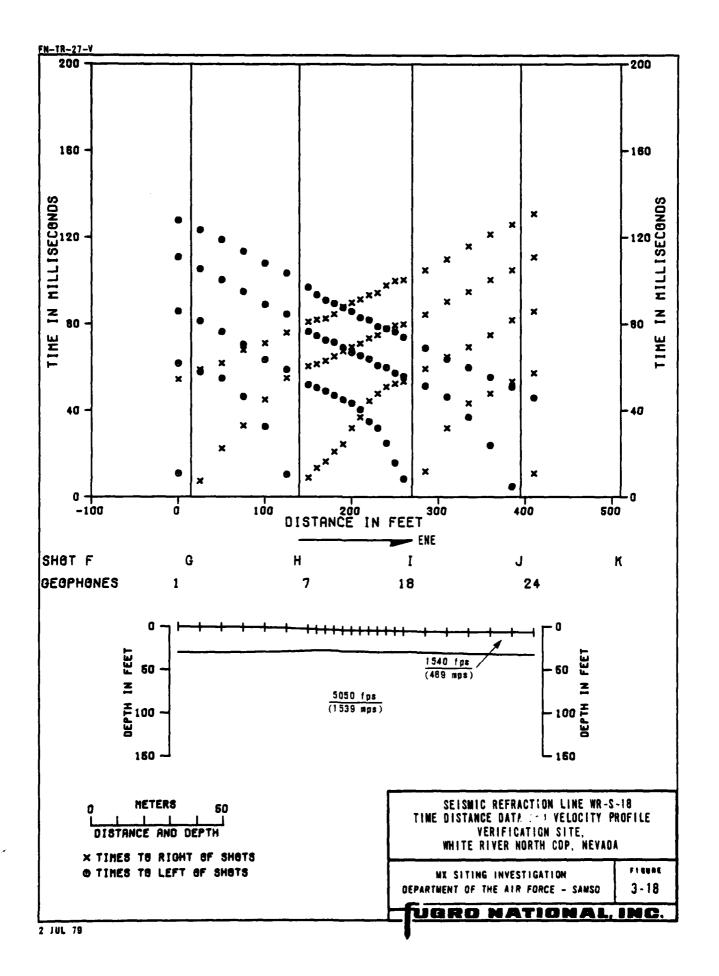


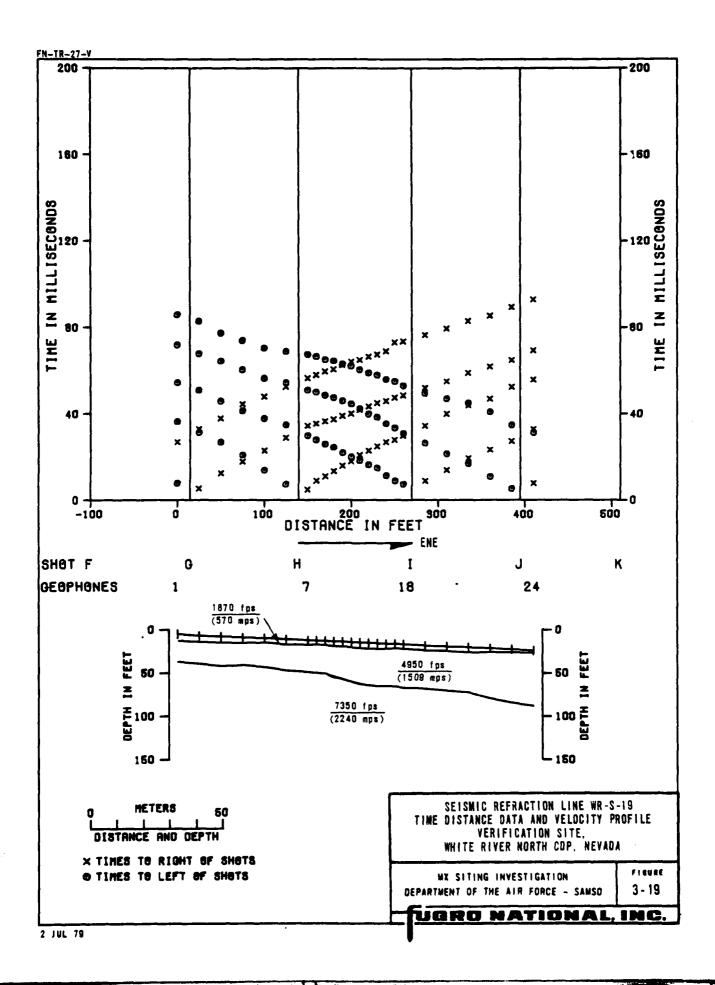












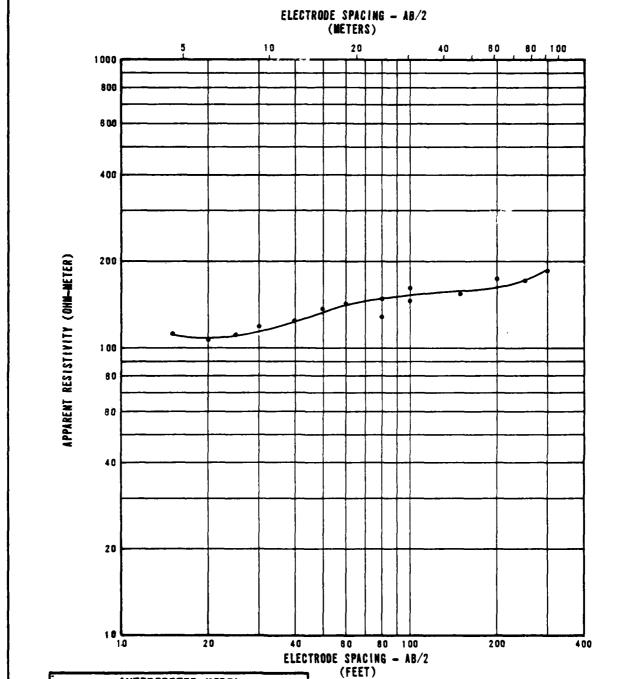
SECTION 4.0
ELECTRICAL RESISTIVITY DATA

EXPLANATIONS OF ELECTRICAL RESISTIVITY DATA

Each figure in this section presents the data obtained from a resistivity sounding and a tabulated model of resistivity layers that would produce a curve similar to the observed curve.

The upper portion of the figures is a graph in which measured apparent resistivity values in ohm-meters are plotted versus one-half the distance between the current electrodes.

The interpreted model tabulated at the bottom of the page shows a combination of true resistivity layers and thicknesses obtained by matching theoretical curves to the field curve.

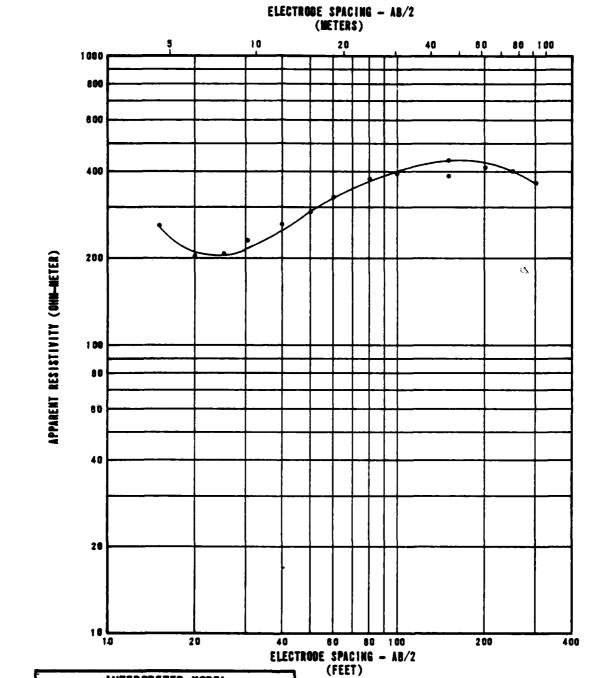


INTERPRETED MODEL		
LAYER DEPTH		RESISTIVITY VALUES
FEET	METERS	OHW-METER
0	0	100
21.	6	21 0
67	20	100
184	56	1700
	i	

RESISTIVITY SOUNDING WR-R-1 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER MORTH COP, NEVADA

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FIGURE 4-1

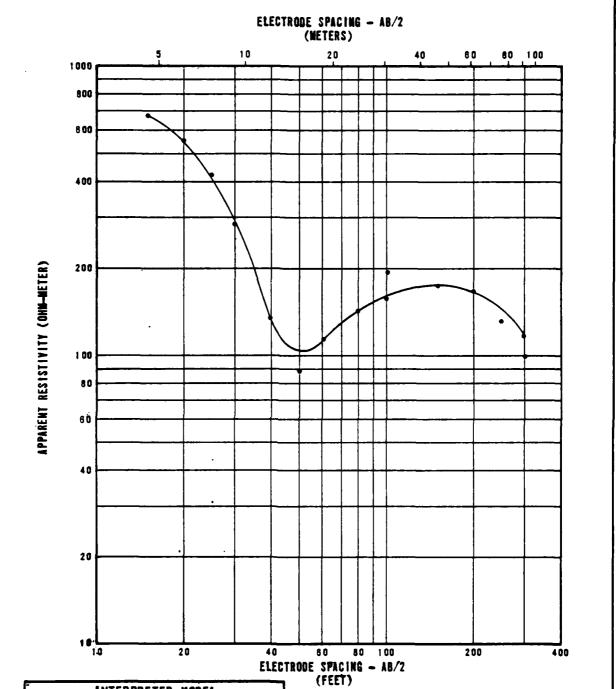


	INTERPRETED MODEL		
LAYE	R DEPTH	RESISTIVITY VALUES	
FEET	METERS	OH#-METER	
0	0	400	
5	2	170	
28	8	2490	
37	11	420	
122	37	170	
		1	

RESISTIVITY SOUNDING WR-R-2 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH CDP, NEVADA

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4-2



	INTERPRETED MODEL		
LAYE	DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	870	
13	4	170	
19	6	35	
30	9	210	
140	43	50	

RESISTIVITY SOUNDING WR-R-3
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE,
WHITE RIVER NORTH COP, NEVADA

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FIGURE 4-3

80

ELECTRODE SPACING - AB/2
(FEET)

	INTERPRETED MODEL		
LAYER	DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	Q	300	
7	2	180	
38	12	380	
189	58	220	
		(

20

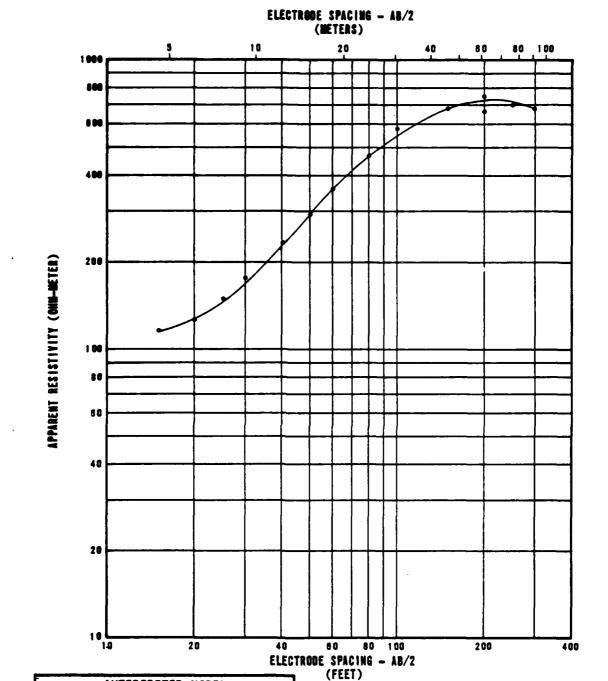
RESISTIVITY SOUNDING WR-R-4 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

200

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FIGURE 4-4

400

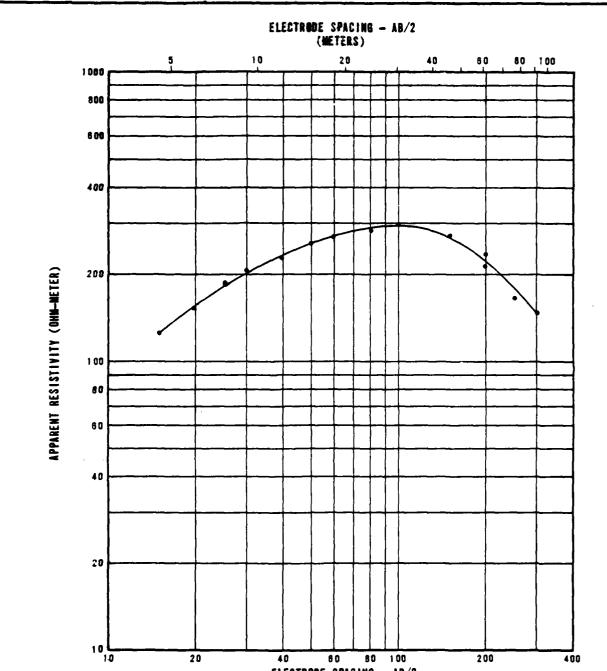


	INTERPRETED MODEL			
LAYE	LAYER DEPTH RESISTIVITY VALU			
FEET	METERS	OHW-METER		
0	0	90		
17	5	4750		
42	13	680		

RESISTIVITY SOUNDING WR-R-5 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP. NEVADA

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4-5



ELECTRODE SPACING - AB/2
(FEET)

	INTERPRE	TED MODEL
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	90
7	2	380
101	31	90
187	51	35

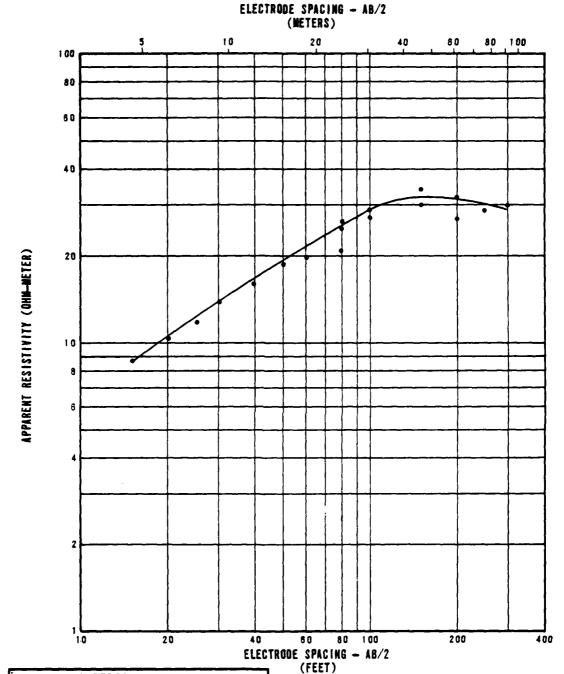
RESISTIVITY SOUNDING WR-R-6 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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4-6

lugro national, inc.





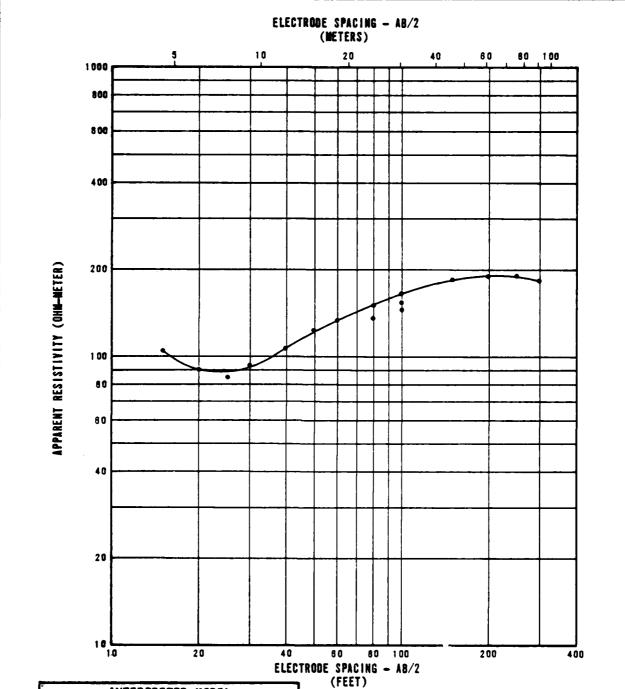
	INTERPRETED MODEL		
LAYER DEPTH		RESISTIVITY VALUE	
FEET	METERS	OHM-METER	
0	0	6	
9	3	30	
25	8	80	
86	20	30	
168	51	15	
	 	1	

RESISTIVITY SOUNDING WR-R-7 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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FIGURE 4-7

<u>ugro national, inc</u>

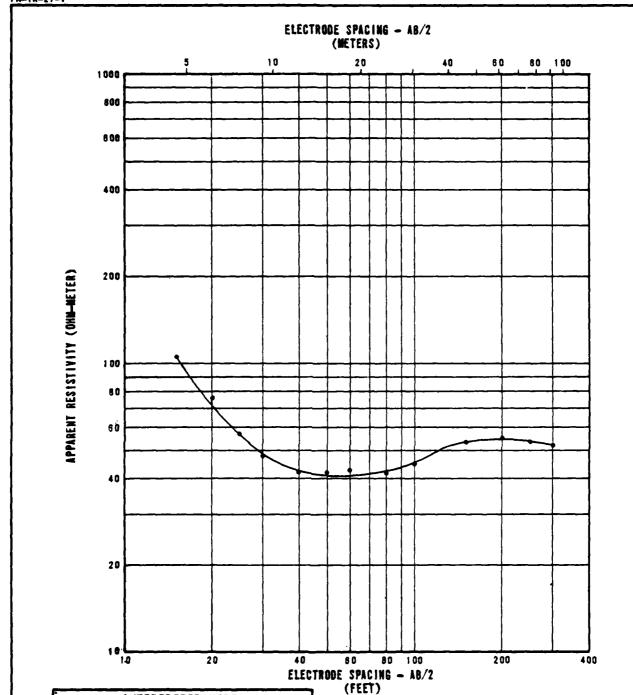


	INTERPRETED MODEL		
LAYE	R DEPTH	RESISTIVITY VALUE:	
FEET	METERS	OHW-METER	
0	0	160	
6	2	70	
26	8	380	
62	19	170	
205	62	110	

RESISTIVITY SOUNDING WR-R-8 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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FIGURE 4-8



	INTERPRETED MODEL		
LAYE	LAYER DEPTH RESISTIVITY VALUE		
FEET	METERS	OHM-METER	
0	0	1940	
7	2	370	
58	18	790	
166	51	320	
	T		

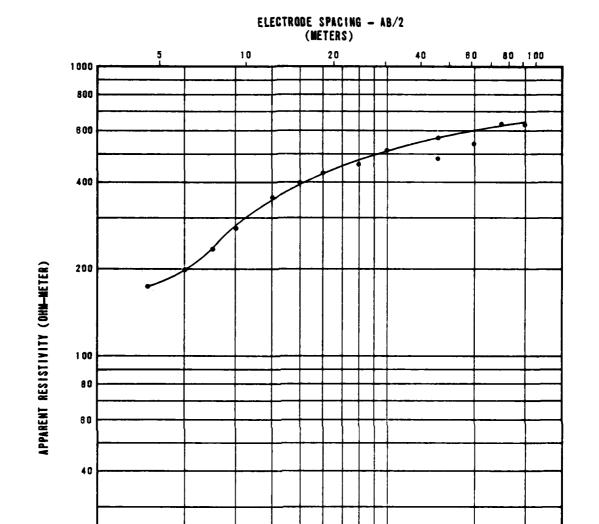
RESISTIVITY SOUNDING WR-R-9
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE,
WHITE RIVER NORTH COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSC

FIGURE 4-9

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AFY-15



10 ELECTRODE SPACING - AB/2 (FEET) INTERPRETER MOREL

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80

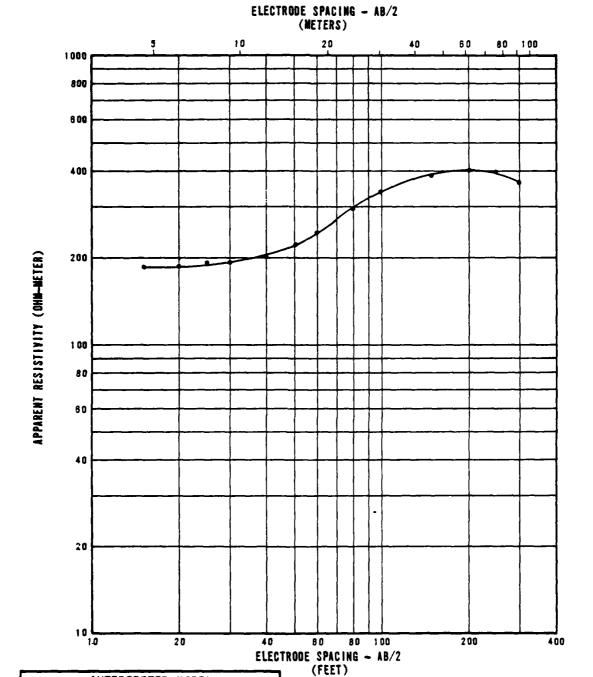
80 100

20

	INTERPRETED MUDEL		
LAYER	DEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	150	
11	3	670	
-	1		

RESISTIVITY SOUNDING WR-R-10 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER MORTH CDP. NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO FIGURE 4-10



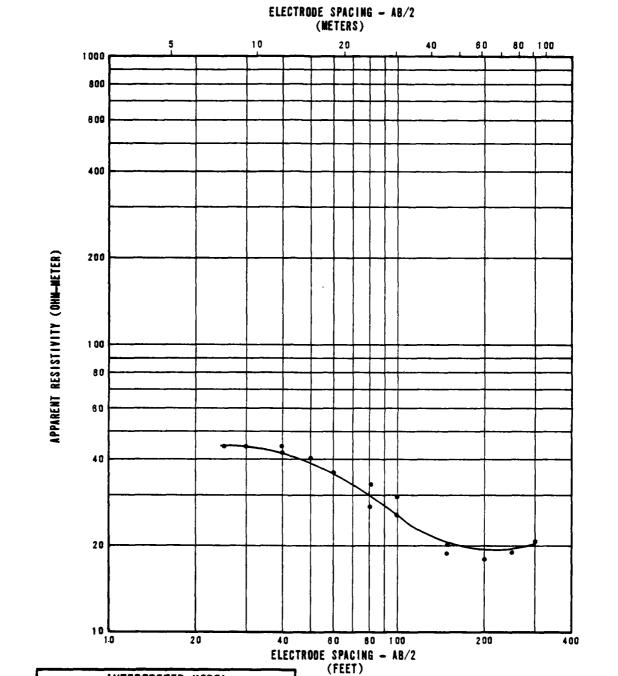
	INTERPRETED MODEL			
LAYE	R DEPTH	RESISTIVITY VALUES		
FEET	METERS	OHM-METER		
0	0	190		
33	10	590		
190	58	75		

RESISTIVITY SOUNDING WR-R-11 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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FIGURE 4-11

ugro nationa<u>l, inc</u>

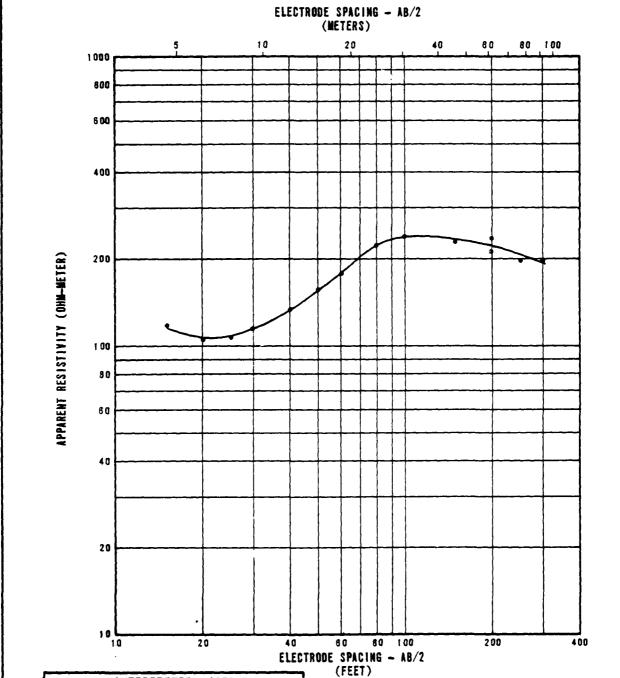


	INTERPRETED MODEL		
LAYE	RDEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0_	0	45	
36	11	14	
144	44	35	
		1	

RESISTIVITY SOUNDING WR-R-12 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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FIGURE 4-12



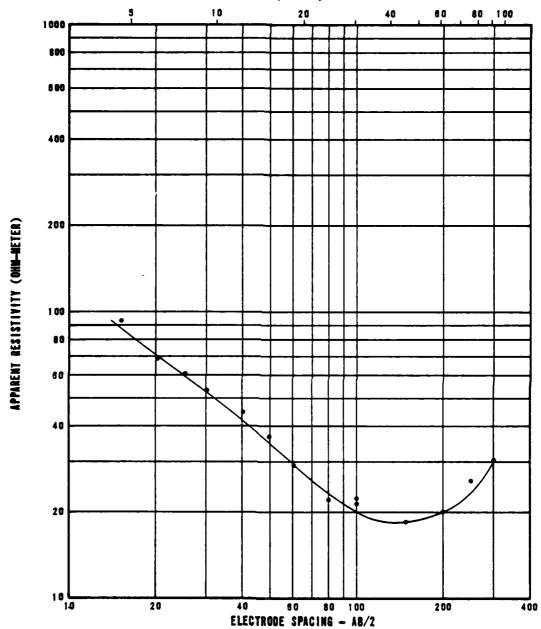
	INTERPRETED MODEL	
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	150
8	2	65
21	8	330
79	24	110

RESISTIVITY SOUNDING WR-R-13
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE.
WHITE RIVER NORTH COP. NEVADA

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4-13





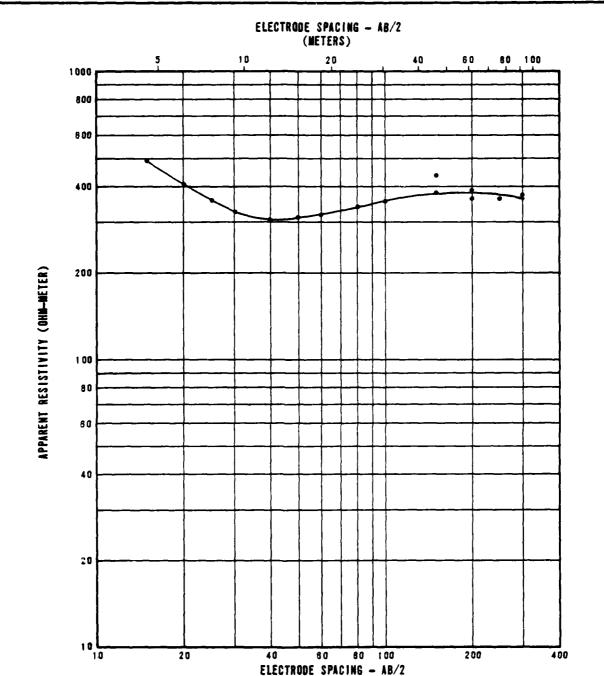
(FEET)

INTERPRETED MODEL		
LAYER	DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	120
g	3	17
131	40	170
156	48	580
		1

RESISTIVITY SOUNDING WR-R-14 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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4-14



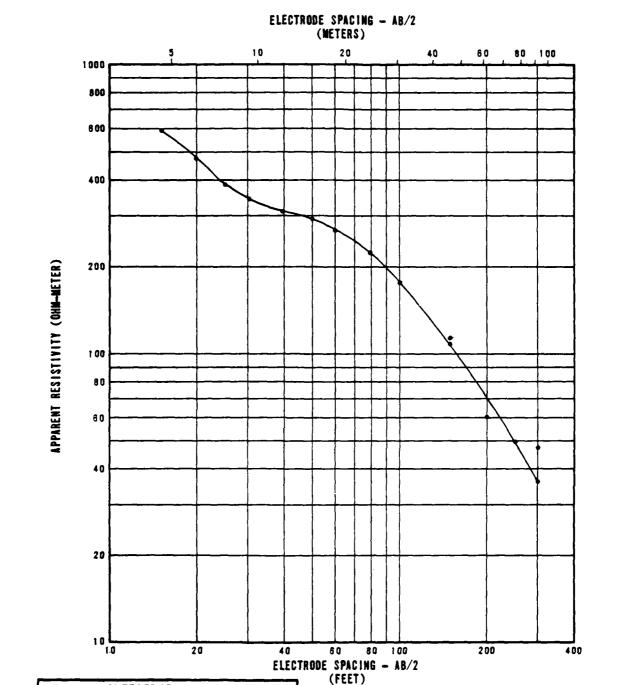
(FEET)

	INTERPRETED MODEL		
LAYER	RDEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	660	
8	2	230	
28	9	530	
59	18	340	
		1	

RESISTIVITY SOUNDING WR-R-15 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH CDP, NEVAGA

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4-15



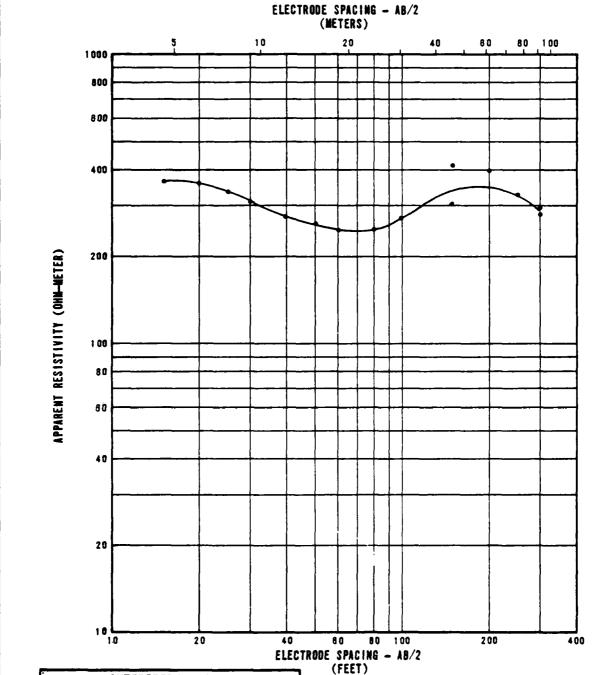
	INTERPRE	TED MODEL
LAYES	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	730
10	3	280
73	22	20

RESISTIVITY SOUNDING WR-R-16 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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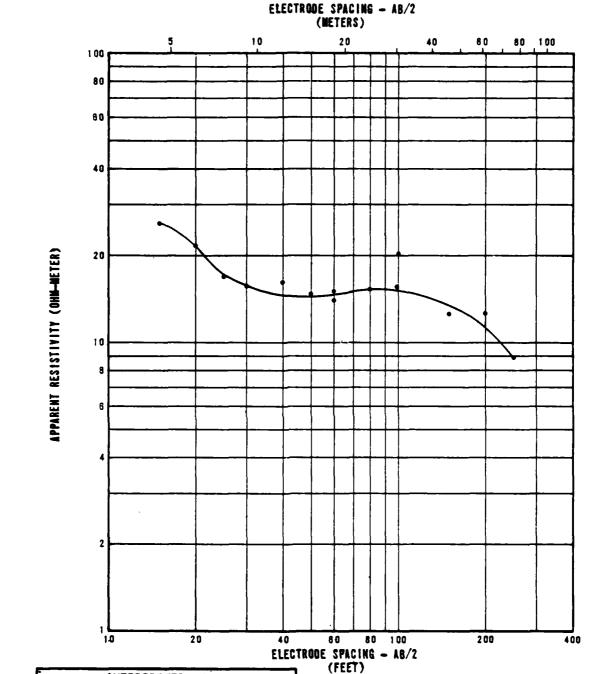
L	INTERPRE	
RESISTIVITY VALUES	LAYER DEPTH	
OH# METER	T METERS	FEET
390	0	0
200	4	14
2570	19	63
370	24	80
60	48	158
_		

RESISTIVITY SOUNDING WR-R-17 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH CDP, NEVADA

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	INTERPRETED MODEL	
LAYE	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	35
10	3	8
21	8	25
74	23	4

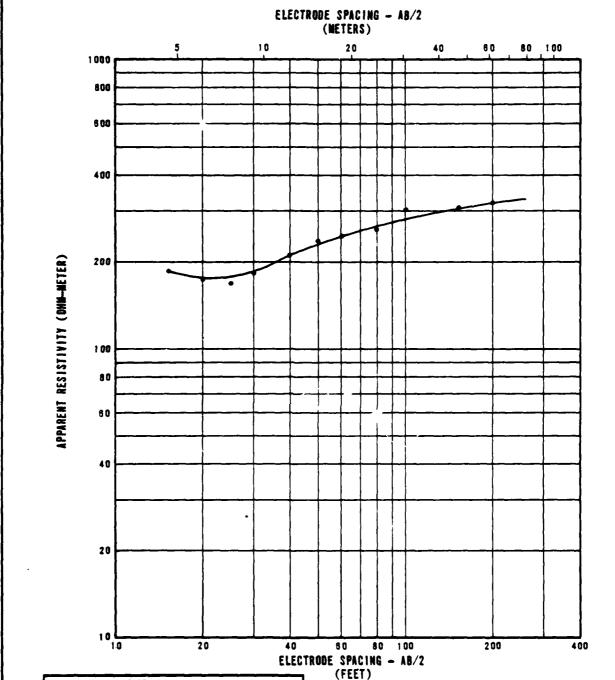
RESISTIVITY SOUNDING WR-R-18
SOUNDING CURVE AND INTERPRETATION
VERIFICATION SITE,
WHITE RIVER MORTH CDP, NEVADA

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4-18

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AFY-15

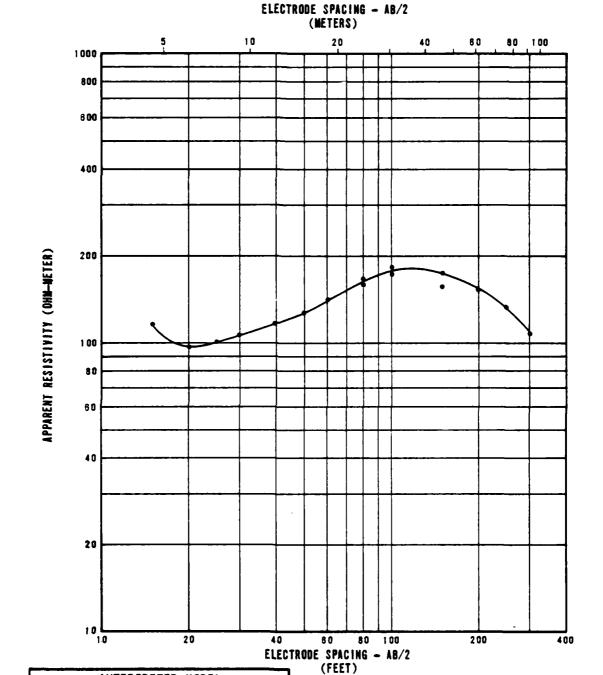


INTERPRETED MODEL		
LAYER DEPTH		RESISTIVITY VALUE
FEET	METERS	OHM-METER
0	0	200
7	2	150
20	8	340
	 	†
		

RESISTIVITY SOUNDING WR-R-19 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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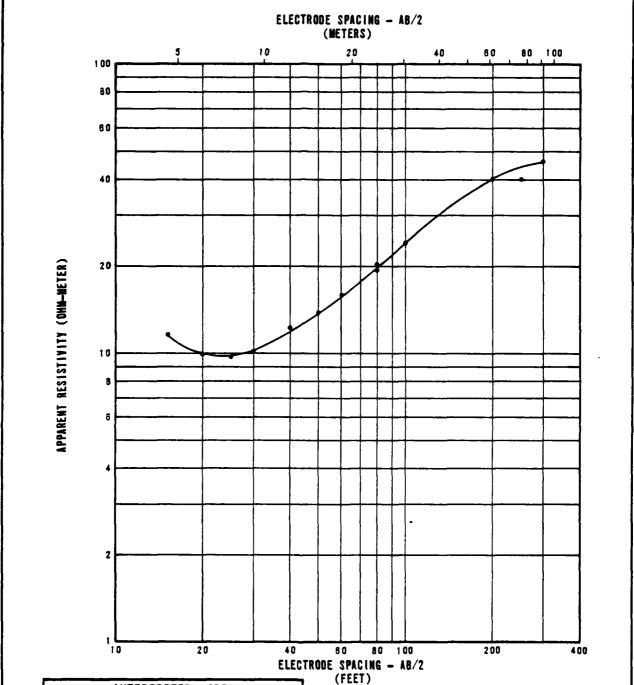


	INTERPRE	TED MODEL
LAYER DEPTH		RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	95
25	8	480
51	16	180
117	36	25
		1

RESISTIVITY SOUNDING WR-R-20 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH CDP. NEVADA

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4-20



	INTERPRETED MODEL		
LAYER	ROEPTH	RESISTIVITY VALUES	
FEET	METERS	OHM-METER	
0	0	9	
26	8	70	
172	52	50	
	J		

RESISTIVITY SOUNDING WR-R-21 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH COP, NEVADA

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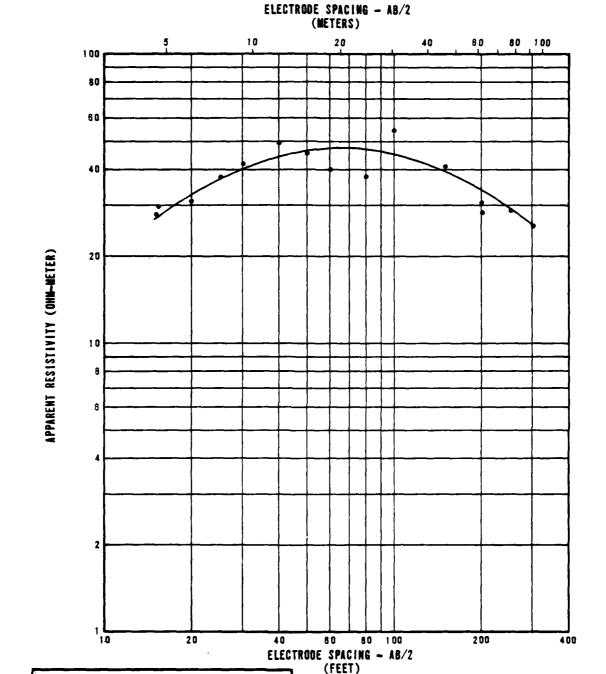
4-21

	INTERPRE	TED MODEL
LAYER	R DEPTH	RESISTIVITY VALUES
FEET	METERS	OHM-METER
0	0	50
31	9	20
	T	

RESISTIVITY SOUNDING WR-R-22 Sounding curve and interpretation Verification site, White river north CDP, Nevada

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FIGURE 4-22



LAYER DEPT	TERS	RESISTIVITY VALUES OHM-METER
FEET ME	TERS	OH#-METER
0		mm + m+
U	0	19
7	2	85
42	13	40
101	31	17

RESISTIVITY SOUNDING WR-R-23 SOUNDING CURVE AND INTERPRETATION VERIFICATION SITE, WHITE RIVER NORTH CDP, NEVADA

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SECTION 5.0 GRAVITY DATA

EXPLANATIONS OF GRAVITY DATA

Gravity data were not available in time (prior to June 1979) for incorporation into this report. A supplemental report containing gravity data and results will be issued at a later date.

SECTION 6.0

BORING LOGS

EXPLANATIONS OF BORING, TRENCH, AND TEST PIT LOGS

All data from borings, trenches, and test pits are presented on standard Fugro National logs in Sections 6.0 and 7.0. The following explanations are provided as a key to the logs.

A. Designations - Borings, trenches, and test pits are identified as follows:

WW-B-1

WW - abbreviation for the site (e.g., WW-Whirlwind)

- B abbreviation for activity (e.g., B-boring, T-trench, P-test pit)
- l number of activity
- B. Sample Type Different sampling techniques were used and the symbols are explained at the bottom of the boring logs. For details of sampling techniques, see Section A5.0 of Appendix in Volume I. Horizontal lines, to scale, indicate the depth where sampling was attempted.
- C. Percent Recovery The numbers shown represent the ratio (in percent) of the soil sample recovered in the sampler to the full penetration of the sampler.
- D. N Value Corresponds to standard penetration resistance, which is number of blows required to drive a standard split-spoon sampler for the second and third of three 6-inch (15 cm) increments with a 140-pound (63.5 kg) hammer falling 30 inches (76 cm) (ASTM D 1586-67).
- E. Depth Corresponds to depth below ground surface in meters and feet.
- F. Lithology Graphic representation of the soil and rock types.

- G. USCS Unified Soil Classification System (see Table 6-1 for complete details) symbols.
- H. Soil Description Except in cases where samples were classified based on laboratory test data, the descriptions are based on visual classification. The procedures outlined in ASTM D 2487-69, Classification of Soils for Engineering Purposes, and D 2488-69, Description of Soils (Visual-Manual Procedure) were followed. Solid lines across the column indicate known change in strata at the depth shown.

Definitions of some of the terms and criteria to describe soils and conditions encountered during the exploration follow.

Gradation: A coarse-grained soil is well graded if it has a wide range in grain size and substantial amounts of most intermediate particle sizes.

Poorly graded indicates that the soil consists predominantly of one size (uniformly graded) or has a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

Moisture : Dry - no feel of moisture

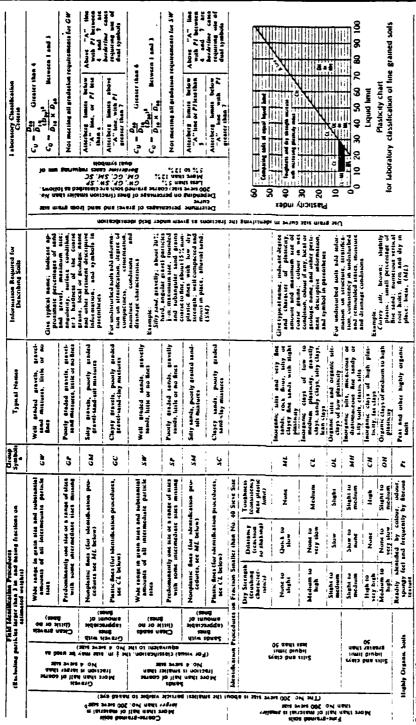
Slightly Moist - much less than normal moisture

Moist - normal moisture for soil Very Moist - much greater than normal

moisture

Wet - for soils below the water

table (if known)



From Wagner, 1937.

S. Sambors Soule poversing characteristics of two groups are designated by combinations of group symbols. For example C.W. C.C. well graded gravel-and mixture with clay binder.

A Mixture two that characters are U.S. satisfied.

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UNIFIED SOIL CLASSIFICATION SYSTEM

WX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

Consistency: Consistency descriptions of coarse-grained soils (GW, GP, GM, GC, SW, SP, SM, SC) are as follows.

Consistency	N Value (ASTM D 1586-67)
Very Loose Loose	0 - 4 4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	>50

Consistency descriptions of fine-grained soils (ML, CL, MH, CH,) are as follows:

	Shear S	Strength	
Consistency	(ksf) (kn/m^2	<u>Fielä Guide</u>
Very Soft	0.25	12	Sample with height equal to twice the diameter, sags under own weight
Soft	0.25- 0.50	12 - 24	Can be squeezed between thumb and forefinger
Firm	0.50- 1.00	24 - 48	Can be molded easily with fingers
Stiff	1.00-2.00	48 - 96	Can be imprinted with slight pres- sure from fingers
Very Stiff	2.00- 4.00	96- 192	Can be imprinted with considerable pressure from fingers
Hard	over 4.00	over 192	Cannot be im- printed by fingers

Grain Shape: Angular - particles have sharp edges and relatively plane sides with unpolished surfaces.

The second secon

Subangular - particles are similar to angular but have somewhat rounded edges.

Subrounded - particles exhibit nearly plane sides but have well-rounded corners and edges.

Rounded - particles have smoothly curved sides and no edges.

Calcareous: Containing calcium carbonate; presence of calcium carbonate is commonly identified on the basis of reaction with dilute hydrochloric acid.

Caliche : Soils cemented by porous calcium carbonate and/or other soluble minerals by upward-moving solutions.

Degree of

Cementation: (Stages of development of caliche profile)

<u>Stage</u>	Gravelly Soils	Nongravelly Soils
I	Thin, discontinu- ous pebble coatings	Few filaments or faint coatings
II	Continuous pebble coatings, some interpebble fill-ings	Few to abundant nodules, flakes, filaments
III	Many interpebble fillings	Many nodules and internodular fillings
IV	Laminar horizon overlying plugged horizon	Increasing carbon- ate impregnation

Secondary

Material : Example - Sand with trace to some silt

Trace - 5-12% (by dry weight) Little - 13-20% (by dry weight) Some - >21% (by dry weight) Plasticity: Plasticity index is the range of water content, expressed as a percentage of the weight of the oven-dried soil, through which the soil is plastic. It is defined as the liquid limit minus the plastic limit. Descriptive ranges used on the logs include:

Nonplastic (PI, 0 - 4) Slightly Plastic (PI, 4 - 15) Medium Plastic (PI, 15 - 30) Highly Plastic (PI, >31)

Cobbles and Boulders

A cobble is a rock fragment, usually rounded by weathering or abrasion, with an average diameter ranging between 3 and 12 inches (8 and 30 cm).

A boulder is a rock fragment, usually rounded by weathering or abrasion, with an average diameter of 12 inches (30 cm) or more.

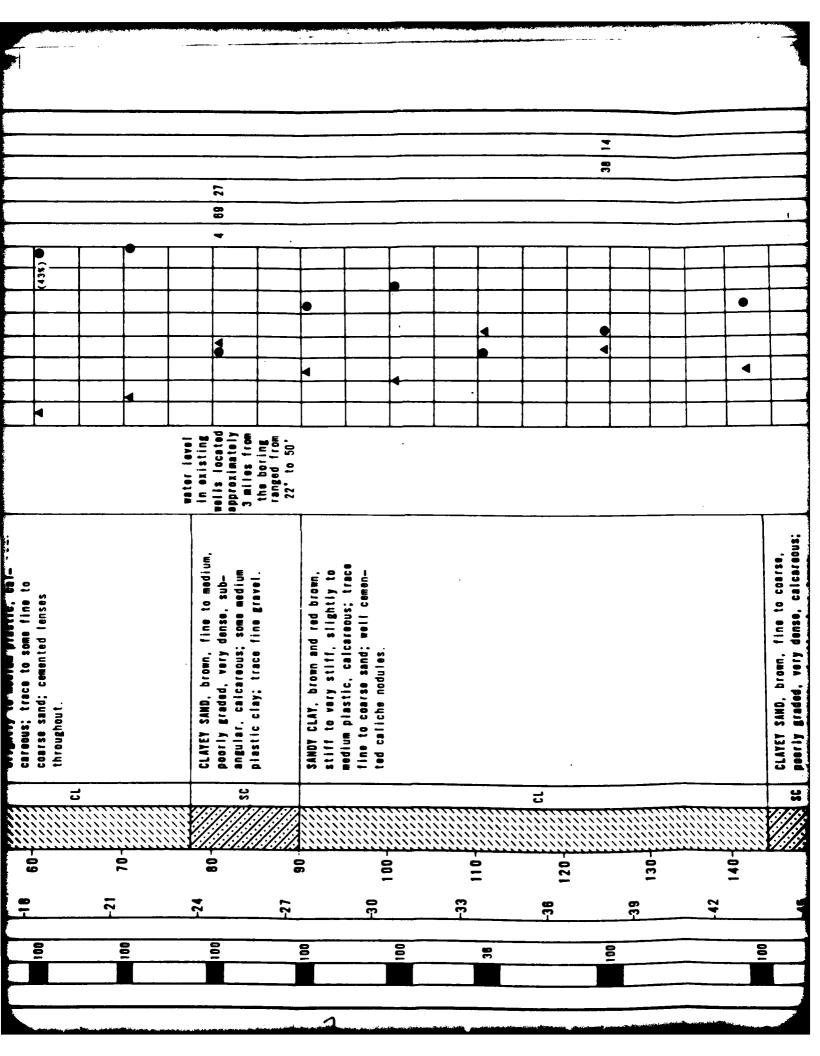
- I. Remarks This column was provided on boring and trench logs for comments regarding drilling difficulty, number and size of cobbles or boulders encountered, trench wall stability, loss of drilling fluid in the boring, and other conditions encountered during drilling and excavations.
- Dry Density and Moisture Content The boring logs include a graphical display of laboratory test results for dry density (ASTM D 2937-71) in pounds per cubic foot and kilograms per cubic meter and moisture content (ASTM D 2216-71) in percent from representative samples taken during drilling. The symbols are explained at the bottom of the boring logs.

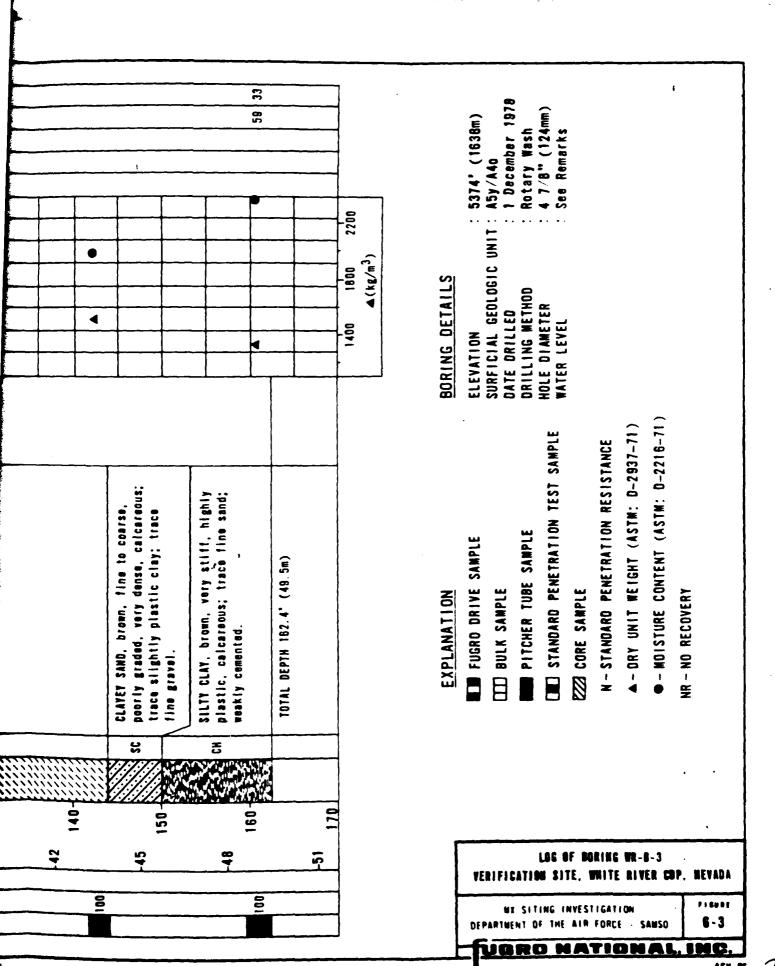
- K. Seive Analysis The numbers represent the percentage by dry weight (ASTM D 422-63) of each of the following soil components:
 - GR Gravel, rock particles that will pass a 3-inch (76 mm) sieve and are retained on No. 4 (4.75 mm) sieve.
 - SA Sand, soil particles passing No. 4 sieve and retained on No. 200 (0.075 mm) sieve.
 - FI Fines, silt or clay, soil particles passing No. 200 sieve.
- L. Atterberg Limits (LL and PI) -
 - LL Liquid Limit, the water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
 - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
 - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
 - NP Nonplastic.
- M. Miscellaneous Information -
 - Elevations indicated elevations on the logs are estimated from topographic maps of the study area, within an accuracy of half the contour interval.
 - Surficial
 - Geologic Unit indicates the surficial geologic unit in which the activity is located.
 - Date Drilled indicates the period from beginning to completion of the activity.
 - Drilling
 - Method signifies the type of drilling procedure used such as rotary wash.
 - Hole Diameter nominal size of boring drilled.
 - Water Level indicates depth from ground surface to water table where encountered.

Trench Length - length at ground surface of final trench excavation.

Trench
Orientation - bearing of longitudinal trench centerline.

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	SOIL		brown, fine,	Careous; some	SILTY CLAY, light brown to brown	plastic, calcaraous; trace to come some fine to coarse sand; well	cemented caliche nodules.	5		3		comented cell	astic.	.0	brown.
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-	USCS NOT OF		SILTY SAND, brown, fine, graded, loose, subangular	Careous; some	SILTY CLAY, I	ਰ 	comented caliche nodules.				SILTY SAND.	Comented cell	SILTY CLAY, 11ght stick, 11ght	Sand (51.0"-54.0"	brown.
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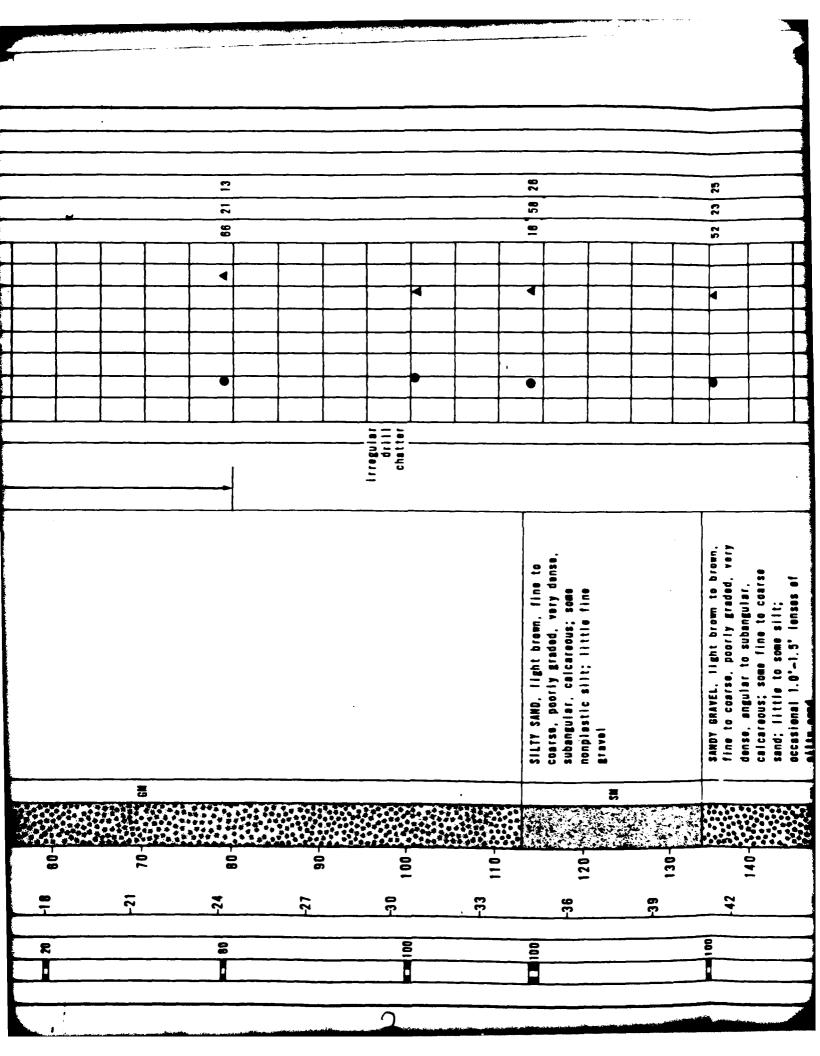
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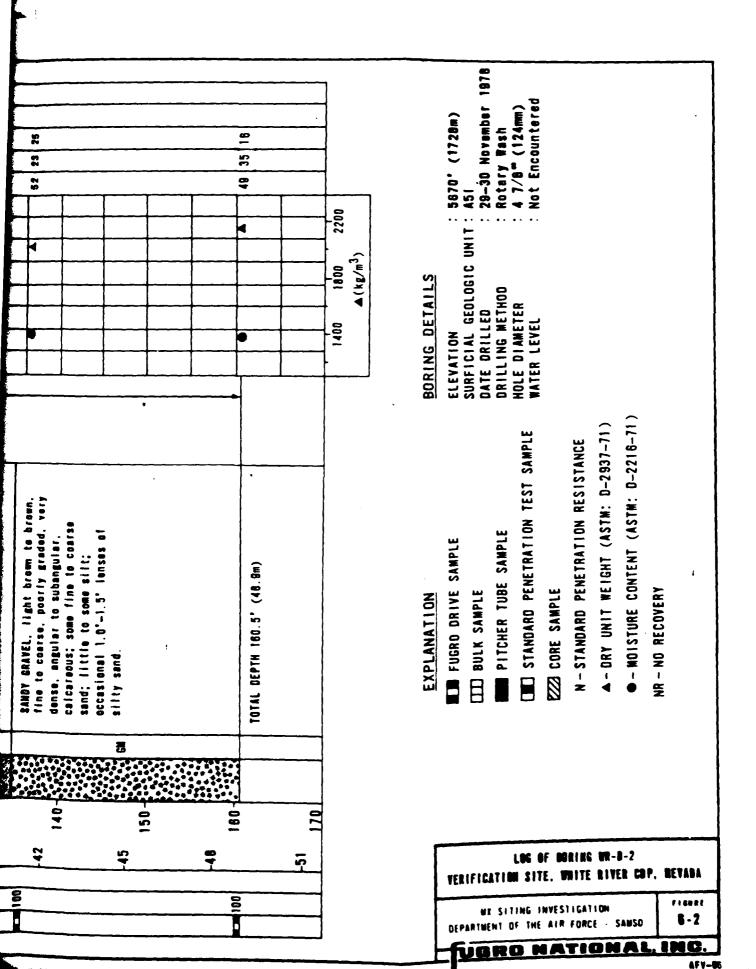
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ANALYSIS

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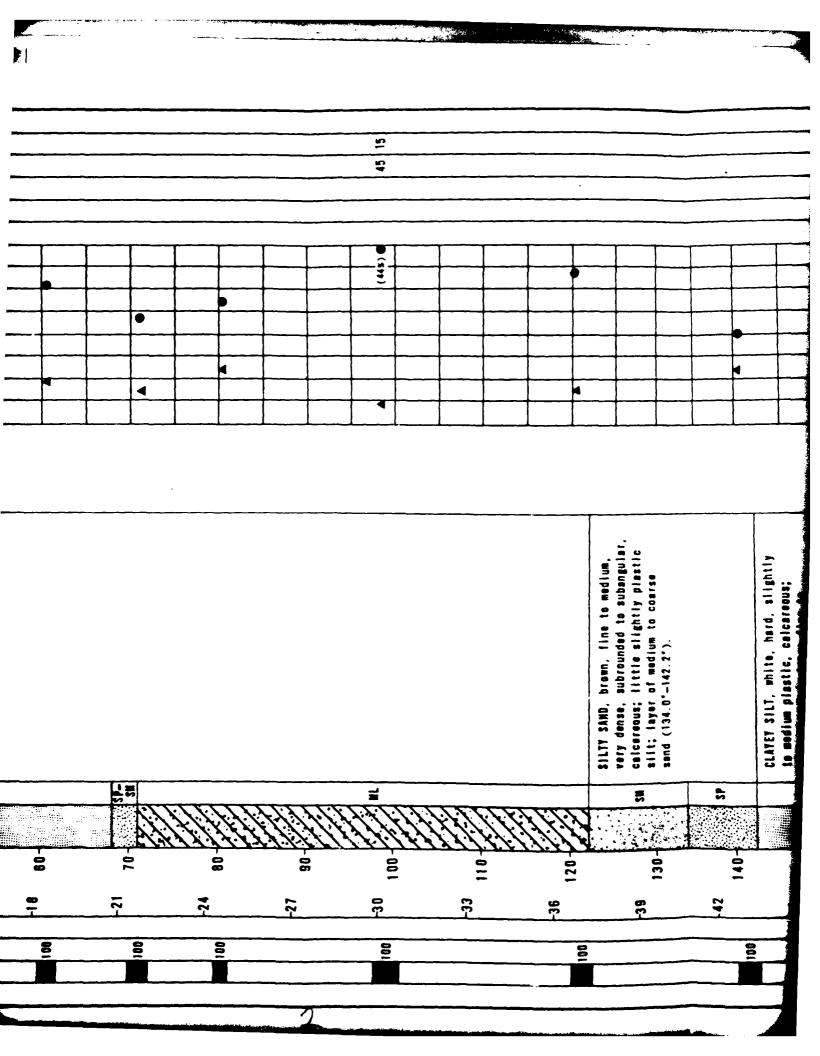
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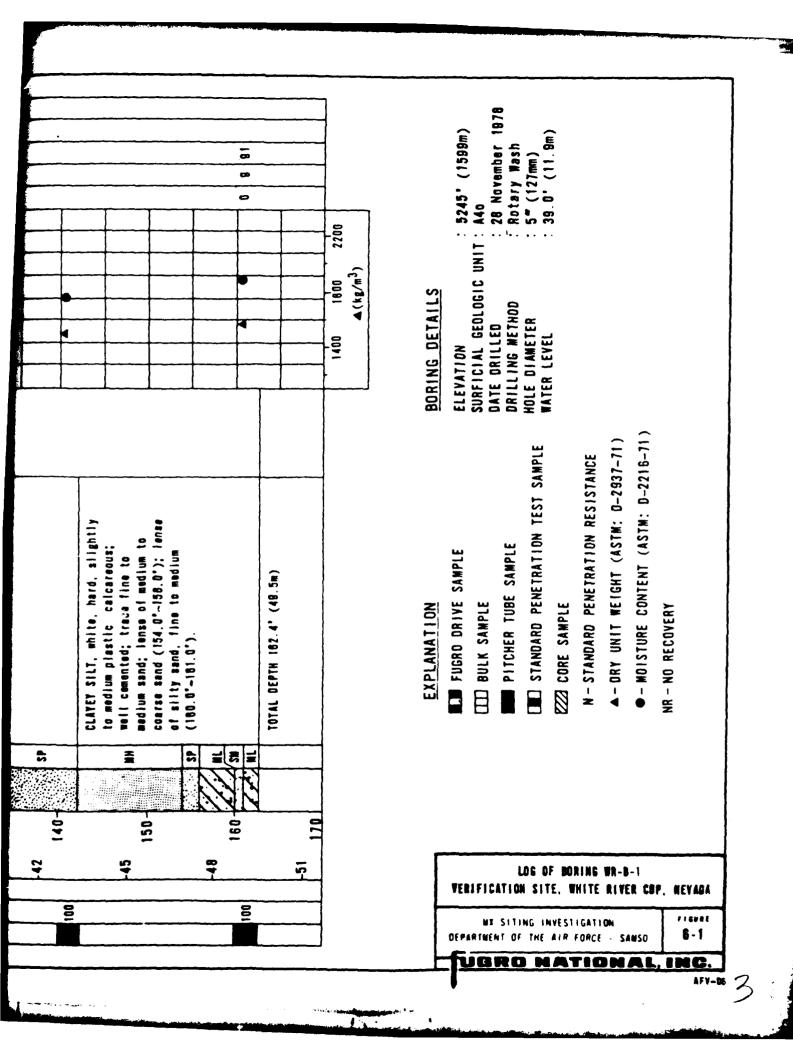




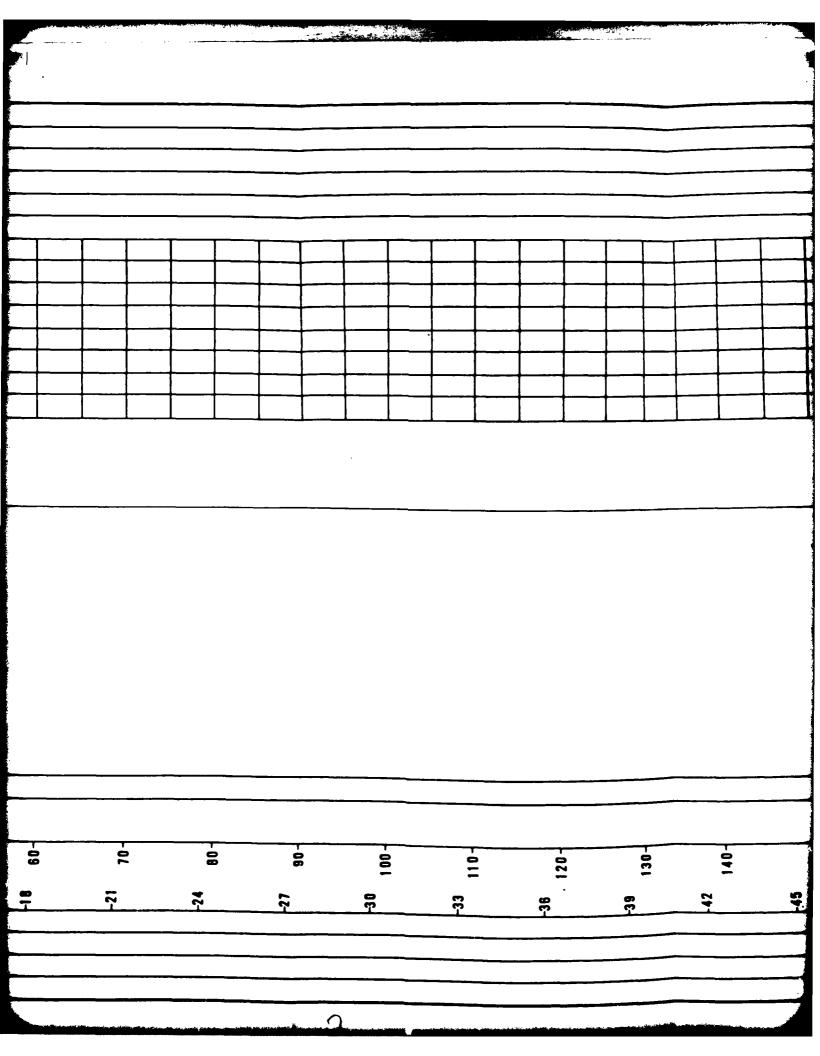
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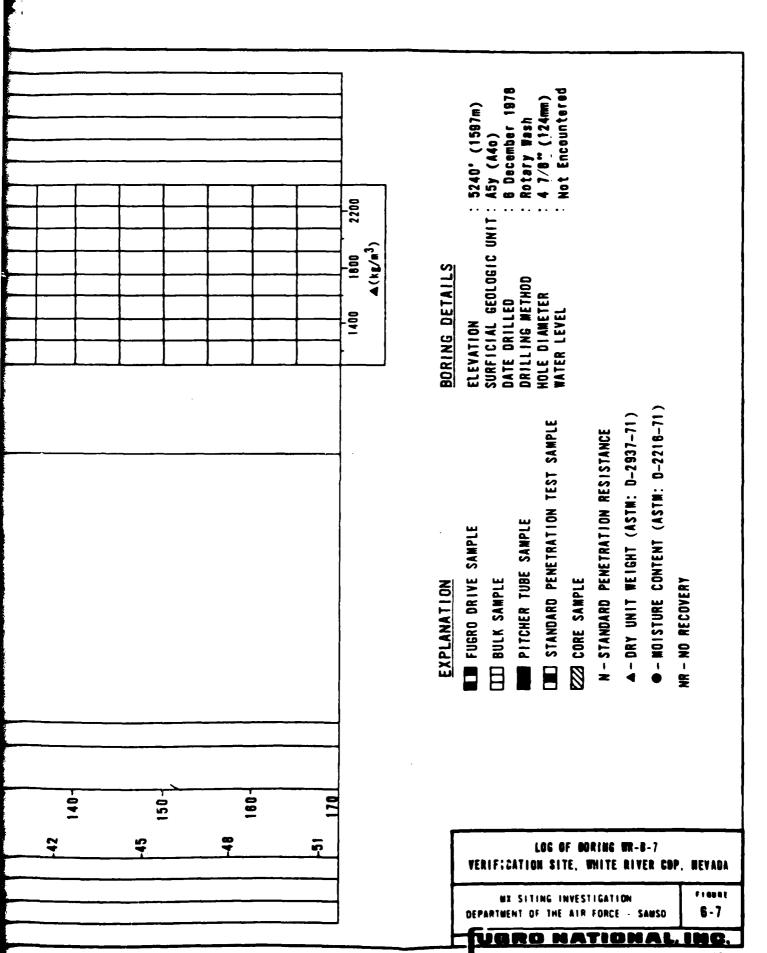
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	SOIL DESCRIPTION	- 1	SiLTY SAND, light brown to brown, fine to coarse, poorly graded.	medium dense to very dense, cal- careous; little to some nonplastic	- .						SANDY SILT, brown, stiff, slightly plastic, calcaraous; some fine to	medium sand.	TOTAL DEPTH 51.0" (15.5m)	
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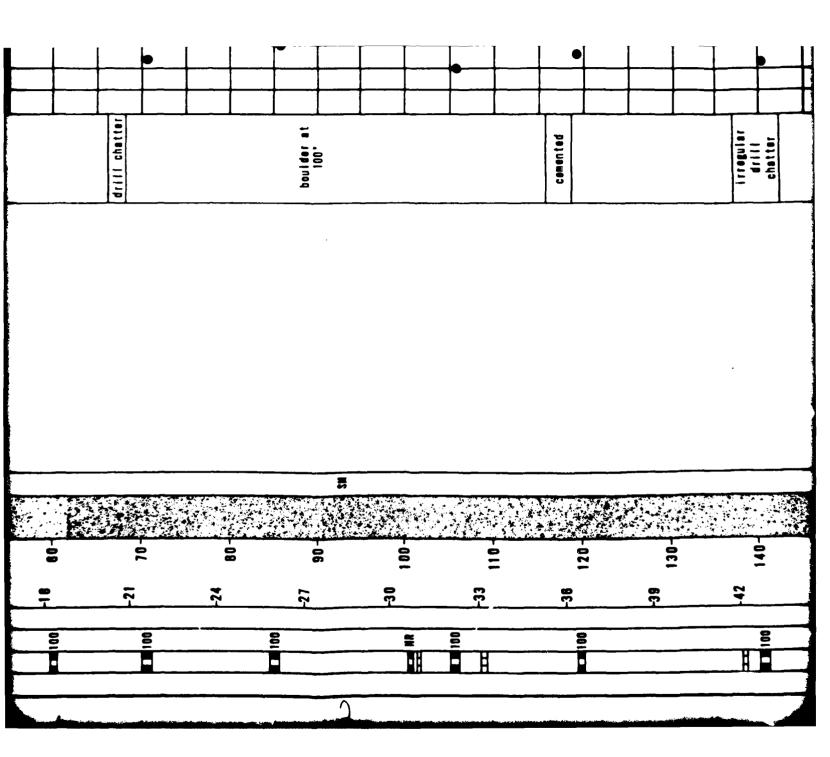


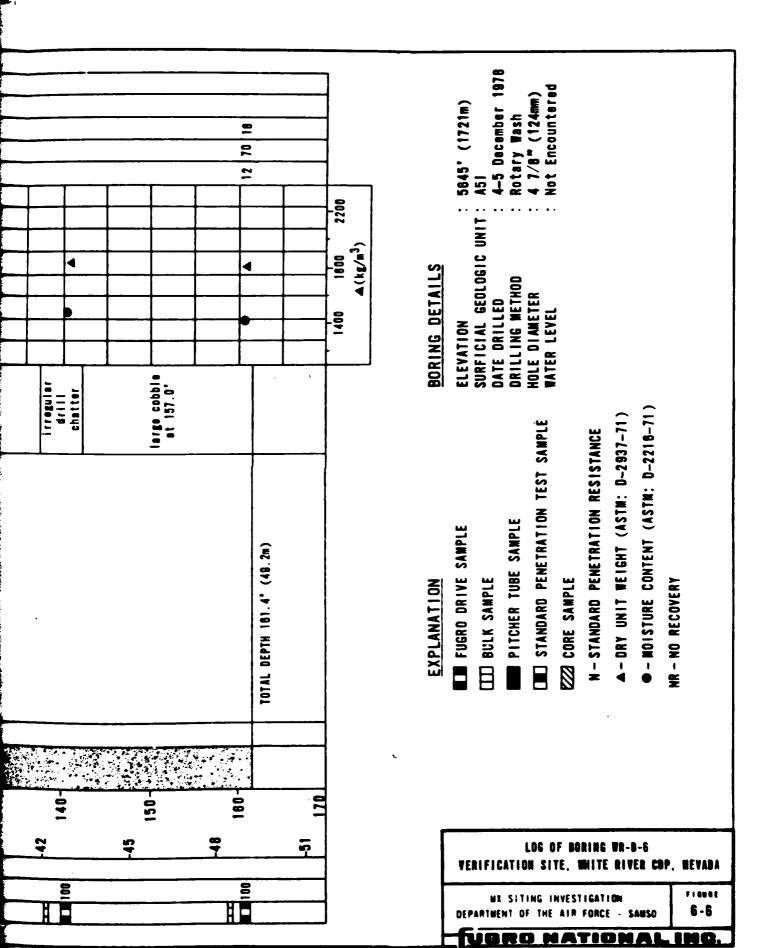


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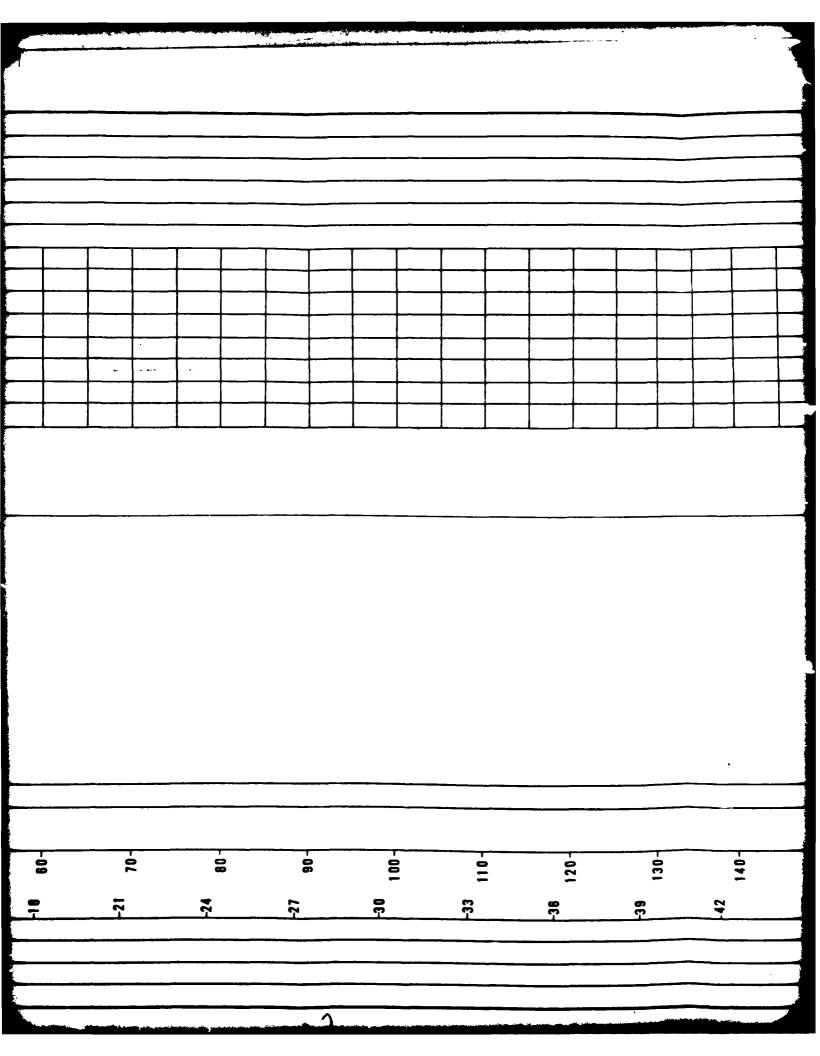
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	SOIL DESCRIPTION		GRAVELLY SAND, light brown to brown.	9	fine to coarse gravel; trace to some	silt; cemented nodules.			SANDY GRAVEL, light brown, fine to	Coarse, well to poorly graded, very dense, subangular, calcareous; some					GRAVELLY SAND, yellow brown to red brown, fine to coarse, poorly graded	= -	(35 -12) throughout	•		
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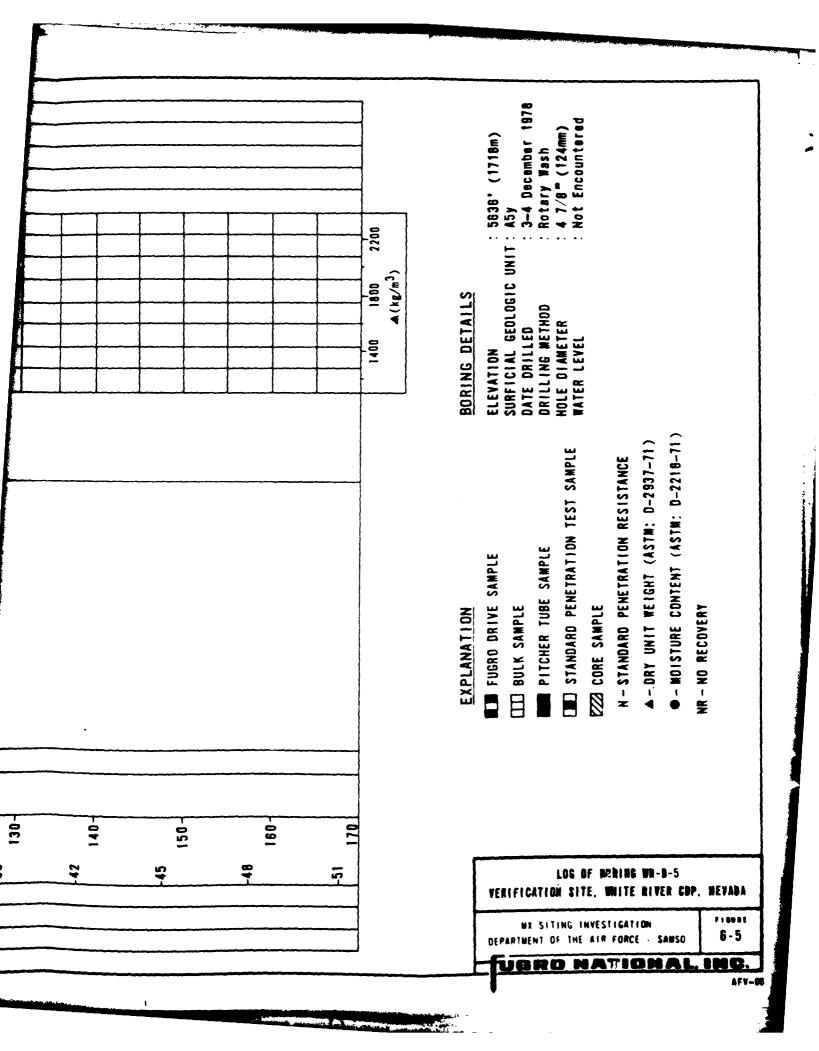
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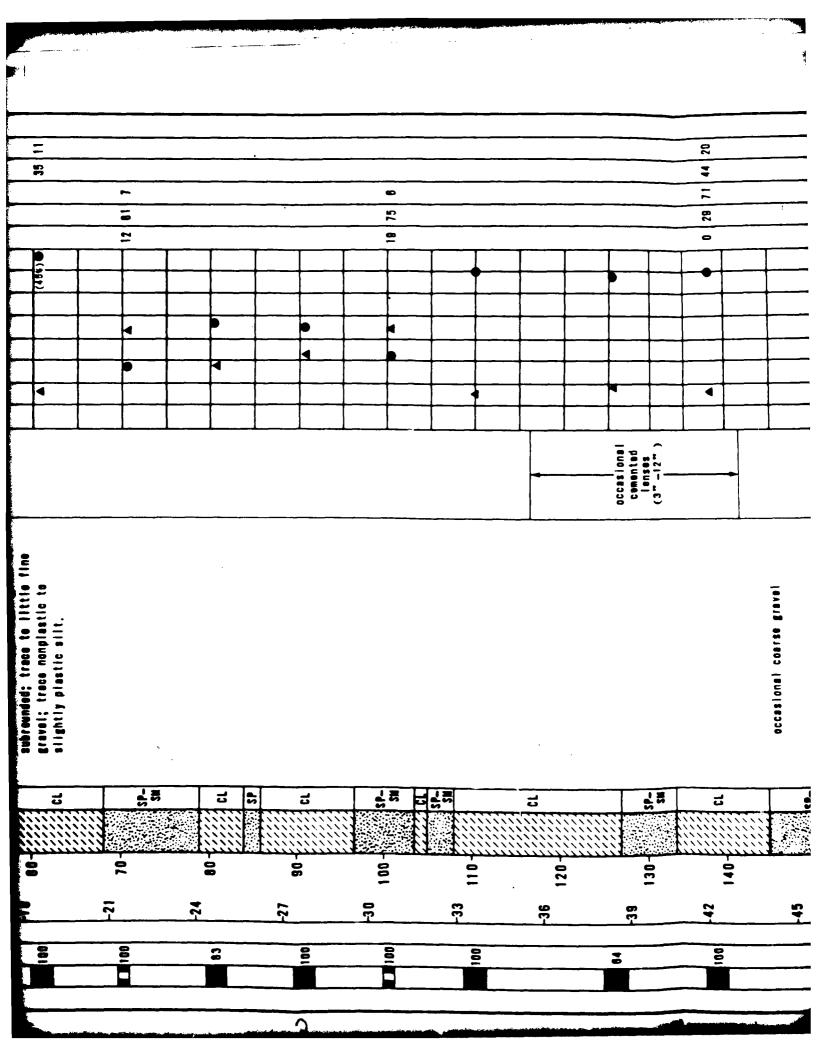
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IL DESCRIPTION		brown, fine to coarse, id, very dense, calcareous;	Z 51 .	IU. Drown, Time to coerse, Id. very dense, cai- e fine to coerse gravel;	RAVEL, brown, fine to coarse, graded, very dense, subangular	to subfounded, calcareous; some fine to cearse sand; trace to little slightly plastic silt and clay.							53.5° (16.3m)
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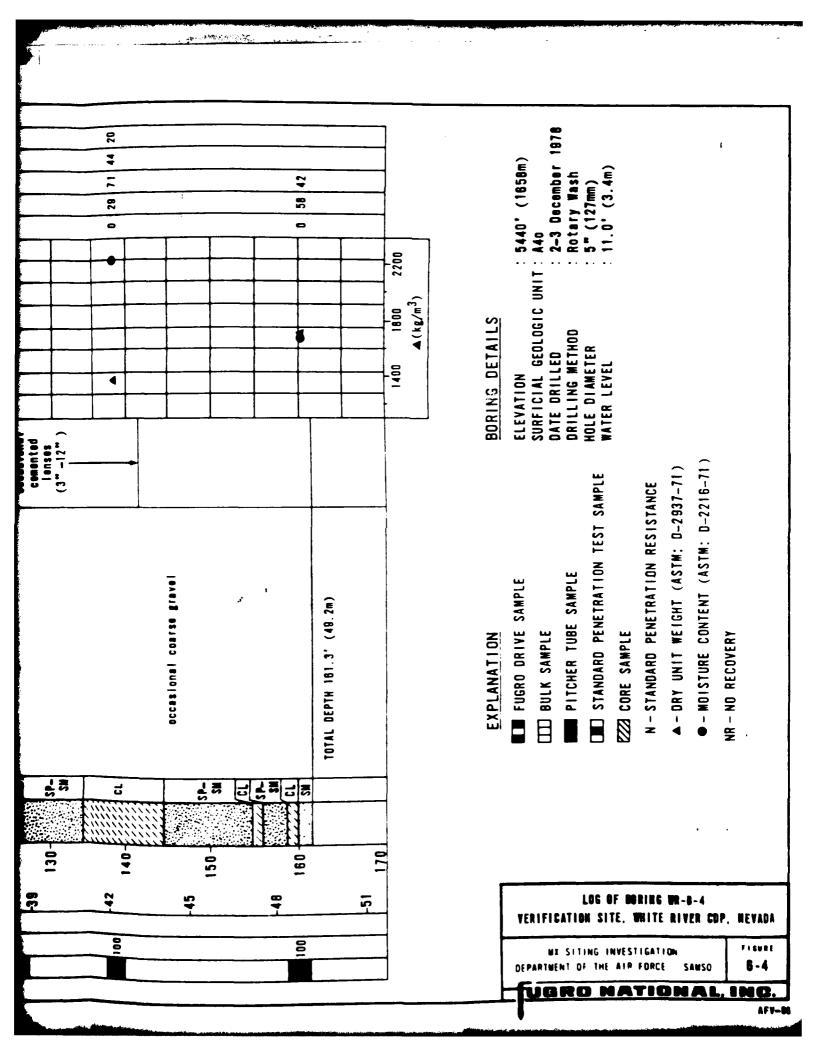




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	SOIL DESCRIPTION		CLATEY SAND, brown, fine to coarse, poor! graded, dense, subangular to subrounded,	calcareous; some highly plastic clay.	SANDY SILT, gray, stiff, medium plastic, calcareous; little silt.	SILTY SAND and SAND, brown	coarse, poorly graded, medium dense to dense, subrounded to subengular; trace to some silt.						SiLTY CLAY, brown, stiff to hard slightly to medium plastic, cal- careous; trace fine sand.	SAND: GRAVELLY SAND, STOWN to derk	_ >
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SECTION 7.0
TRENCH AND TEST PIT LOGS

EXPLANATIONS OF TRENCH AND TEST PIT LOGS

See Section 6.0, "Boring Logs", for explanations.

SURFACE ELEVATION : 5240° (1597m)
DATE EXCAVATED : 28 NOVEMBER 1976

SURFICIAL GEOLOGIC UNIT: ASy (A40)

TRENCH LENGTH :15.0° (4.8m)

TRENCH ORIENTATION : E-W

LOG OF TRENCH WR-T-1

VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-1

VERO NATIONAL, INC.

SILTY SAMD, brown, fine to coarsa, poorly graded, moist, subangular to angular, calcareous; little fine to coarse gravel. SAMDY GRAVEL, light brown, fine to coarse, poorly graded, slightly moist, angular to subangular, calcareous; some fine to coarse sand; occasional cabbles to 10" size; stage III caliche (1.5'-3.0').	(\$	REMA	EMARKS	AN		1515	L	
SANDY SRAVEL, light brown, fine to coarse, poorly graded, slightly moist, angular to subangular, calcareous; some fine to coarse and; socasional cobbles to 10" size; stage III caliche (1.5'-3.0'). TOTAL DEPTH 7.0' (2.1m) TOTAL DEPTH 7.0' (2.1m) TOTAL DEPTH 7.0' (2.1m) commentation at 7.0' exceeded capacity of Case 550C backhoe						F	T	L PI
moist, angular to subangular, calcareus; some fine to casrae sand; occasional cobbles to 10" size; stage III caliche (1.5"-3.0"). TOTAL DEPTH 7.0" (2.1m) TOTAL DEPTH 7.0" (2.1m) TOTAL DEPTH 7.0" (2.1m) 12- 14-								
TOTAL DEPTH 7.0° (2.1m) cementation at 7.0° exceeded capacity of Case 580C backhoe						2		
12-	eeded y of BOC	7.0° e: capac Case	excaaded pacity of ase 580C			2		
14-	, a	940	GACK II GA		 			
18-								
-5								
18-								
-8 20-								

SURFACE ELEVATION : 5645' (1721m)

DATE EXCAVATED : 29 NOVEMBER 1978

SURFICIAL GEOLOGIC UNIT: AST

TRENCH LENGTH

:12.0° (3.7m)

TRENCH ORIENTATION : NE-SW

LOG OF TRENCH WR-T-2 VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-2

UGRO NATIONAL, INC.

SURFACE ELEVATION : 5245' (1599m)
DATE EXCAVATED : 30 NOVEMBER 1978

SURFICIAL GEOLOGIC UNIT: A44

TRENCH LENGTH : 15.0" (4.6m)

TRENCH ORIENTATION : E-W

LOG OF TRENCH WR-T-3

VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

FIGURE 7-3

<u>ugro national in</u>

BULK SAMPL	METERS F	FEET MY	LI THOLOGY	nscs	CONSI STENCY	SOIL DESCRIPTION	REMARKS	AN		\$1\$		12.
	0	2 -		ML	soft	SAMBY SILT, light brown, slightly meist, nonplastic, calcareous; sees fine to coarse peerly graded sand; trace fine to coarse gravel.		+-	1	F1	Г	
	- 2	4		6 P	med i um dense	SAMOY GRAVEL, light brown, fine to coarse, peerly graded, dry, sub- angular te angular, calcareous; some fine to coarse sand,	vertical walls					
	-	8 -				SILTY SAND, light brown, fine to cearse, poorly graded, dry, sub- angular, calcareous.	stable					
	- 3	10-		SM	medium densa							
	-4	12-										
		14-		<u> </u>		TOTAL DEPTH 14.0' (4.3m)						
	- 5	16-		' :		-						
		18~										
	- 6	20~										

SURFACE ELEVATION

: 5320° (1622m)

DATE EXCAVATED

: 1 DECEMBER 1978

SURFICIAL GEOLOGIC UNIT: A4e

TRENCH LENGTH

:14.0" (4.3m)

TRENCH ORIENTATION

E-#

LOG OF TRENCH WR-T-4
VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

FIGURE 7-4

UBRO NATIONAL INC.

BULK SAMPLE	METERS A	PTH LEEL	L! TH0L0GY	nscs	CONSISTENCY	SOIL DESCRIPTION	REM	ARKS		IEV	E S I S	
106 	C	0			medium dense	SANDY GRAVEL, brown, fine, poorly graded, dry, angular to subangular, calcareous; some silt and fine to coarse sand; stage IIT to stage IV caliche (2.0°-5.0°)					F1	N
	- 1	2 -		GM	dense	caliche (2.0°-5.0°),		i tical stable				
		·			very dense							
!	- 2	6 -				TOTAL DEPTH 5.0° (1.5m)	5.0° e capac Case	stion at acceded ity of 580C khos				
		8 -						,				
	- 3	10-										
		12-										
	-4	14-										
	- 5	16										
	1	18-			į			,				
	- 6	20-										
								!				

SURFACE ELEVATION

:5870° (1728m) : 2 DECEMBER 1978 DATE EXCAVATED

SURFICIAL GEOLOGIC UNIT: ASI

:9.0° (2.7m) TRENCH LENGTH

TRENCH ORIENTATION

: NE-SW

LOG OF TRENCH WR-T-5

VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO FIEURE 7 - 5

UBRO NATIONAL, INC.

BULK SAMPLE	HETERS A	HTH (334	LITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS	AN		SIS		
2	0	0	3	SP	10010	SAND, brown, fine to medium, poerly graded, meist, calcareous.	-	GR	SA	FI	LL	PI
	-1	2 -		СИ	very	CLAY, gray, slightly meist, medium plastic, calcareous; little fine to coarse peerly graded sand; trace fine gravel; stage II caliche (1.5°-3.0°).	vartical	2	13	85	50	24
	- 2	8 -				SANDY CLAY, light brown, dry, slightly plastic, calcareous; little fine to coarse sand.	walls stable					
	- 3	10-		CL	stiff							
	-4	14-				TOTAL DEPTH 14.0° (4.3m)						
	 - 5	16-			i							
		16-			1							
	- 6	20-										

SURFACE ELEVATION

:5374' (1638m)

DATE EXCAVATED

: 3 DECEMBER 1978

SURFICIAL GEOLOGIC UNIT: A5y/A4e

TRENCH LENGTH

:14.0' (4.3m)

TRENCH ORIENTATION

: E-#

LOG OF TRENCH WR-T-6 VERIFICATION SITE, WHITE RIVER COP, NEVADA

UBRO NATIONAL, INC.

MX SITING INVESTIGATION

FIGURE

DEPARTMENT OF THE AIR FORCE - SAMSO

BULK SAMPLE	METERS 30	PTH	LITHOLOGY	USCS	CONSISTENCY	SOIL DESCRIPTION	REMARKS	IEV	- 1	
	0	0	=	SM	icese	SILTY SAND, brown, fine to coarse, poorly graded, moist, calcareous; some nonplastic silt; little fine gravel.	†	_	F1	P1 NP
	1	2 4			med i um	SANDY GRAVEL. light brown, fine to coarse, poerly graded, dry, sub-angular to angular, calcareous; some fine to coarse sand; stage II caliche (1.5'-5.0').	vertical walls stable			
	- 2	6 8		6P	dense	_				
	-3	10-	10000			TOTAL DEPTH 10.0' (3.0m)	cementation at 10.0' exceeded capacity of Case 5800			
	-4	12-			:		backhoe			
	- 5	16~								
	- 6	18-								

TRENCH DETAILS

SURFACE ELEVATION

:5636" (1718m) :4 DECEMBER 1978

DATE EXCAVATED

SURFICIAL GEOLOGIC UNIT: A59 TRENCH LENGTH

:14.0" (4.3m)

TRENCH ORIENTATION

: E-W

LOG OF TRENCH WR-T-7

VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO FIGURE 7-7

UGRO NATIONAL, INC.

BULK SAMPLE	BETERS 30	PTH	L! THOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS	AN		\$15		
콜	<u>=</u>	<u> </u>	5					GR	SA	FI	ı	PI
П	"	U		SP	leese	SAND, brown, fine to medium, poorly graded, moist, calcareous.		,	57	42	67	35
Ш		2 -		sc	medium dense	CLAYEY SAND, light brown, fine to coarse, poorly graded, slightly moist, calcareous; some highly plastic clay.						
	- 1	4 -				CLAY, brewn, slightly meist, highly plastic.	vertical					
	- 2	8 -		CH	very stiff		walls stable					
	-3	10-			hard							
	-4	12-		ML ·	soft	SANDY SILT, dark brown, wet, slightly plastic; some fine sand.	water level 11.0"					
		14-	7.7.7.			TOTAL DEPTH 14.0° (4.3m)	V					
	-5	16-										
		18-										
	- 6	20-										

TRENCH DETAILS

SURFACE ELEVATION

: 5440° (1658m)

DATE EXCAVATED

:5 DECEMBER 1978

: E-W

SURFICIAL GEOLOGIC UNIT: A40

TRENCH LENGTH :14.0° (4.3m)

TRENCH ORIENTATION

LOG OF TRENCH WR-T-8
ERIFICATION SITE WHITE RIVER COP NEVADA

VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

7-8

UGRO NATIONAL, INC.

SURFACE ELEVATION: 5397 (1 SURFICIAL GEOLOGIC UNIT: ASY

LOG OF TEST PIT WR-P-1

	CL CL	soft	SAMBY CLAY, brown, meist, medium plastic, calcareaus; little fine to cearse peerly graded sand; trace fine gravel.			
2	gr	medium dense	SANDY GRAVEL, light brown, fine to coarse, poorly graded, slightly meist, rounded to subangular, calcarecus; little fine to coarse sand; stage II caliche (1.0°-5.0°).			
1 5			TOTAL DEPTH 5.0' (1.5m)			

SURFACE ELEVATION: 5485 (1672m) SURFICIAL GEOLOGIC UNIT: A5y

LOG OF TEST PIT WR-P-2

LOGS OF TEST PITS WR-P-1 AND WR-P-2 VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO FIGURE 7-9

<u>ugro national, inc.</u>

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UGRO NATIONAL, INC.

BULK SAMPLE	WE TERS S	FEET #	LITHOLOGY	SOSO	C ON SISTENCY	SOIL DESCRIPTION	REMARKS		IE1	_	s		
<u>ā</u>			5		8 5			GR	SA	F	ıŢι	L P	PI
	0	0			loose	SILTY SAND, brown and gray, fine to coarse, peorly graded, moist, sub- angular, calcareous; trace fine gravel.							
	_	2 -		SM									
	- 1	3 -			medium danse								
		4 -											
		•				TOTAL DEPTH 5.0' (1.5m)		٦.			1	-	
RF	ACE I	TEV	ATION . 5430 .	/10						_	_		
IRF	ICIA	GE	OLOGIC UNIT:	ASV	55m)	LOG OF TEST PIT WR-P-5							
JRF	ICIA	L GE	ATION: 5430' Ologic Unit:	A5y	55m)	LOG OF TEST PIT WR-P-5							
JRF	CIA	L GE	OLOGIC UNIT:	A5y	55m)	LOG OF TEST PIT WR-P-5 SILTY SAND, brown, fine to coarse, peerly graded. meist, subangular, calcareeus; occasional cobbles to 5° size.		1	80	11	9		_
RF			OLOGIC UNIT:	A5y	55m)	SILTY SAND, brown, fine to coarse, peerly graded. meist, subangular, calcareeus; occasional cobbles to		1	80	119	9		
RF		1		ASy	loose -	SILTY SAND, brown, fine to coarse, peerly graded. meist, subangular, calcareeus; occasional cobbles to		1	80	119	9		
JRF	0	2 - 3 -				SILTY SAND, brown, fine to coarse, peerly graded. meist, subangular, calcareeus; occasional cobbles to		1	80		9		
		0 1 2 3 5		SM	10088 -	SILTY SAND, brown, fine to coarse, peerly graded. meist, subangular, calcareeus; occasional cobbles to		1	80	1 1 5	9		
		0 1 2 3 5		SM	10088 -	SILTY SAND, brown, fine to coarse, peorly graded. meist, subangular, calcareeus; occasional cobbles to 5 % size.		1	80	15	9		_
		0 1 2 3 5		SM	10088 -	SILTY SAND, brown, fine to coarse, peorly graded, meist, subangular, calcareeus; occasional cobbles to 5" size. TOTAL DEPTH 5.0" (1.5m) LOG OF TEST PIT WR-P-6	EST PITS WR-P SITE, WHITE F	-5 AI	NO	WR			

UGRO NATIONAL, INC.

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<u>ugro national, inc.</u>

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UBRO NATIONAL, INC.

<u>•</u> 1	DEPT	ſ	LITHOLOGY	USCS	ONS! STENCY	SOIL DESCRIPTION	REMARKS	1	IEV ALY:	_		
Ĭ	1311	FEET	LI 14	3	15 E		ì	GR	SA	FI		P
	0	0		SM	leese	SILTY SAND, light brown, fine to cearse, poorly graded, slightly melst, angular, calcareous; some nemplastic silt; trace fine gravel.			62			N
**		2 -				SANDY CLAY, light brown, slightly meist, medium plastic, calcareous; some fine to medium poorly graded sand; stage II caliche (1.5'-2.5').						
-	· 1	3 -		CL	stiff							
-	•	5 -				TOTAL DEPTH 5.0° (1.5m)		┨				
URFAC	CE EL	EV/	ATION: 5300'	(16	(5m)			<u> </u>	Щ.	_	_	_
URFAC URF 10	CE EL	EVA	ATION: 5300' Ologic unit:	(18 A1	(5m)	LOG OF TEST PIT WR-P-13		1		·		_
URFIC	O I	EVA GET	ATION: 5300' OLOGIC UNIT:	(18 A1	I sesse			7	81	32		
URFIC	G I	GE 1	ATION: 5300' OLOGIC UNIT:	A1		LOG OF TEST PIT WR-P-13 SILTY SAND, light brown, fine to coerse, poerly graded, maist, angular, calcareous; trace fine gravel; stage III caliche (2.0"-		7	81	32		
I I	G 1	2 -	ATION: 5300' OLOGIC UNIT:	A1	lossa	LOG OF TEST PIT WR-P-13 SILTY SAND, light brown, fine to coerse, poerly graded, maist, angular, calcareous; trace fine gravel; stage III caliche (2.0"-	cementation at 3.5° exceeded capacity of Case 580C backhoe	7	61	32		
URFIC	CIAL	2 -	OLOGIC UNIT:	SM	leese	LOG OF TEST PIT WR-P-13 SILTY SAND, fight brown, fine to coarse, poorly graded, maist, angular, calcareous; trace fine gravel; stage III coliche (2.0'-3.5'). TOTAL DEPTH 3.5' (1.1m)	3.5' exceeded capacity of Case 5800	7	81	32		
URFIC	CIAL	2 -	ATION: 5300' OLOGIC UNIT:	SM	leese	LOG OF TEST PIT WR-P-13 SILTY SAND, light brown, fine to coarse, poorly graded, maist, angular, calcareous; trace fine gravel; stage III coliche (2.0"-3.5"). TOTAL DEPTH 3.5" (1.1m) LOG OF TEST PIT WR-P-14	3.5' exceeded capacity of Case 5800	3 AI	10 1	WR-	P-1	

2 JUL 78.

AFV-03

FIGURE

7-16

MX SITING INVESTIGATION

DEPARTMENT OF, THE AIR FORCE - SAMSO

BULK SAMPLE	HETERS 30	FEET #	LITHOLOGY	SOSA	C DNS! S TE MCY	SOIL DESCRIPTION	REMARKS		IEV ALY:			
3			=		8			GR	SA	FI	LL	PI
	0	0		WŁ	firm	SAMDY SILT, brown, moist, nemplastic, calcareous; some fine to coarse sand; little fine gravel.		18	24	58	23	2
	-	2 -				SANDY GRAVEL, light brown, fine to coarse, poorly graded, slightly meist, angular to subangular, calcareous; little fine to coerse sand; stage I caliche (1.0'-2.0').						
	- 1	3		GP	medium dense							
-	-	5										
	CE	FIEV	ATION: 5485°	(16	70->	TOTAL DEPTH 5.0° (1.5m)		<u> </u>			L.	L
URFI	I C I A I	L GE	OLOGIC UNIT:	ASy		LOG OF TEST PIT WR-P-17		.,	,	,	,	,
URF	O O	0 1 -	OLOGIC UNIT:	A5y SM	loese	GRAVELLY SAND, brown, fine to coarse, poerly graded, meist, angular, calcareeus; some fine gravel; accasional cebbles to 5° size; stage IV caliche (1.25°-1.50°).						
URFI	I C I A I	L GE	OLOGIĆ UNIT:	A5y		GRAVELLY SAND, brown, fine to coarse, poerly graded, moist, angular, calcareous; some fine gravel; occasional cobbles to 5° size; stage IV caliche	cementation at 1.5° exceeded capacity of Case 580C backhoe					
URFI	I C I A I	0 1 -	OLOĞİĞ UNIT:	A5y		GRAVELLY SAMD, brown, fine to coarse, poerly graded, moist, angular, calcareous; some fine gravel; occasional cobbles to 5° size; stage IV caliche (1.25°-1.50°).	at 1.5° exceeded capacity of Case 580C					
URFI	O .	0 1 -	OLOĞIC UNIT:	A5y		GRAVELLY SAMD, brown, fine to coarse, poerly graded, moist, angular, calcareous; some fine gravel; occasional cobbles to 5° size; stage IV caliche (1.25°-1.50°).	at 1.5° exceeded capacity of Case 580C					
URFI	- 1	1 = 2 = 3 = 5 = 5	OLOGIC UNIT:	A5y	loose	GRAVELLY SAMD, brown, fine to coarse, poerly graded, moist, angular, calcareous; some fine gravel; occasional cobbles to 5° size; stage IV caliche (1.25°-1.50°).	at 1.5° exceeded capacity of Case 580C					
URFA	O	1 - 2 - 3 - 5 - ELEVY	OLOGIC UNIT:	A5y	loose	GRAVELLY SAMD, brown, fine to coarse, poerly graded, moist, angular, calcareous; some fine gravel; occasional cobbles to 5° size; stage IV caliche (1.25°-1.50°).	at 1.5° exceeded capacity of Case 580C					
URFA	O	1 - 2 - 3 - 5 - ELEVY	OLOGIC UNIT:	A5y	loose	GRAVELLY SAND, brown, fine to coarse, poerly graded, moist, angular, calcareous; some fine gravel; occasional cobbles to 5" size; stage IV caliche (1.25"-1.50"). TOTAL DEPTH 1.5" (0.5m) LOG OF TEST PIT WR-P-18 LOGS OF TEST	at 1.5° exceeded capacity of Case 580C					-

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SECTION 8.0 SURFICIAL SAMPLE LOGS

EXPLANATIONS OF SURFICIAL SAMPLE LOGS

Finalized logs of the surficial samples are presented in this section. The explanations provided here are to serve as general guidelines to reading the logs.

- A. Designations Surficial samples are identified as follows: SE-CS-1
 - SE abbreviation for the site (e.g., SE Snake East)
 - CS abbreviation for surficial sample
 - l number of activity
- B. Ground Surface Elevation Indicated elevations on the logs are estimated from topographic maps of the study area within an accuracy of half the contour interval.
- C. Surficial Geologic Unit Indicates the surficial geologic unit in which the activity is located.
- D. Depth Indicates depth interval for which soil description is given.
- E. USCS Unified Soil Classification Symbol; see Table 6-1 of Section 6.0, "Boring Logs", for details of USCS.
- F. Soil Description Soil is described based on field visual descriptions and/or laboratory test results. See Section 6.0, "Boring Logs", for procedures of soil description.
- G. Sieve Analysis, LL and PI These are from results of laboratory tests. See Section 6.0, "Boring Logs", for explanation.

NUMBER	GROUND SURFACE ELEVATION, FEET		DE PTH. FEET	uscs	SOIL DESCRIPTION		IEV ALY:	_		
	(METERS)	UNIT	(METERS)			GR	SA	FI	LL	P
WR-CS-1	5638 (1716)	A5y	0.0-2.0 (0.0-0.6)	CL	SANDY CLAY, brown, slightly plastic, calcareous; some fine to coarse sand.					
WR-CS-3	6000 (1829)	A5y	0.0-2.0 (0.0-0.8)	SM	SILTY SANO, brown, fine to coarse, poorly graded, angular, calcareous; some slightly plastic silt, some fine to coarse gravel.	30	35	35		
WR-CS-5	5400 (1648)	A4a	0.0-2.0 (0.0-0.6)	CL	SANDY CLAY, brown, slightly plastic, calcareous; little fine to medium sand.					
WR-CS-6	5360 (1634)	A1	0.0-2.0 (0.0-0.8)	CH	CLAY, red brown, highly plastic, cal- careous; trace fine sand.					
WR-CS-7	5380 (1634)	A40	0.0-2.0 (0.0-0.6)	SM	SILTY SAND, brown, fine to medium, poorly graded, angular, calcareous; seme slightly plastic silt.	1	67	32	35	11
WR-CS-11	5356 (1833)	A40	0.0-2.0 (0.0-0.8)	CL	SILTY CLAY, brown, medium plastic, calcareous; trace fine sand.					
WR-CS-14	5560 (1695)	A5i	0.0-0.75 (0.0-0.2)	SM	SILTY SAND, brown, fine to medium, poorly graded, angular, calcareous; some silt; trace fine gravel.					
			0.75-2.0 (0.2-G.8)	€P	SANDY GRAVEL, white, fine to coarse, peorly graded, angular to subangular, calcareous; some fine to coarse sand, occasional cobbles to 6" size.					
WR-CS-15	5472 (1668)	A 1	0.0-2.0 (0.0-0.8)	ML	SANDY SILT, light-brown, nonplastic, calcareous; some fine to medium sand.	1	24	75		N
WR-CS-16	5470 (1887)	A4e	0.0 -1 .0 (0.0 -0 .3)	CL	SANDY CLAY, brown, slightly plastic, calcareous; little fine to medium sand.					
			1.0-2.0 (0.3-0.8)	ML	SAMOY SILT, white, nonplastic, cal- careous; some fine to medium sand.					
WR-CS-17	5460 (1664)	A4e	0.0-1.25 (0.0-0.4)	SM	SILTY SANO, brown, fine to medium, poorly graded, calcareous; some silt.					
			1.25-2.0 (0.4-0.6)	CL	SANDY CLAY, light brown, slightly plastic, calcareous; little fine sand.					
WR-CS-20	5480 (1870)	A40	0.0-2.0 (0.0-0.8)	CL	SILTY CLAY, brown to white, slightly plastic, calcaraous; little fine sand; stage III caliche.					
WR-CS-23	5360 (1834)	A4a	0.0-2.0 (0.0-0.8)	SM	SILTY SAND, light brown, fine to coarse, poorly graded, angular to subangular, calcareous; some silt; trace fine gravel.					

LOGS OF SURFICIAL SOIL SAMPLES
VERIFICATION SITE,
WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SANSO

F1 GURE 8 - 1 1 OF 3

UGRO NATIONAL INC.

ACTIVITY	GROUND SURFACE ELEVATION.	SURFICIAL GEOLOGIC	DE PTH,	uscs	SOIL DESCRIPTION	1 '	IE\	E S I S		
NUMBER	FEET (METERS)	UNIT	FEET (METERS)	0303	SOIL SESSITITION			FI	<u> </u>	Р
WR-CS-24	5300 (1815)	A1	0.0-2.0 (0.0-0.6)	СН	CLAY, gray, highly plastic, cal- careous.				98	60
WR-CS-26	5310 (1618)	A40	0.0-2.0 (0.0-0.6)	CL	SILTY CLAY, brown gray, medium plastic, calcareous; little fine to medium sand.					
WR-CS-27	5312 (1619)	A40	0.0-2.0 (0.0-0.6)	СН	SILTY CLAY, light brown, highly plastic, calcareous; trace fine sand.				69	4
WR-CS-28	5385 (1641)	A5y	0.0-2.0 (0.0-0.8)	SM	SILTY SAND, light brown to white, fine to coarse, poorly graded, angular, calcareous; trace silt; trace fine gravel; stage IV caliche (1.85'-2.0').					
WR-CS-32	5230 (1594)	A40	0.0-0.75 (0.0-0.2) 0.75-2.0 (0.2-0.8)	ML SP-SM	SANDY SILT, brown, slightly plastic, calcareeus; little fine sand. GRAYELLY SAND, light brown, fine to coarse, peorly graded, angular to subangular, calcareous; little fine gravel; trace silt.					
WR-CS-34	5285 (1605)	A4a	0.0-1.5 (0.0-0.5) 1.5-2.0 (0.5-0.8)	SM SP-SM	SILTY SAND, brown, fine to coarse, poorly graded, angular to sub-angular, calcareous; trace silt. GRAVELLY SAND, light brown, fine to coarse, poorly graded, angular to subengular, calcareous; some fine to coarse gravel; stage II-III caliche (1.5'-2.0').					
WR-CS-35	5210 (1588)	A40	0.0-2.0 (0.0-0.8)	sc	CLAYEY SAND, brown to white, fine to coarse, poorly graded, calcareous; some slightly plastic clay.					
WR-CS-36	5210 (1588)	A40	0.0-1.0 (0.0-0.3)	CL	SANDY CLAY, brown, slightly plastic, calcareous; some fine to medium sand.					
WR-CS-37	5360 (1833)	A4a	0.0-2.0 (0.0-0.8)	SM	SILTY SAND, brown to white, fine to medium, pearly graded, calcareous; little to some silt; stage \coprod caliche $(1.5'-2.0')$.					
WR-CS-39	5270 (1808)	A5y	0.0-2.0 (0.0-0.8)	SC	CLAYEY SAND, brown to white, fine to coarse, poorly graded, angular to subangular, calcareous; some slightly plastic clay; stage III caliche (1.5'-2.0')-					
WR-CS-40	5328- (1824)	ASy	0.0-2.0 (0.0-0.6)	SM	SILTY SAND brown to white, fine to coarse, poorly graded, angular to subangular, calcareous; some silt; trace fine gravel; stage III caliche (1.5'-2.0').	7	48	45		

LOGS OF SURFICIAL SOIL SAMPLES
VERIFICATION SITE,
WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

F1 SURE 8-1 2 OF 3

TUGRO NATIONAL, INC.

ACT IVITY	BROUND SURFACE ELEVATION,	SURFICIAL BEOLOGIC	DE PTH. FEET	uscs	SOIL DESCRIPTION	1	IEV ALY:	_		
NUMBER	FEET (METERS)	UNIT	(METERS)			GR	SA	FI	LL	PI
WR-CS-42	5440 (1658)	A5y	0.0-2.0 (0.0-0.8)	ML	SANDY SILT, brown to white, nonplastic, calcareous; some fine sand.	a	35	85		Nf
WR-CS-44	5560 (1695)	A5 i	0.0-2.0 (0.0-0.6)	CL	SANDY CLAY, brown to white, slightly plastic, calcareous; some fine to coarse sand; trace fine gravel; stage IY (1.5'-2.0').					
WR-CS-47	5540 (1889)	A5 i	0.0-1.75 (0.0-0.5)	CL	SANDY CLAY, brown, slightly plastic, calcareous; some fine to medium sand:					
			1.75-2.0 (0.5-0.8)	SP-SM	trace fine gravel. GRAYELLY SAND, white, fine to coarse, poorly graded, subangular to angular, calcareous; some fine to coarse gravel; stage [1] caliche (1.75'-2.0').					
WR- CS -4 9	5290 (1612)	A5y	0.0-2.0 (0.0-0.6)	ML	SANDY SILT, brown, slightly plastic, calcareous; little fine sand,	0	19	81	31	7
WRCS-50	5244 (1598)	A4e	0.0-2.0 (0.0-0.8)	SC	CLAYEY SAND, brown to white, fine to medium, poorly graded, calcareous; little slightly plastic clay; stage III caliche (1.75'-2.0').					
WR-CS-51	5230 (1594)	A40	0.0-1.0 (0.0-0.3)	SM	SILTY SAND, brown, fine to medium, paorly graded, calcareous; little silt.					
			1.0-2.0 (0.3-6.6)	CL	SILTY CLAY, light brown, slightly plastic, calcareous; trace fine to medium sand.					
	_									
		!								
	i									

LOGS OF SURFICIAL SOIL SAMPLES
VERIFICATION SITE,
WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

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UBRO NATIONAL INC.

SECTION 9.0

LABORATORY TEST RESULTS

EXPLANATIONS OF LABORATORY TEST RESULTS

Laboratory test results are presented in this section. Table 9-1 contains a summary of laboratory test results. This table contains results of sieve analysis; plasticity data; in-situ dry unit weight, moisture content, degree of saturation, and void ratio for drive and Pitcher samples; results of compaction tests; and specific gravity of solids. Other tests such as triaxial compression, unconfined compression, direct shear, consolidation, chemical, and California Bearing Ratio (CBR) are indicated on the table. Tables 9-2 through 9-6 and Figures 9-1 through 9-3 present results of triaxial compression, unconfined compression, direct shear, consolidation, chemical, and CBR tests.

All tests were performed in general accordance with the American Society for Testing and Materials (ASTM) procedures. The following table presents the ASTM designations for the tests performed during the investigation.

Type of Test	ASTM	Designations
Particle Size Analysis Liquid Limit Plastic Limit Unit Weight Moisture Content Compaction Specific Gravity of Solids Triaxial Unconfined Compression Direct Shear Consolidation Test for Alkalinity (pH)	000000000000000000000000000000000000000	422-63 423-66 424-59 2937-71 2216-71 1557-70 854-58 2850-70 2166-66 3080-72 2435-70 1067-70
Water Soluble Sodium	D	1428-64
Water Soluble Chloride Water Soluble Sulphate	D	512-67 516-68
Water Soluble Calcium Calcium Carbonate California Bearing Ratio (CBR)	D	511-72 1126-67 1883-73
	_	

Explanation for the tables and figures presented in this section are as follows.

- A. Activity Number Boring, trench, test pit, or surficial sample designation.
- B. Sample Number Prefix indicates the type of sample; explanation is at the bottom of the table.
- C. Sample Interval This is the depth range measured from ground surface over which the sample was obtained.
- D. Percent Finer by Weight Presents the results of laboratory particle size analysis (ASTM D 422-63) performed on representative soil samples at the depth indicated. The numbers represent the percent (by dry weight) of the total sample weight passing through each sieve size indicated.
- E. Atterberg Limits (ASTM D 423-66 and D 424-59)
 - LL Liquid Limit, the water content (as percent of soil dry weight) corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
 - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
 - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
 - NP Nonplastic.
- F. USCS Unified Soil Classification Symbols are given here; see Table 6.1 in Section 6.0, "Boring Logs", for complete details of USCS system.

- G. In Situ Presents results of tests on drive and Pitcher samples.
 - Dry Unit Weight indicates dry unit weight of soil determined as per ASTM D 2937-71
 - Moisture Content weight of water reported in percent of dry weight of soil sample (ASTM D 2216-71)
 - Saturation the degree of saturation in a soil sample is defined as the ratio (in percent) of the volume of water to the volume of all voids in the soil
 - Void Ratio the numerical ratio of the volume of voids to the volume of solids in a soil specimen
- H. Compacted Indicates results of laboratory maximum dry density and optimum moisture content test as per ASTM D 1557-70.
- I. Specific Gravity of Solids (ASTM D 854-58) Indicates the ratio of (1) the weight in air of a given volume of soil solids at a stated temperature, to (2) the weight in air of an equal volume of distilled water at a stated temperature.
- J. Triaxial The triaxial compression tests were performed in accordance with the procedures of ASTM D 2850-70. The following explanations and definitions apply.

Triaxial Compression Test - a cylindrical specimen of soil is surrounded by a fluid in a pressure chamber and subjected to an isotropic pressure. An additional compressive load is then applied, directed along the axis of the specimen called the axial load.

Consolidated-Drained (CD) Test - a triaxial compression test in which the soil was first consolidated under an all-around confining stress (test chamber pressure), and was then compressed (and hence sheared) by increasing the

vertical stress. Drained indicates that excess pore water pressure generated by strains are permitted to dissipate by the free movement of pore water during consolidation and compression.

Consolidated-Undrained (CU) Test - a triaxial compression test in which essentially complete consolidation under the confining (chamber) pressure is followed by a shear test at constant water content.

Confining Pressure (σ_3) - the isotropic chamber pressure applied to the soil specimen during consolidation and compression.

Maximum Deviator Stress $(\sigma_1 - \sigma_3)$ - the difference between the major and minor principal stresses in the specimen at failure. The major principal stress on the specimen is equal to the unit axial load plus the chamber pressure and the minor principal stress on the specimen is equal to the chamber pressure.

Strain Rate – axial strain, ϵ , at a given stress level is defined as the ratio of the change in length ($^{\Delta}$ L) of the specimen to the original length of the specimen (L O). The rate of strain was controlled during the test so that this ratio increased at equal increments for each minute of testing.

Back Pressure - pressure in excess of atmospheric applied to the pore water of a soil sample. Back pressure is usually applied to (1) increase saturation of the sample, or (2) simulate the actual in-situ pressure regime.

K. Unconfined Compression - Test procedures were as described in ASTM D 2166-66. Unconfined compressive strength is defined as the load per unit area at which an unconfined prismatic or cylindrical specimen of soil will fail in a simple compression test. In these methods, unconfined compressive strength is taken as the maximum load attained per unit area or the load per unit area at 20 percent axial strain, whichever occurred first during the performance of a test.

- L. Direct Shear The procedures of ASTM D 3080-72 were followed for direct shear testing. In this test, soil under an applied normal load is stressed to failure by moving one section of the soil container (shear box) relative to the other section. Normal stress is the value of load per unit area acting perpendicular to the plane of shearing. Maximum shear strength is defined as the maximum resistance (ksf) of a soil to shearing (tangential) stresses.
- M. Consolidation (ASTM D 2435-70) A consolidation test is a test in which a cylindrical soil specimen is laterally confined in a ring and compressed between porous plates. The term "consolidation", as used here, indicates the gradual reduction in volume of the soil mass resulting from an increase in compressive stress (axial load per unit area).
- N. Chemical The chemical tests performed on soil samples included: pH; water soluble sodium, chloride, sulphate, calcium; and calcium carbonate content. pH is an index of the acidity or alkalinity of a soil in terms of the logarithm of the reciprocal of the hydrogen ion concentration.

 ASTM test procedure designations for these chemical tests are included in the table at the beginning of the "Explanation of Laboratory Test Results".
- O. CBR California Bearing Ratio (CBR) is the ratio (in percent) of the resistance to penetration developed by a subgrade soil to that developed by a standard crushed-rock

base material. The procedures for conducting a CBR test were as outlined in ASTM D 1883-73. The materials tested for CBR were also analyzed for particle size distribution (ASTM D 422-63) and compaction characteristics (ASTM D 1557-70). The term "percentage of maximum density" indicates the ratio (as a percentage) of the compacted sample dry unit weight to maximum dry density obtained in the laboratory from ASTM D 1557-70, "Moisture-Density Relations of Soils Using 10-pound (4.5 kg) Hammer and 18-inch (457 mm) Drop".

	(3)								PERCE	NT FINE	R BY W	EIGHT
11.		SAMPLE INTER	NTERVAL		\$	TANDARI	SIEV	E OPEN	ING		U S	STAN
ACT I V I TY Number	SAMPLE Number	1 0.8-1.6 0.24 2 4.9-5.7 1.49		BLDRS	COSE	ILES		GRA	VEL			SA
A SE	1 P-1 0.8-1.6 0.24-0.49 P-2 4.9-5.7 1.49-1.74	3/8"	4	10								
WR-B-1	P-1	0.8-1.6	0.24-0.49								100	96
	P-2	4.9-5.7	1.49-1.74				<u> </u>				100	95
	D-3	7.5-8.2	2.29-2.50			1	i	·				
	P-4	10.0-10.9	3.05-3.32				1	ì				
	P-4	10.9-11.8	3.32-3.60									
	P-5	15.9-16.5	4.85-5.88					I		I		
	P-5	16.5-17.2	5.03-5.24									
	P-5	17.2-17.9	5.24-5.46									
	P-6	20.0-20.8	6.10-6.34									
	P-7	25.0-25.9	7.62-7.89								100	97
	P-8	30.7-31.4	9.36-9.57									
	P-9	40.9-41.8	12.47-12.74									
ļi	P-10	50.0-50.4	15.24-15.36							100	99	95
	P-10	50.4-51.2	15.36-15.61									
	P-11	60.0-60.9	18.29-18.56									
	P-12	70.8-71.6	21.58-21.82									
ļ	P-13	80.8-81.3	24.63-24.78									
	P-14	98.0-98.8	29.87-30.11	[
ļ	P-15	121.4-122.1	37.00-37.22									
	P-16	140.5-141.4	42.82-43.10	1				L		.	L	
ļ	P-17	160.8-161.6	49.01-49.26	-				 		ļ		8
WR-B-2	D-1	0.2-0.9	0.06-0.27	\vdash				100	83	80	68	58
	D-2	3.5-4.0	1.07-1.22					100	90	68	54	44
	D-4	7.3-7.9	2.19-2.41				†					- ' '
	D-5	10.8-11.4	3.29-3.47							†		
	D-6	15.2-15.9	4.63-4.85				1		100	86	59	41
	D-8	25.0-25.4	7.62-7.74									
	D-9	30.0-30.6	9.14-9.33					100	66	49	43	37
	D-10	40.0-40.3	12.19-12.28						-	}- <u></u> -	1-3-	·
	D-11	50.0-51.0	15.24-15.54					100	87	70	60	51
	D-13	79.0-79.3	24.08-24.17				100	57	49	40	34	28
	D-14	100.0-100.5	30.48-30.63									
	D-15	114.2-114.9	34.81-35.02						100	93	84	69
	D-16	135.0-135.4	41.15-41.27					100	80	64	48	40
	D-17	160.0-160.3	48.77-48.86					100	88	68	51	37
]								
WR-B-3	P-1	0.8-1.6	0.24-0.49								100	97
	D-2	4.2-4.9	1.28-1.49							100	99	96
	D-3	7.3-7.9	2.23-2.41									
	P-4	10.0-10.8	3.05-3.29									
	P-4	10.8-11.3	3.29-3.44								100	99
	P-5	15.0-15.9	4.57-4.85			L						

NOTES:

(a) Sample types

- (c) USCS Unified Soil Classification System
- SS Standard split spoon
- P Pitcher
- D Fugro Drive
- (d) * Indicates that test has been performed and results are included in this report

- 8, b Bulk
- (b) NP Not Plastic

1 87 1	THOLS											11	4-S I TU				OMPACTE	D	<u> </u>
V S	STAN SA		IEVE N		PART SIZE LT OR C	(RM)		TERBE IITS ((c)	DRY L		MOISTURE Content (\$)	SATURATION (\$)	VOID RATIO	MAX Dry Di	MUM NSITY	OPTIBUR Hoisture (\$)	SPECIFIC GRAVITY
4	10	40	100	200	.005	. 001	LL	PL	PI		(pcf)	(kg/m ³)		TS.	22	(pcf)	(kg m3)	18 B	5 31
100	96	2	45	34						SM	92.6	1483	10.7	35.2	0.82		-	 	
100	95	51	16	11	1	<u> </u>				SP-SM	99.7	1597	5.3				†	 	ł
										SM	96.6	1548	13.0		0.74		1		
										CL	92.2	1477	21.0		0.83		<u> </u>	†·	†
							43	22	21	CL	83.2	1333	21.7	57.1			1	†	
										ML	85.9	1376	24.4	68.6	0.96				
							45	2₽	17	ML	93.8	1503	17.1	58.0	0.80		1		2.63
										ML	92.2	1477	29.3	95.7	0.83		1	1	1
							64	34	30	MH	77.4	1240	33.6	77.2	1.18		<u> </u>	1	
100	97	87	74	69						MH	74.6	1195	42.6	91.4	26		Ī		<u> </u>
										МН	80.6	1291	38.2	94.6	1.09		<u> </u>	1	
										МН	76.1	1219	37.0	82.2	1.22				
99	95	74	57	52		L	59	40	19	MH							I		
										MH	76.8	1230	39.9	90.1	1.19		Ī		
										MH	89.9	1440	30.1	92.8	0.87		<u> </u>		
						I				ML	93.2	1493	23.7		0.81		1	†	
					Ī					ML	92.7	1485	26.1		0.82				
							45	30	15	ML	79.2	1269	43.8	100.0	1.13)	1	
										ML	85.1	1363	33.7	92.7	1.00		<u> </u>		
										ŞP	93.4	1496	19.8	66.6	0.81			1	
	00	99	98	91	I					ML	97.9	1568	23.7	88.7	0.72				
					Ī								1					1 1	
68	58	48	40	33						SM	90.8	1455	12.9	40.7	0.86			1	_
54	44	33	24	18		1				GM	101.1	1620	5.9	24.2			! —-	†	
										GM	121.4	1945	2.9	20.8				*** * * 1	
										GM	115.2	1846	5.2	30.4			†	1	
59	41	26	17	12	<u> </u>					SP-SM	115.4	1849	12.1		0.46			!	
										SP-SM	116.2	1862	14.9		0.45				
43	37	27	ľ	15	<u> </u>	<u> </u>				GM	112.6	1804	17.2	93.4					·
	-		•		<u> </u>	<u> </u>				GM	1.2	2134	10.8	100.0					
60	51	43	38	33	†					GM	7.6	1884	15.5	96.7				†	
34	28	15	<u> </u>	13	1	<u> </u>				GM	\$5.9	2177	9.0	100.0			<u> </u>	<u> </u>	
										GM	128.0	2051	9.9	85.2					
84	69	42	30	26	1					SM	129.3		7.6	67.2					
48	40	32	27	25	1					GM	126.4			68.6				† 1	
51	37	24	19	16						6M	133.9		8.9		0.26		<u> </u>	1	
	<u> </u>	-			 	 						T	† - · ·	- 	 ****		 	1	
100	97		44	30	†	}				SM	74.0	1185	21.7	46.0	1.28	 	 	╅	}
99	96	93	89	86	†	<u> </u>				СН		1349		41 2	1.00		 	†	
	<u> </u>			 -	t		54	29	25	СН		1367					 	 	
	├ ──┤			}	 		<u> </u>	=		СН	88.0	1410	16.9	49.9			 	 	
100	99	97	82	60			39		16	CL		1	1 = 0.3	77.7	7. 31			╂──┤	
			-		}		37	23	14	CL	91,2	1461	27.8	100 6	0.85			1	

0

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DE PI

			1)	I-SITU			C	OMPACTE			Î	_=		=		
ERG (b)	uscs	DRY WEIG		MOISTURE CONTENT (\$)	SATURATION (\$)	. 0	MAX! DRY DE		OPTIMUS Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT Shear	CONSOLIBATION	CHEDICAL	
PI	(c)		(kg/m ³)	MOIST CONTE (\$)	SATU CS	YOID RATIO	(pcf)	(kg m ³)	140 101 101	SPE GRA OF	TRI		SHE			8 93
+	SM	92.6	1483	10.7		0.82	(901)	("" "")			<u> </u>	-		3		┡┷┩
+	SP-SM	99.7	1597	5.3		0.69						ļ				
+	SM	96.6	1548	13.0	47.2		} 	}					 			
+	CL	92.2	1477	21.0	68.9	0.83										
21	CL	83.2	1333	21.7	57.1	1.03						ļ				
+	MIL	85.9	1376	24.4	68.6											
17	ML	93.8	1503	17.1	58.0	0.80	·			2.63		t				
1	ML	92.2	1477	29.3	95.7	0.83				2.03	*	 	-			
30	MH	77.4	1240	33.6		1.18						†	h	*		
1	MH	74.6	1195	42.6	91.4	26						1	 		*	
1	MH	80.6	1291	38.2		1.09					·	†	1			
1	MH	76.1	1219	37.0	82.2	1.22						1				
19	MH											1				
	MH	76.8	1230	39.9	90.1	1.19										
1	MH	89.9	1440	30.1	92.8	0.87									*	
	ML	93.2	1493	23.7	79.0							1				
	ML	92.7	1485	26.1	86.2	0.82						1				
15	ML	79.2	1269	43.8	100.0	1.13						1				
	ML	85.1	1363	33.7	92.7	1.00									*	
	ŞP	93.4	1496	19.8	66.6	0.81						1				
	ML	97.9	1568	23.7	88.7	0.72									*	
\mathbf{L}_{-}																
	SM	90.8	1455	12.9	40.7	0.86										
	GM	101.1	1620	5.9	24.2											
	GM	121.4	1945	2.9	20.8											
	GM	115.2	1846	5.2		0.46										
	SP-SM	115.4	1849	12.1	71.1											
	SP-SM	116.2	1862	14.9	89.7	0.45										
	GM	112.6	1804	17.2	93.4	0.50		L					*			
	GM	<u> </u>	2134	10.8	100.0	0.27										
	GM	7.6	1884	15.5	96.7	0.43										
4	GM	Ø5.9	2177	9.0	100.0	0.24										
+	GM	128.0	2051	9.9	85.2											
4	SM	129.3	2071	7.6	67.2	0.30			ļļ		 					
	GM	126.4			68.6	0.33		<u> </u>					ļ			
	6M	133.9	2145	8.9	92.3	0.26	L						L			
		<u> </u>	ļ <u>. </u>									L]
	SM	74.0	1185		46.0							 				
	СН	84.2		15.3				<u> </u>	ļ							
25	СН	85.3	1367		44.3											
	СН	88.0	1410	16.9	49.9	0.91										
16	CL		 .						L						<u>_</u>	
14	CL	91.2	1461	27.8	88.6	0.85		L	L			<u> </u>				L}

SUMMARY OF LABORATORY TEST RESULTS
VERIFICATION SITE, WHITE RIVER CDP. NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAUSD

TAOLE 9-1 1-07-5

UGRO NATIONAL INC

	(8)								PERCEI	IT FINE	R BY	EIGHT	
E _		SAMPLE I	NTERVAL		2	TANDARI	SIEV	E OPEN	ING		U S	NATS	DAR
ACT I V I TY Number	SAMPLE Number			BLDRS	COBI	ILES		GRA	VEL			SA	ND
¥ ¥	S	FEET	METERS	24"	12"	6"	3	15"	3/4"	3.8"	4	10	4
WR-B-3	P-6	20.0-20.8	6.10-6.34										
	P-7	25.0-25.4	7.62-7.74										
	P-7	25.4-26.2	7.74-7.99			I							
	P-8	30.0-30.7	9.14-9.36						1				
	P-9	40.9-41.8	12.47-12.74						100	97	96	91	7
	P-10	50.0-50.8	15.24-15.48								100	99	7
	P-11	60.0-60.9	18.29-18.56										
	P-12	70.0-70.8	21.34-21.58										
	P-13	80.8-81.6	24.63-24.87			I				100	96	88	4
	P-14	90.0-90.8	27.43-27.68						1				
	P-15	100.9-101.8	30.75-31.02		-	I							
	P-16	110.2-111.0	33.59-33.83			$\mathbf{I}^{}$							
	P-17	124.9-125.8	38.07-38.34	[]		L Ì							
	P-18	142.8-143.6	43.53-43.77			I							
	P-19	160.8-161.7	49.01-49.29										
									†	i i			
WR-B-4	P-1	0.8-1.7	0.24-0.76						1	1	100	96	72
	P-2	.4.5-5.3	1.37-1.62			ì			100	99	96	80	50
	P-3	7.9-8.6	2.41-2.62			1							
	P-4	10.0-10.8	3.05-3.29										
	P-5	15.0-15.6	4.57-4.75										
	P-5	15.6-16.2	4.75-4.94	1			1 1		1	100	97	78	2
	P-6	20.8-21.5	6.34-6.55		· · · · · · · · · · · · · · · · · · ·	1							
	D-7	25.2-25.9	7.68-7.89										
	D-8	30.2-30.9	9.20-9.42								100	98	A
	P-9	36.0-36.7	10.97-11.19								100	97	8 6
	P-10	41.4-42.3	12.62-12.89										
	D-11	50.0-50.3	15.24-15.33						100	99	85	57	12
	P-12	60.9-61.8	18.56-18.84										-
	D-13	70.2-70.9	21.40-21.61			†			100	96	88	64	24
	P-14	80.7-81.4	24.59-24.81			†			1			73	•
	P-15	90.8-91.7	27.68-27.95										
	D-16	100.2-100.9	30.54-30.75						100	95	81	54	24
	P-17	109.9-110.7	33.50-33.74			<u> </u>			1				
	P-18	125.0-125.8	38.10-38.34		·	1			†				
	P-19	137.6-138.4	41.94-42.18									100	9
	P-20	160.4-161.2	48.89-49.13								100	99	ê
									 	$\vdash \lnot$		 	-
WR-B-5	P-1	0.1-0.7	0.03-0.21						100	92	84	77	7
	D-2	3.0-3.5	0.91-1.07			†			100	99	94	83	6
	D-3	5.2-5.9	1.58-1.80			 		100	93	80	62	37	72
	D-5	10.5-1.07	3.20-3.26			 		100	89	58	43	34	1
	D-6	14.5-14.8	4.42-4.51			 		100					-4
								<u> </u>			——		-

NOTES:

(a) Sample types

- (c) USCS Unified Soil Classification System
- SS Standard split spoon
 - P Pitcher
- (d) * Indicates that test has been performed and results are included in this report
- D Fugro Orive
- B.b Bulk
- (b) NP Not Plastic

96 100			100 100 53	SIL 200	PART SIZE T OR C	(MM)		TERBE		USCS (c)	DRY U		MOISTURE CONTENT (\$)	SATURATION (\$)	0	MAXI	MUM NSITY	OPTIMUM Moisture (%)	SPECIFIC COARLER
96 100	91 99	78	53	200	T OR C	LAY	LL				WEIG	нт		 	0	004 05	WT12M	트등의	<u> </u>
96 100	91 99	78	53		.005	.001		PL	PI	```			INTE (\$)	TURA (\$)	22	טע זאט ו	M3111		3 4
100	99						82				(pcf)	(kg/m³)		SAT	YOID RATI((pcf)	(kg m ³)	8 =	S a
100	99						82			СН	77.7	1245	26.5	61.2	1.17				
100	99							35	47	СН	76.5	1226	35.1	78.7	1.20				
100	99									СН	68.2	1093	45.1	82.8			I		
100	99									CL	94.5	1514	22.1	76.1					
		86	.76	28						SM	91.3	1463	27.1	86.6	0.85				
96	88		'''	69	_					CL							<u> </u>	L	
96	88									CL	76.2	1221	43.0	96.0	1.21				
96	88									CL	81.7	1309	40.5	100.0			L		
		47	32	27						SC	108.6	1740	15.7	76.7				L]	
		1								CL	94.6	1515	27.2	94.2			L	1	
										CL	89.9	1440	31.2	96.4	0.87		L	L	
										CL	110.8	1775	15.7	81.1	0.52				
	l						38	24	14	CL	103.7	1661	21.1	91.2	0.62		L		
ll.	-1									CL	95.4	1528	26.9	94.7			L	,	
	I						59	26	33	CL	82.6	1323	39.5	100.0	1.04		L		
				L	l	l	L						ļ	ļ	L		_	ļ	L
	96	72	48	37	L			L		SC	83.1	1331	23.9	62.7					l
96	80	58	47	40	l	L	ļ			SC	94.4	1512	16.9	58.1				↓ .	ļ
					L	L	46	28	18	ML	85.6	1371	33.6	23.7		L	L	ļ	ļ
					ļ	 	L	<u></u>		SM	90.1	1443	30.3	94.1	0.87	.		ļ	ļ
1 1							1			SP-SM			l	l			1	ļ .	ļ
97	78	27	15	8		ļ	<u> </u>	 	L	SP-SM	107.4	1721	13.1	62.2		.	L	↓ .	
						L	L	ļ	ļ	SP-SM	108.4	1737	19.3	93.4					ļ
L						ļ		L		SP-SM	113.3	1815	11.4	63.1			ļ		ļ
	98	88	58	35	.	L		<u> </u>		SM	100.4	1608	23.9	95.1		ļ	L		
100	97	65	38	24	4	3	!		NP	SM	78.4	1256	36.2	84.9				ļ	
igspace				L		↓	 	<u> </u>	ļ	CL	98.1	1572	32.1	100.0			ļ	ļ	L_
85	57	12	5	4	ļ			 	ļ	SW	110.5	1770	18.2	93.6					
	1						35	24	11	CL	87.4	1400	44.7	100.0			ļ	L	
88	64	24	8	7	 		 	 -	 	SP-SM	114.2	1829	14.8	84.1			 -	 	
├			ļ		 	 	 	 	 -	CL	98.7	1581	22.6	86.2				 .	
++		-35	 -	-	 	 	 	₩-		CL CL	101.5	1626	23.0	94.1		 	 	 -	 -
81	54	26	8_	6	 	 	 	 -	 	SP-SM	114.9	1841	15.7		0.47	ł	 		
├ ──-}					 	 	 	 	 -	CL	84.7	1357	34.5	+			 	 -	├
 -			<u> </u>		 	 	1	1	 -	CL	89.3	1431	34.2	104.1	0.89		₩	 	<u>-</u>
	100	99	83	71	 	 	44	24	20	CL	86.0		35.2				 	 -	
100	99	88	67	42	 	 	}	}	↓	sc	107.1	1716	17.6	82.8	10.3/	 		 _	
+				172	↓	 -	 	 	 -		00.0	1456	1,22	40.4	0 05		 	 	 -
	77	70	62	49	 	├	 	₩-	 	SM	90.9	1436	12.8	40.4	10.83	ļ	 	 	-
	83	60	46	38	↓		}	↓	 -	SM	132 2	1 2020	+	 == =	l	}	 	 	
	37	20	14	12	 		├	 	├ ──	SP-SM	126.7			50.3			 	 	
43	34	19	14	13	├ -	 	╂		 	GC	124.8			61.3			}	}	}
			<u></u>	<u> </u>	<u> </u>	<u></u>		Ц		GC	127.8	2047	1 3.3	104.0	10.32	<u> </u>	ــــــــــــــــــــــــــــــــــــــ	 	Ц_

	<u>r</u>	 	1 2	-SITU			r	OMPACTE	<u> </u>		<u> </u>			_		
RG	ł	DAY ::			<u> </u>				ш	ြွှ	ן כנ	SEDI			_ [İ
b)	uscs	DRY U		MOISTURE Content (\$)	SATURATION (\$)		MAXI		OPTINUM Moisture (*)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED Compression	L &	CONSOLIDATION	CHEMICAL	
	(c)	WEIG		DIST ONTE (\$)	TURA (\$)	V010 RAT10	DRY DE		PT M 0 ST (%)	PEC	7 ×		DIRECT	OS	2	CBR
PI		(pcf)	(kg/m ³)				(pcf)	(kg. m ³)	0 2	SPE GR/ OF	=	3 2	ی ⊡	93	13	3
	CH	77.7	1245	26.5		1.17										
47	СН	76.5	1226	35.1	78.7							[i				
	СН	68.2	1093	45.1	82.8	1.47								*		
	CL .	94.5	1514	22.1	76.1	0.78						ļ				
	SM	91.3	1463	27.1	86.6	0.85			ļ							
	CL		1001	42 2					 .							
	CL	76.2 81.7	1221	43.0	96.0				ļ			ļ				
	CL		1309	40.5	100.0							ļ ļ				. 4
├ ─	SC	108.6 94.6	1740	15.7	76.7	0.55			┡ ┤		ļ	 			ļ	
	CL CL	89.9	1515	27.2 31.2	96.4	0.78					 	ļ		ļ		
┝╌┤	CL	110.8	1440 1775	15.7	90.4	0.87			<u> </u>		<u></u>	ļ		L		
14	CL	103.7	1661	21.1	81.1 91.2	0.52										-
┝╧┸╽	CT	95.4	1528	26.9	94.7	0.77	· · · · · · · · ·		} ~			}		-		
33	CL	82.6	1323	39.5	100.0			<u>-</u>	 			∤			<u> </u>	├ · · -
┝╌┤	CD	52.0	1323	37.5	100.0	1		L- · -	├ -	}		 -				├ ┪
┝──╂	SC	83.1	1331	23.9	62.7	1.03						-		٠ ٠	∤	
	SC	94.4	1512	16.9	58.1	0.79		·							h + 1	} -
18	ML	85.6	1371	33.6	93.7	0.97							1		· · · · · · · · · · · · · · · · · · ·	├ ┤
<u> </u>	SM	90.1	1443	30.3	94.1				t			†		1	<u> </u>	}, ⊢
	SP-SM					T			·			+	-			
	SP-SM	107.4	1721	13.1	62.2	0.57		=-		1	•	† †			1	
	SP-SM	108.4	1737	19.3	93.4	0.56			· · · · ·			† †	}			1
	SP-SM	113.3	1815	11.4	93.4 63.1	0.49						†				
	SM	100.4	1608	23.9	95.1	0.68						† †				
NP	SM	78.4	1256	36.2	84.9	1.15										
	CL	98.1	1572	32.1	100.0											1
	SW	110.5	1770	18.2		0.52						1				
11	CL	87.4	1400	44.7	100.0											
	SP-SM	114.2	1829	14.8	84.1	0.48										
I	CL	98.7	1581	22.6	86.2	0.71										
$\vdash \vdash$	CL	101.5	1626	23.0	94.1											
├	SP-SM	114.9	1841	15.7	90.6				ļ	ļ		 			L	
 	CL	84.7	1357	34.5	94.3				i		ļ	 			l	
	CL	89.3	1431	34.2	104.1	0.89	 		ļ		ļ	ll		L		
20	CL	86.0	1378						 	L		ļ				
igspace	SC	107.1	1716	17.6	82.8	0.57			ļ		<u> </u>	 				
-			1365	1,2 2	 	10.05		<u> </u>	 							
	SM	90.9	1456	12.8	40.4	0.85	ļ		ļ			├ ─				
	SM	102 =	1 222		 	10-35	ļ		ļ		ļ	├				
	SP-SM	126.7	2030		50.3			 .	 	L		1				
	GC CC	124.8			61.3			ļ				├		<u> </u>		
	GC_	127.8	2047	9.9	84.0	10.52			L		L			L		

SUMMARY OF LABORATORY TEST RESULTS
VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MR SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAMSO

740LE 9-1 1-07-3

UGRO NATIONAL, INC.

	3	<u> </u>							PERCEI	IT FINE	R BY W	EIGHT
£ ~		SAMPLE I	NTERVAL		S	TANDAR	SIEV	E OPEN	ING		U S	IDNATZ
ACT I V I TY Number	SAMPLE Number			BLORS	COBE	BLES		GRA	VEL			SAM
AC M	SA	FEET	METERS	24"	12"	6"	3"	15"	3/4"	3/8"	4	10
	D-7	19.2-19.9	5.85-6.07					100	79	59	38	27
	D-8	24.0-24.5	7.32-7.47								1	
	D-9	29.0-29.8	8.84-9.08					100	87	57	43	35
	D-10	40.0-40.3	12.19-12.28				100	49	49	44	33	22
	D-11	53.0-53.4	16.15-16.28									
						<u> </u>					l	
WR-B-6	D-1	0.7-1.4	0.21-0.43						100	86	73	62
	D-2	3.0-3.6	0.91-1.10			<u></u>			100	91	72	58
L	D-3	6.2-6.9	1.89-2.10			<u> </u>		100	82	65	53	42
	D-4	10.2-10.9	3.11-3.32			L			.			
	D-5	15.0-15.5	4.57-4.72						100	86	71	57
	D-6	20.0-20.6	6.10-6.28			ļ			100	76	49	32
	D-7	25.2-25.9	7.68-7.89	ļ		!			ļ			
	D-8	30.2-30.9	9.20-9.42			L		100	92	72	53	38
	D-9	39.9-40.4	12.16-12.31	L		L			100	99	94	88
	D-10	50.9-51.4	15.51-15.67			L			ļ			
	D-11	60.2-60.7	18.35-18.50			ļ		100	85	84	72	59
	D-12	70.9-71.4	21.61-21.76						ļ			
	D-13	85.4-85.9	26.02-26.18					L	100	92	70	55
	D-15	105.4-105.9	32.13-32.28			!						
	D-17	119.5-119.9	36.42-36.55						\			
	D-19	140.2-140.7	42.73-42.89						<u> </u>	.		
	D-21	160.8-161.3	49.01-49.16						100	97	88	81
		<u> </u>				ļ			L	ļ		
WR-B-7	D-1	0.4-1.0	0.12-0.30			1			100	96	89	78
	D-2	3.2-3.9	0.98-1.19			ļ	<u> </u>	ļ		100	94	84
	D-3	8.4-8.9	2.56-2.71	├		ļ		<u> </u>	ļ	100	96	87
ļ	D-4	14.2-14.9	4.33-4.54			 	L			<u> </u>	100	97
ļ	D-5	20.2-20.9	6.16-6.37	ļ					L		 	
	D-6	30.0-30.4	9.14-9.27			L					1	
}	D-7 D-8	40.1-40.8 50.2-50.9	12.22-12.44	}			ļ	ļ			100	95
<u> </u>	D-8	30.2-30.9	13.30-13.31			 -	├		├			
WR-T-1	B-1	0.1-2.0	0.03-0.61					100	-			53
 "\		0.1-2.0	0.03-0.61		<u> </u>	 		100	90	81	66	33
WR-T-2	B-1	0.25-1.5	0 (8-0 46	ł		 	100		07	102	86	70
HK-1-2	b-2		0.(B-0.46			 	100	99	97	92		79
 	5-2	6.0-6.5	1.83-1.98	 	ļ	 -	100	79	52	28	16	10
WR-T-3	B-1	0.1-1.5	0.03-0.46	}		 			 	100		93
- "K-1-3	b-3	9.0-9.5		 						1.00	99	
}	1 2-3	7.0-7.3	2.74-2.90	ļ		} -	_	<u> </u>		 	 	}
WR-T-4	B-1	0.25-2.0	0.08-0.61	}		 		100	99	96	92	90
_ "K 1 3	⊢∸ ∸−	0.23-2.0	0.00-0.81	 		 	 	100	1 33	1 70	 36 -	1 34
				<u> </u>		<u> </u>						

NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System

SS — Standard split spoon

P - Pitcher

D - Fugro Orive

(d) * Indicates that test has been performed and results are included in this report

B, b - Bulk

(b) NP - Not Plastic

87 W					BART.	AT P	47	TERBE	DC				N-SITU				OMPACTE		I
U S	STAN	DARD S	IEVE N	0.	PART	(MM)				11000	DRY (JNIT	K =			MAX	I MEUM	2 5	
	SAI	(D		SIL	T OR C		L ()	1175 ((ט	USCS (c)	WEIG	THE	MOISTURE CONTENT (\$)	SATURATION (\$)	VOIO RATIO	DRY DI	MSITY	OPTIMUM MOISTURE (\$)	SPECIFIC GRAVITY OF SOLIDS
4	10	40	100	200	.005	.001	LL	PL	PI	(-)	(pcf)	(kg/m ³)	물중	SAT	8	(pcf)	(kg, m ³)	등물	2 2 2
38	27	21	18	17			·			GC	124.5	1994	11.2	86.0	0.35				
										GC	128.3	2055	10.9	93.6	0.31		1	1	1
43	35	17	11	10						GP-GC	138.3	2216	9.5		0.33				
33	22	14	11	9						GP-GM	131.5	2107	7.2	69.3	0.28		I		
										GP-GM	117.3	1879	12.5	77.5	0.44			L	
H	 }					ļ						l	 						ļ
73	62	46	35	26						SM	91.8	1471	17.9	58.1			-		
72	58	40	28	22					<u> </u>	SM	98.2	1573	7.4	28.0			L	├	
53	42	27	16	11						SM	118.0	1890	7.6	48.2		<u> </u>	-	├	ļ
 +	- [] 	37		16			} 	\vdash	 -	SM SM	115.6 115.4	1852 1849	11.6	68.6		L	 	 	
71 49	57 32	12	22	16			-	<u> </u>		GW-GM	110.7	1773	15.8	81.9			 -	 	}
├ च्य	- 32		6	5						GP-GM	121.5	1946	11.2	78.3				 	}
53	38	19	12	9						GP-GM	116.1	1860	8.9	53.6			<u> </u>		}
94	88	68	44	31						SM	105.3	1687	16.9	76.1				 -	
 	- 50	-00								SM	99.6	1596	14.0	54.6				.	├
72	59	37	22	17						SM	107.2	1717	16.8	79.4		} -	.		
 									·	SM	110.5	1770	11.6	59.6					
70	55	40	31	21						SM	107.0	1714	14.7	69.3			†	†	
					1					SM	116.8	1871	10.0	61.3				†	
										SM	115.3	1847	13.4		0.46		·	†	
1									1	SP-SM	114.9	1841	11.2		0.47		ì ·	1	t
88	81	64	32	18					<u> </u>	SM	113.0	1810	10.1		0.49			†··	†
												i — —	1				i	1	† — — — — — — — — — — — — — — — — — — —
89	78	54	34	20						SM	102.7	1645	12.1	51.2	0.64				
94	84	42	21	15						SM	103.4	1656	7.2	30.8	0.63				
96	87	54	37	28						SM	86.5	1386	14.5	41.2					
100	97	86	64	39					L	SM	90.9	1456	13.7	43.4				L	
	I]]				L	L	<u> </u>	SM	80.2	1285	17.6	43.1					
										SM	108.8	1743	18.0	88.8					
100	95	72	52	42	16	4		ــــ	<u> </u>	SM	101.3	1623	20.3	82.6				 	
-				67			42	35	7	ML	77.6	1243	37.1	85.5	1.17			 	ļ
 				-	<u>-</u>			 -	 -		<u> </u>		 	 		126 6	2010	1	ļ
66	53	29	17	13				 -	}	SM	}	 -	}	}	-	126.0	2019	9.0	ļ
 				43	 				├		}	 	 -	 	├┤	114 5	1034	14 6	
86	79	62	51	42	 	ļ		 -	├	SM	ļ ———	 -	 	ł	 	114.5	1834	14.0	-
16	10	6	4	2	 				 -	GP		 	 	ļ				 	
99		67	38	27	├ ───┤	L	 		 	SM	·	ł	 	ł				 	ļ
-22 -	93	0/	70	61	 		40	25	23	CL	 -	 	 	 	 			 	
├			 		 	ļ <u>.</u>	48	43	43			 	 	 	├ ┤		 	 	
92		84	67	55	 	<u> </u>	24	23	1	ML	 	 	 	 		122.8	1967	11.3	2.62
-24-	90	04	- ° / -	22	├─ ──┤			 "'	┝╧	PIL.		 	 	 		144.0	130/	14.3	4.04
			L			<u> </u>		<u> </u>		<u> </u>	<u> </u>	4					<u> </u>		

-	7		11	-SITU			r.	DMPACTE			=			=		
K	1				=	-				2	5			100		
5	uscs	DRY U		MOISTURE Content (\$)	SATURATION (\$)		MAXI		OPTIMUM Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED Compression	: _	CONSOLIDATION	CHEMICAL	
	(c)	MEIG	HT	MOISTURI CONTENT (\$)	TURA (\$)	YOID RATIO	DRY DE	YTERM	OPTIMUM Moistur (\$)	SPECIFI GRAVITY OF SOLI	133	5	DIRECT SHEAR	SOL	=	a .
PI	1 `	(pcf)	(kg/m ³)	9 5	SAI	22	(pc1)	(kg, m ³)	6 S	2 2 2	==	58	2 2	3	5	88 3
	GC	124.5	1994	11.2	86.0	0.35										
	GC	128.3	2055	10.9	93.6	0.31										
	GP-GC	138.3	2216	9.5	76.8							l				
	GP-GM	131.5	2107	7.2	69.3	0.28										
	GP-GM	117.3	1879	12.5	77.5	0.44				ļ		ļ				
_	1		3.453	12.0		0 04									ļ	
 	SM	91.8	1471 1573	17.9 7.4	58.1 28.0											
-	SM	98.2														
<u> </u>	SM	118.0	1890 1852	7.6 11.6		0.43					·	}				
H	SM	115.6	1849	11.7	68.6 68.6	0.40					ļ	}				
-	GW-GM	110.7	1773	15.8	81.9	0.52										} -
\vdash	GP-GM	121.5	1946	11.2	78.3	0.39									·	
┢	GP-GM	116.1	1860	8.9		0.45						ļ	<u> </u>			
┝	SM	105.3	1687	16.9		0.60										
┝	SM	99.6	1596	14.0	54.6	0.69										
\vdash	SM	107.2	1717	16.8	79.4	0.57	·									1
\vdash	SM	110.5	1770	11.6		0.53										
	SM	107.0	1714	14.7	69.3	0.57										
r	SM	116.8	1871	10.0	61.3	0.44						1				
	SM	115.3	1847	13.4		0.46										
	SP-SM	114.9	1841	11.2	65.1	0.47										
	SM	113.0	1810	10.1	55.5	0.49						I				
					I											
	SM	102.7	1645	12.1		0.64										
	SM	103.4	1656	7.2	30.8	0.63										
	SM	86.5	1386	14.5	41.2				ļ	L				ļ	ļ	
L	SM	90.9	1456	13.7		0.85								ļ		
L	SM	80.2	1285	17.6	43.1			<u> </u>	ļ	ļ	 		ļ	ļ	 	
_	SM	108.8	1743	18.0	88.8			 	ļ			ļ	 	ļ	ļ	├ ─┤
<u> </u>	SM	101.3	1623	20.3		0.66					}	 	}	}	 	
با	ML	77.6	1243	37.1	85.5	1.17		ļ					 		}	
┝		 		 	 -		126 0	2019	9.0			 		 	 	
┝	SM	}	 		}		126.0	2019	3.0	}		 -		 -	 	
┝	SM	ł	 	 	 	 	114.5	1834	14.0		}	 			 	-
-	GP	 	 	 	 	 	114.5	1034	1.3.0	}	 	 		}	 	
├-	- GF	 	 	 	 	-				 		 	 	 	 -	├──┪
 	SM	}	 	 	 	 	 			·	 	 	 	 	t	
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t÷		 	 	 	┼	 	 		t	<u> </u>		1	t		 	
1	MI	 	 	 	 	 	122.8	1967	11.3	2.62		<u> </u>	1		1	•
Ľ	1 -			1	1											

SUMMARY OF LABORATORY TEST RESULTS
VERIFICATION SITE, WHITE RIVER COP. NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAUSO

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UGRO NATIONAL INC.

									PERCE	IT FINE	R BY W	EIGHT
ACT I V I TV Number	.E ER (8)	SAMPLE 1	NTERVAL		S	ANDARO	SIEV	E OPEN	ING		U S	MATS
ACT I V I	SAMPLE			BLDRS	COBB	LES		GRA				AZ
4 2	S =	FEET	METERS	24"	12"	6"	3"	15"	3/4"	3/8"	4	10
WR-T-5	B-1	0.0-2.0	0.00-0.61	ļ					100	74	62	53
WR-T-6	B-1	0.75-2.0	0.23-0.61							100	98	96
WR-T-7	B-1	0.1-0.75	0.03-0.23	 					100	91	85	79
WR-T-8	B-1	0.5-2.0	0.15-0.61							100	99	94
WR-P-3	b-1	0.25-0.5	0.08-0.15					100	93	87	80	75
WR-P-6	b-1	0.25-2.0	0.08-0.61							100	99	96
WR-P-7	b-1	0.25-1.5	0.08-0.46	1					100	89	82	74
WR-P-8	b-1	0.25-1.0	0.08-0.30	!					100	98	96	94
WR-P-9	b-1	0.5-1.0	0.15-0.30							100	99	94
WR-P-11	B-1	1.0-2.0	0.30-0.61									100
WR-P-13	b-1	0.25-1.0	0.08-0.30						100	97	92	86
WR-P-14	b-1	0.25-1.25	0.08-0.38						100	95	93	87
WR-P-15	b-1	0.25-2.0	0.08-0.61						100	99	92	87
WR-P-16	b-1	0.25-1.0	0.08-0.30									
WR-P-17	b-1	0.25-1.0	0.08-0.30						100	92	82	76
WR-P-18	b-1	0.25-1.0	0.08-0.30									<u> </u>
WR-P-19	b-1	0.25-2.0	0.08-0.61						100	91	85	84
WR-P-20	b-1	0.25-1.5	0.08-0.46								-	-
WR-P-21	b-1	0.25-1.0	0.08-0.30					100	83	79	69	59
WR-P-22	b-1	0.25-1.0	0.08-0.30									=
WR-CS-3	b-1	0.25-1.0	0.08-0.30	†				100	84	76	70	63
WR-CS-7	b-1	0.25-1.0	0.08-0.30							100	99	94

NOTES:

(a) Sample types

- SS Standard split spoon
- P Pitcher
- D Fugro Drive
- B,b Bulk
- (b) NP Not Plastic

(c) USCS - Unified Soil Classification System

(d) * Indicates that test has been performed and results are included in this report

			·																	
FIN	R BY V					DABT	1612	AT	TERBE	ec				N-SITU				OMPACTE		
	US		DARD S	I EVE		PART SIZE	(mm)		ILKBE IITS (uscs	DRY		MOISTURE CONTENT (\$)	SATURATION (\$)		MAXI		OPTIMUM Moisture (\$)	SPECIFIC BRANTY
		AZ		100		LT OR C		<u> </u>			(c)	WEI		SES (\$)	ATURA (\$)	VOID RATIO	DRY DE		PTIM DIST	24
7.	4	10	40	100	200	.005	.001	LL	PL	P1		(pcf)	(kg/m³)	2 0	S	>~	(pcf)	(kg/m ³)	-	× 4
14	62	53	45	39	32	7	3	<u> </u>		NP	GM		 	 			 	ļ	 	
00	98	96	93	86	85	<u> </u>	<u> </u>	50	26	24	СН						110.0	1762	19.0	_
					1															
1	85	79	73	64	49	 -		}	} -	NP	SM			1		-	·	 		-
00	99	94	70	52	42			67	32	35	SC						104.7	1677	20.7	
77	80	75	68	61	E4	14	-		120				ļ	ļ		ļ		ļ	ļ	<u> </u>
<u> </u>	80	/3	- 08	01	54	14	7	27	19	8	CL		 	-		 		 -	 	
00	99	96	65	32	19						SM									
9	82	74	67	57	46	11	5	}	 -	NP	SM						-		 	
										† <u>"</u>		<u> </u>	<u> </u>	†		<u>†</u>	<u> </u>	<u> </u>	<u> </u>	
3	96	94	75	52	37	ļ			ļ		SM				ļ		I	I		
00	99	94	61	32	22	 	 -	}			SM		 			 - -		 	 	
Ë														<u> </u>	\	<u> </u>	<u> </u>			
		100	97	80	64	ļ	ļ		ļ	NP	ML	ļ ———	ļ				 	ļ	}	_
77	92	86	62	41	30	<u> </u>	} -	}	 	NP	SM	}	 			-	 	}	 	
				<u> </u>													Ī		1	
5	93	87	68	46	32	}	 -	}	 	ļ	SM	ļ		ļ				ļ		
5	92	87	80	72	59	1			 	NP	SM	 	-	 		 	 	 	 	
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2	82	76	70	65	58		 	23	21	2	ML	<u> </u>	 	† ———	 -	 		<u> </u>	<u> </u>	
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				<u> </u>	 	 	 	 -	 	\vdash	SM	}	 			 	}	 -	 -	
1	85	84	80	63	40						SM				<u> </u>	1				
	 						 		 							1	<u> </u>	 	 	↓ _
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5	69	59	48	42	35						SM				 			<u> </u>		
				·		ļ		1 35	22	13		ļ							ļ	1-
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	70	63	50	41	35						SM			<u> </u>	\vdash					
<u> </u>	99	94	71	16				33	25	10	SM			ļ				ļ <u> </u>		
	77	94	71	46	32	<u> </u>	L	1 23	23	10	3M	L	L	<u> </u>	<u> </u>		<u> </u>	Щ.	ــــــــــــــــــــــــــــــــــــــ	ــــــــــــــــــــــــــــــــــــــ

		1			UT 12-1			C	OMPACTE	ß		9	- E		8		
TERBE TTS		USCS (c)	DRY		MOISTURE Content (\$)	SATURATION (\$)	VOID RATIO	MAXI DRY DE		OPTIMUM Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT SWEAR	CONSOLIDATION	CHEMICAL	_
PL	PI	l	(pcf)	(kg/n^3)		SA	22	(pc1)	(kg/m ³)	8 8	9 2 2	¥.	38	2 %	50	CH	89 3
	NP	GM													-		
26	24	СН				<u> </u>		110.0	1762	19.0							•
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19	8	CL															
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2	13	CL					1		 	t	2.61	 -	†				
		SM															
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SUMMARY OF LABORATORY TEST RESULTS
VERIFICATION SITE, WHITE RIVER COP. NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE SAWSO

749LR 9-1

UGRO NATIONAL INC

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SAMPLE INTERVAL STANDARD SIEVE OPENING US STAN	f1	^			Ι					PERCEI	IT FIN	R BY V	ELGHT
WR-CS-15 b-1 0,25-1,25 0.08-0.38 100 99 95 WR-CS-23 b-1 0.25-2.0 0.08-0.61	E_	3	SAMPLE I	NTERVAL		\$	TANDARI	SIEV	E OPEN				
WR-CS-15 b-1 0,25-1,25 0.08-0.38 100 99 95 WR-CS-23 b-1 0.25-2.0 0.08-0.61	T 1 V	MPL (BLDRS	COBE	ILES		GRA	VEL			SA
WR-CS-23 b-1 0.25-2.0 0.08-0.61	A SE	NS SA	FEET	METERS	24"	12"	6"	3"	1 5 "	3/4"	3/8"	4	10
WR-CS-24 B-1 0.5-2.0 0.15-0.61 WR-CS-27 B-1 0.25-2.0 0.08-0.61 WR-CS-36 B-1 0.25-1.5 0.08-0.46 WR-CS-40 b-1 0.25-1.5 0.08-0.46 WR-CS-42 b-1 0.25-1.5 0.08-0.46 WR-CS-44 B-1 0.25-1.5 0.08-0.46	WR-CS-15	b-1	0.25-1.25	0.08-0.38							100	99	95
WR-CS-24 B-1 0.5-2.0 0.15-0.61 WR-CS-27 B-1 0.25-2.0 0.08-0.61 WR-CS-36 B-1 0.25-1.5 0.08-0.46 WR-CS-40 b-1 0.25-1.5 0.08-0.46 WR-CS-42 b-1 0.25-1.5 0.08-0.46 WR-CS-44 B-1 0.25-1.5 0.08-0.46	WR-CS-23	b-1	0.25-2.0	0.08-0.61	╁	<u> </u>							
WR-CS-27 B-1 0.25-2.0 0.08-0.61													
WR-CS-36 B-1 0.25-1.5 0.08-0.46	WR-CS-24	B-1	0.5-2.0	0.15-0.61	ļ		 -			}i			
WR-CS-40 b-1 0.25-1.5 0.08-0.46 100 95 93 91 WR-CS-42 b-1 0.25-1.5 0.08-0.46 100 WR-CS-44 B-1 0.25-1.5 0.08-0.46	WR-CS-27	B-1	0.25-2.0	0.08-0.61									
WR-CS-40 b-1 0.25-1.5 0.08-0.46 100 95 93 91 WR-CS-42 b-1 0.25-1.5 0.08-0.46 100 WR-CS-44 B-1 0.25-1.5 0.08-0.46	WR-CS-36	B-1	0 25-1 5	0.08=0.46			<u> </u>						
WR-CS-42 b-1 0.25-1.5 0.08-0.46 100 WR-CS-44 B-1 0.25-1.5 0.08-0.46				0.08-0.40									
WR-CS-44 B-1 0.25-1.5 0.08-0.46	WR-CS-40	b-1	0.25-1.5	0.08-0.46						100	95	93	91
WR-CS-44 B-1 0.25-1.5 0.08-0.46	WR-CS-42	b-1	0.25-1.5	0.08-0.46									100
	UD CC AA	5.1	0.05.3.5	2 22 2 46									
WR-CS-49 b-1 0.25-1.0 0.08-0.30 100	WK-CS-44	R-1	0.25-1.5	0.08-0.46						\vdash			
	WR-CS-49	b-1	0.25-1.0	0.08-0.30									100
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NOTES:

- (a) Sample types
 - SS Standard split spoon

 - P Pitcher
 - 0 Fugro Orivo
 - B, b Bulk
- (b) MP Not Plastic

- (c) USCS Unified Sail Classification System
- (d) * Indicates that test has been performed and results are included in this report

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		U S			SIEVE I		PART	(開門)		TERBE HITS (nzcz	ORY	UNIT	MOISTURE CONTENT (\$)	SATURATION (\$)	0	MAXI ORY DE	MUM	DPT HINE BOISTURE
=1			SA		T		LT OR C					(c)	WEI	in i	S = 3	2	YOID RATIO		M2111	14 S
_	3/8"	4	10	40	100	200	. 005	.001	LL	PL	PI		(pc1)	(kg/m^3)	= 3	S	25	(pcf)	(kg-m ³)	0 =
4	100	99	95	90	83	75	ļ	 		<u> </u>	NP	ML								
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		-	100	99	93	81	26	12	31	24	7	ML							†	
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TERBE BITS (RG b)	USCS (c)	DRY (HT	MOISTURE Content (\$)	SATURATION (\$)	YOID Ratio	MAXI DRY DE		OPTIMUM Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT SHEAR	CONSOLIDATION	CHEBICAL	_
PL	PI		(pcf)	(kg/n ³)	03 08	SAI	20	(pcf)	(kg: m ³)	5 2	222	=	58	三芸	83	E	8 5
	NP	ML															
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SUMMARY OF LABORATORY TEST RESULTS
VERIFICATION SITE, WHITE RIVER COP, MEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

740LE 9-1 1-07-5

JORO NATIONAL INC

SYMBOL	BORING NO.		SAMPLE I	NTERVAL	SOIL		FIAL ENSITY	INITIAL MOISTURE CONTENT	INITIAL VOIO RATIO	INITIAL DEGREE OF SATURATION
		I SOUL DRY DENSITY	T 4~> 1	KAIIU	(\$)					
0	WR-8-1	P-6	20.0-20.8	6.10-6.34	MH	77.4	1240	33.6	1.18	77.2
Δ	WR-8-3	P-7	25.4-28.2	7.74-7.99	CH	68.2	1093	45.1	1.47	82.8

AT FIELD MOISTURE

AFTER ADDITION OF WATER

COMPRESSION

- - REBOUNG

CONSOLIDATION TEST RESULTS VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION

FIGURE

DEPARTMENT OF THE AIR FORCE - SAMSO

2 JUL 79

AFY-02

SUMMARY OF TRIAXIAL COMPRESSION TEST RESULTS VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-2

UGRO NATIONAL

AFV-10

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HE I GHT /		2.4	2.4	2.4																						
DEGREE OF SATURATION	(\$)	68.8	88.8	93.7																						
MOISTURE	(\$)	21.0	27.8	33.6																						
1 1		1411	1461	1371															į							
DRY DENSITY	pct	92.2	91.2	85.6																						
IF I NED TRENGTH	kN/m2	445	239	129																						
UNCONFINED COMP. STRENGTH	181	8.3	5.0	1.1																						
7108	TYPE	13	13	H																						
NTERVAL	METERS	3.05-3.32	4.57-4.85	2.41-2.62							; ;															
SAMPLE INTERVAL	FEET	10.0-10.8	15.0-15.9	7.9-8.6																						
12		1-d	P-5	p-3																						
•	MO.	WR-B-1	WR-B-3	WR-8-4																						

SUMMARY OF UNCONFINED COMPRESSION
TEST RESULTS
VERIFICATION SITE, WHITE RIVER COP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE

MERO NATIONAL INC

AFV-09

BORING	SAMPLE	SAMPLE I	NTERVAL	SOIL	NORMAL	STRESS	MAXI SHEAR S	MUM Trength
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m²	ksf	kN/m ²
WR-8-2	0-9	30.0-30.6	9.14-9.33	GM	3.0	144	3.7	177
WR-8-4	P-5	15.0-15.6	4.57-4.75	SP-SM	1.5	72	1.2	57
	P-5	15.0-15.6	4.57-4.75	SP-SM	3.0	144	2.3	110
	P-5	15.0-15.6	4.57-4.75	SP-SM	4.5	215	3.2	153
WR-8-6	0-11	60.2-60.7	18.35-18.50	SM	6.0	288	7.8	373
	0-11	60.2-60.7	18.35-18.50	SM	9.0	431	10.9	522
	0-11	60.2-60.7	18.35-18.50	SM	12.0	575	11.1	531
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SUMMARY OF DIRECT SHEAR TEST RESULTS
VERIFICATION SITE, WHITE RIVER CDP. NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-4

UGRO NATIONAL INC

SAMPLE S				1700				Ä	WATER SOLUBLE	E L	CALCIUM
P-15 25.0-25.9 2.6-8.2 2.29-2.50 SM 6.8 314 422 104 103 P-7 25.0-25.9 7.62-7.89 MH 6.9 89 19 -14 88 P-11 60.9-61.9 1.6.56-18.07 MH 7.0 50 11 -13 63 P-15 120.7-121.4 36.79-37.00 ML 7.0 50 11 -13 63 P-15 120.7-121.4 36.79-37.00 ML 7.0 55 15 -14 110 P-15 160.0-161.6 48.01-49.26 ML 7.0 65 18 32 58 b-1 0.25-1.0 0.08-0.30 SM 7.2 81 22 452 120 b-1 0.25-1.5 0.08-0.46 CL 7.0 78 29 21 194 112 B-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 B-1	<u>-</u>	<u> </u>		MICHAL	SOIL TYPE	푎	S0010M		SULPHATE	CALCIUM	CARBONA TE
D-3 7.5-8.2 2.29.2.50 SM 6.8 314 422 104 103 P-7 25.0-25.9 7.62-7.89 MH 6.9 69 19 -14 103 P-15 160.9-61.9 16.50-18.07 ML 7.0 50 11 -13 68 P-15 120.7-121.4 36.79-37.00 ML 7.0 55 15 -14 110 P-17 160.6-161.6 49.01-48.26 ML 7.0 55 15 -14 110 P-1 160.6-161.6 49.01-48.28 ML 7.0 55 16 22 58 b-1 0.25-1.5 0.08-0.30 SM 7.2 81 22 4552 120 b-1 0.25-1.5 0.08-0.46 CL 7.0 28 21 194 112 B-1 0.25-1.5 0.08-0.46 CL 7.0 28 21 194 112 B-1 0.25-1.5 0.08-0.46<			FEET	METERS			mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
P-7 25.0-25.9 7.62-7.89 MH 6.8 89 18 414 68 P-11 60.9-61.9 18.66-18.67 MH 7.0 50 11 413 63 P-15 120.7-121.4 38.79-37.00 ML 7.0 55 15 414 110 P-17 160.8-161.6 49.01-49.26 ML 7.0 65 18 32 56 D-1 0.25-1.0 0.08-0.30 CH 7.3 161 21 3438 122 D-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 4552 120 D-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112	WR-B-1	0-3	7.5-8.2	2.28-2.50	¥S	8.8	314	422	104	103	553
P-11 60.9-61.9 18.56-18.87 MH 7.0 50 111 -13 63 P-15 120.7-121.4 36.79-37.00 ML 7.0 55 15 14 110 P-17 160.8-161.6 49.01-49.26 ML 7.0 65 18 32 56 D-1 0.25-1.0 0.08-0.30 CH 7.3 161 21 3438 122 D-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 4552 120 D-1 0.25-2.0 0.08-0.46 CH 7.1 442 22 4552 120 D-1 0.25-1.5 0.08-0.46 CL 7.0 755 601 646 219 B-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112		P-7	25.0-25.9	7.62-7.89	=	6.9	68	61	¥ v	88	219
P-15 120.7-121.4 38.79-37.00 ML 7.0 55 15 -14 110 P-17 160.6-161.6 48.01-48.26 ML 7.0 65 18 32 58 b-1 0.25-1.0 0.08-0.30 CM 7.3 161 21 3438 122 b-1 0.25-1.0 0.08-0.30 CM 7.3 161 22 380 162 b-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 4552 120 b-1 0.25-2.0 0.08-0.46 CH 7.1 442 22 4552 120 B-1 0.25-1.5 0.08-0.46 CL 7.0 28 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.		11-d	6.19-6.09	18.56-18.87	¥	7.0	50	=	~13	63	263
P-17 160.6-161.6 48.01-49.26 ML 7.0 65 18 32 58 b-1 0.25-1.0 0.08-0.30 CH 7.3 161 21 3438 122 b-1 0.25-1.0 0.08-0.30 SM 7.2 81 22 380 162 b-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 452 120 b-1 0.25-2.0 0.08-0.46 CL 7.0 28 21 184 112 B-1 0.25-1.5 0.08-0.46 CL 7.0 28 21 184 112 C 0.08-0.46 CL 7.0 28 21 184 112 C 0.25-1.5 0.08-0.46 CL 7.0 28 21 184 112 C 0.25-1.5 0.08-0.46 CL 7.0 28 21 184 112		P-15	120.7-121.4	36.79-37.00	¥	7.0	55	15	4	110	442
b-1 0.25-1.0 0.08-0.30 CH 7.3 16i 21 3438 122 b-1 0.25-1.6 0.08-0.30 SM 7.2 81 22 380 162 b-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 4552 120 b-1 0.25-2.0 0.08-0.46 CH 7.0 755 601 846 219 B-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 0.25-1.5 0.08-0.46 CL		P-17	160.6-161.6	49.01-49.26	=	7.0	65	18	32	58	568
h-1 0.25-1.0 0.08-0.30 SM 7.2 81 22 380 162 b-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 4552 120 b-1 0.25-2.0 0.08-0.46 CH 7.0 765 601 846 219 B-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 C 1.0 29 21 194 112 112 112 C 1.0 2.0	WR-P-16	1-q	0.25-1.0	0.08-0.30	3	7.3	191	21	3438	122	643
b-1 0.25-1.5 0.08-0.46 CH 7.1 442 22 4552 120 b-1 0.25-2.0 0.08-0.61 SM 7.0 765 601 846 218 8-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1<	WR-P-18	1-q	0.25-1.0	0.08-0.30	3 5	7.2	20	22	380	162	468
b-1 0.25-2.0 0.08-0.61 SM 7.0 765 601 846 218 8-1 0.25-1.5 0.08-0.46 CL 7.0 29 21 194 112 1 1 1 1 1 1 1 1 1 1 1	WR-P-20	D-1	0.25-1.5	0.08-0.46	*5	7.1	442	22	4552	120	909
8-1 0.25-1.5 0.08-0.46 CL 7.6 29 21 194 112 112 112 112 112 112 113 113 113 114 115	WR-CS-23	1-q	0.25-2.0	0.08-0.61	NS.	7.0	765	109	848	219	612
	WR-CS-44	8-1	0.25-1.5	0.08-0.46	73	7.0	29	21	194	112	412
	_										

SUMMARY OF CHEMICAL TEST RESULTS
VERIFICATION SITE, WHITE RIVER COP, NEVADA

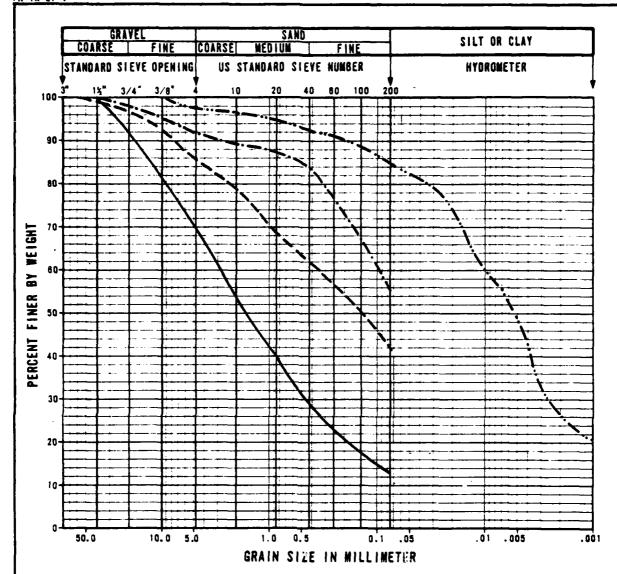
MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-5

UGRO NATIONAL IN

AFY-07

CHECKED BY



SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
3 I MDUL	NUMBER	NUMBER	FEET	METERS	TYPE
	A	WR-T-1	0.1-2.0	0.03-0.61	SM
	В	WR-T-2	0.25-1.5	0.07-0.46	SM
	С	WR-T-4	0.25-2.0	0.07-0.61	ML
	0	WR-T-6	0.75-2.0	0.23-0.61	СН

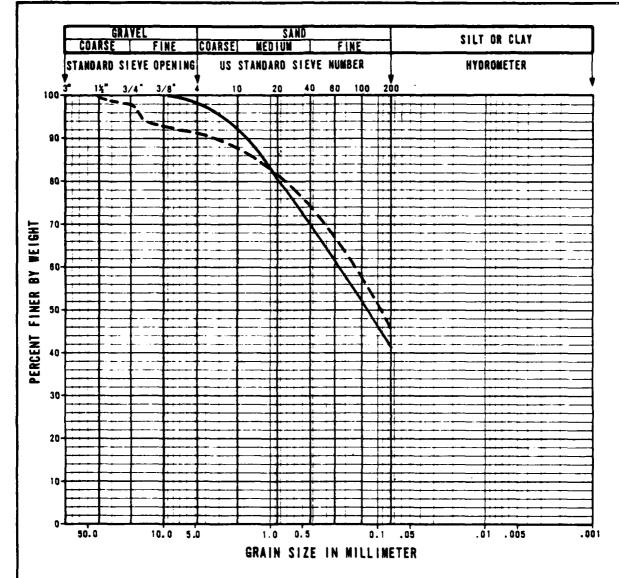
GRAIN SIZE CURVES, CBR TESTS VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-2

UGRO NATIONAL INC

AFV-12



SYMBOL	COMPOSITE SAMPLE	ACTIVITY	SAMPLE	INTERVAL	SOIL
31800	NUMBER	NUMBER	FEET	METERS	TYPE
	E	WR-T-8	0.5-2.0	0.15-0.61	SC
	F	WR-CS-36 WR-CS-44	0.25-1.50 0.25-1.50	0.08-0.46 0.08-0.46	M2
		-			1

GRAIN SIZE CURVES, CBR TESTS
VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SAMSO

9-2

UGRO MATIONAL INC

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-6

UBRO NATIONAL INC.

SC 42 67 35 104.7 1677 20.7 85.3 156. 20.8 89.3 SL 42 67 35 104.7 1677 20.7 85.3 1367 20.4 81.5 SM 46 NP 120.0 1922 13.3 102.5 1642 12.7 88.9 120.0 1922 13.3 102.5 1642 12.7 88.9	COMPOSITE Sample	SOIL	PERCENT PASS ING	ATTER	ATTERBERG LIMITS	SPECIFIC		MAXIMUM DRY DENSITY	OPT IMUM MOISTURE	COMPJ DRY DE	COMPACTED DRY DENSITY	COMPACTED	PERCENT OF MAXIMUM	CBR
SC 42 67 35 104.7 1677 20.7 85.3 1367 20.8 98.3 NP 120.0 1822 13.3 102.5 1642 12.4 65.4 SM 48 120.0 1822 13.3 102.5 1642 12.4 65.4	NUMBER	ITE	#200	11	PI	BKAVII		kg/m3	(%)		kg/m3	(%)	ORY DENSITY	(\$)
SG 42 67 35 104.7 1677 20.7 65.3 1367 20.8 90.4 SM 46 MP 120.0 1922 13.3 102.5 1642 12.4 65.4 100.0 1922 13.3 102.5 1642 12.4 65.4										102.9	1648	8.02	98.3	30
SG 42 67 35 104.7 1677 20.7 85.3 1367 20.4 81.5 SM 48										94.7	1517	20.8	90.4	l
SM 48 MP : 120.0 1922 13.3 102.5 1642 12.4 98.9	w	SC	42	67	35		104.7	1677	20.7	85.3	1367	20.4	81.5	2
SM 46 MP : 120.0 1922 13.3 102.5 1642 12.4 65.4														
SW 46 MP : 120.0 1922 13.3 102.5 1642 12.4 665.4														
SM 46 NP 120.0 1822 13.3 102.5 1642 12.4 85.4										118.7	1902	12.7	88.9	64
SM 46 MP : 120.0 1922 13.3 102.5 1642 12.4										109.3		12.3	1 . 18	01
	4	S	48		랖		120.0		13.3	102.5	1642	12.4	85.4	7

					-									

CALIFORNIA BEARING RATIO (CBR) TEST RESULTS VERIFICATION SITE, WHITE RIVER CDP. NEVADA

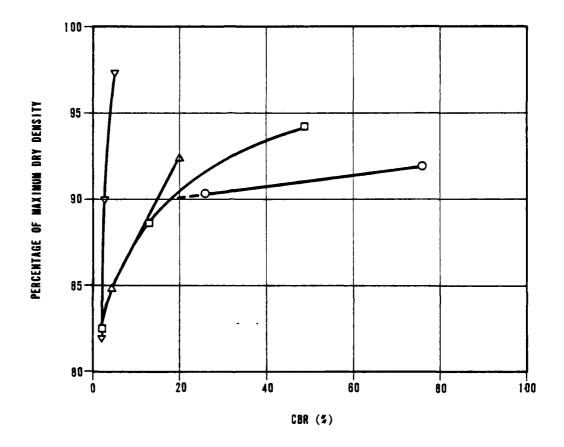
MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

TABLE 9-6 2 of 2

UBRO NATIONAL, INC

AFV-13





SYMBOL	COMPOSITE Sample Number	SOIL TYPE
0	A	SM
0	В	SM
Δ	C	ML
▽	0	CH

CALIFORNIA BEARING RATIO (CBR) CURYES VERIFICATION SITE, WHITE RIVER CDP, NEVADA

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - SAMSO

9-3

UGRO NATIONAL, INC.

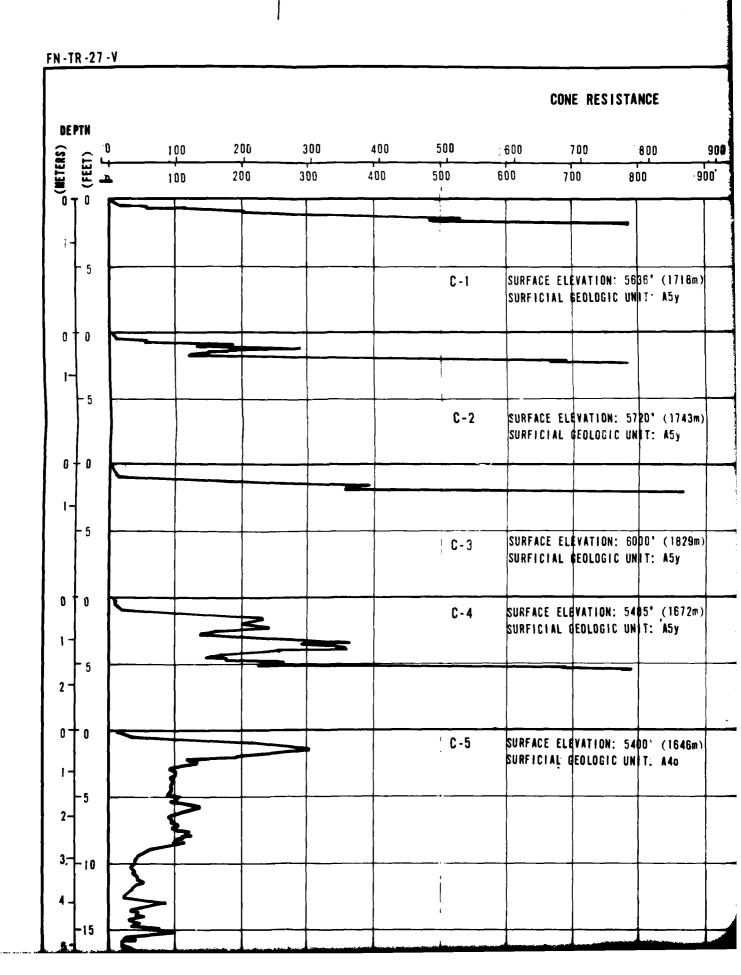
AFV-14

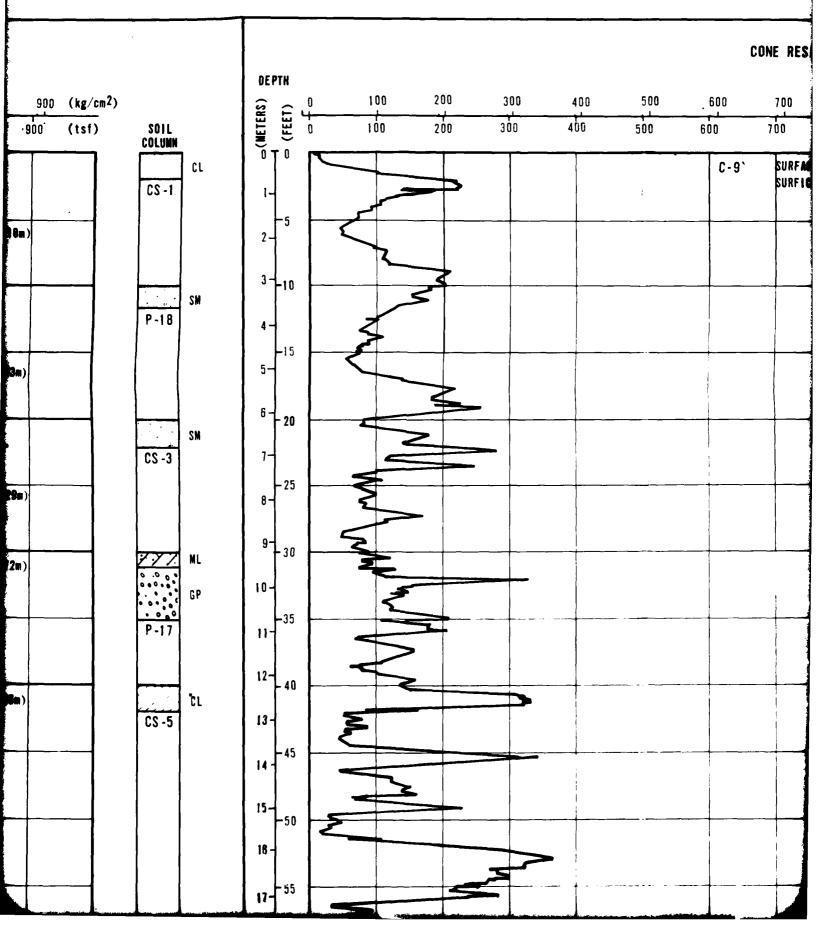
SYMBOL	COMPOSITE SAMPLE NUMBER	SOIL
0	E	SC
0	F	SM

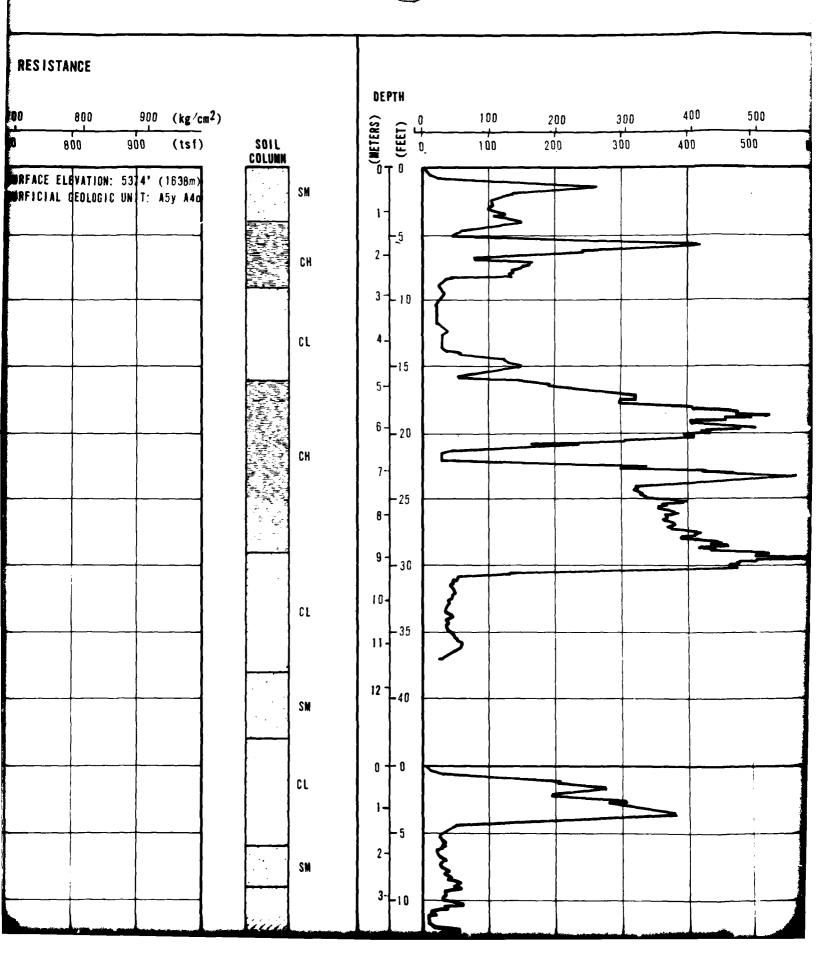
CALIFORNIA BEARING RATIO (CBR) CURVES VERIFICATION SITE, WHITE RIVER CDP, NEVADA

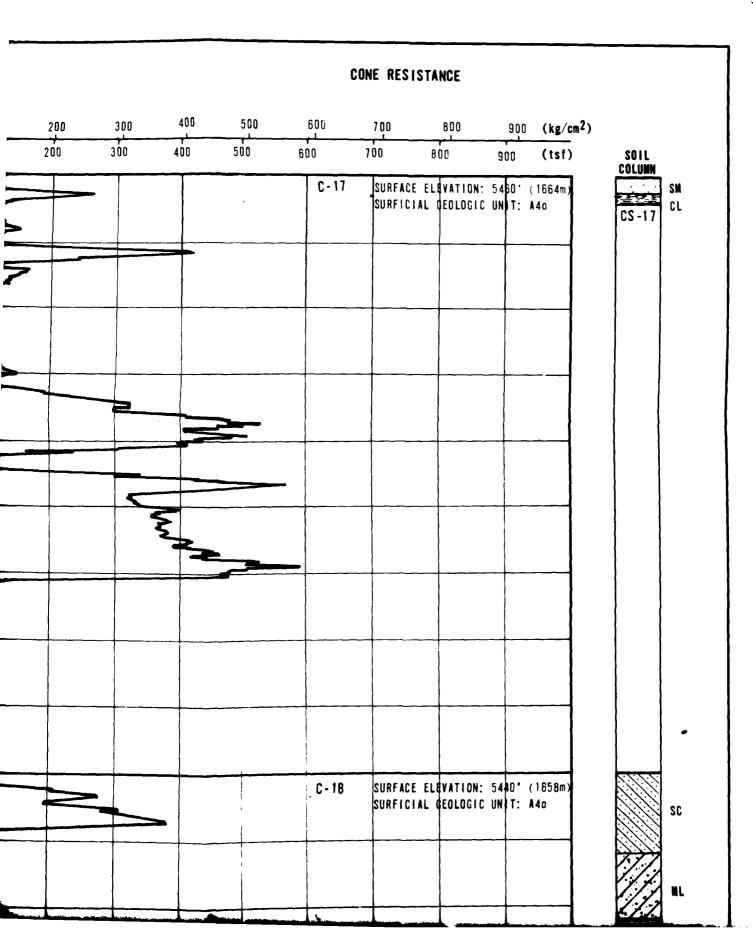
MK SITING INVESTIGATION DEPARTMENT OF THE ALR FORCE - SANSO F | GURE 9-3

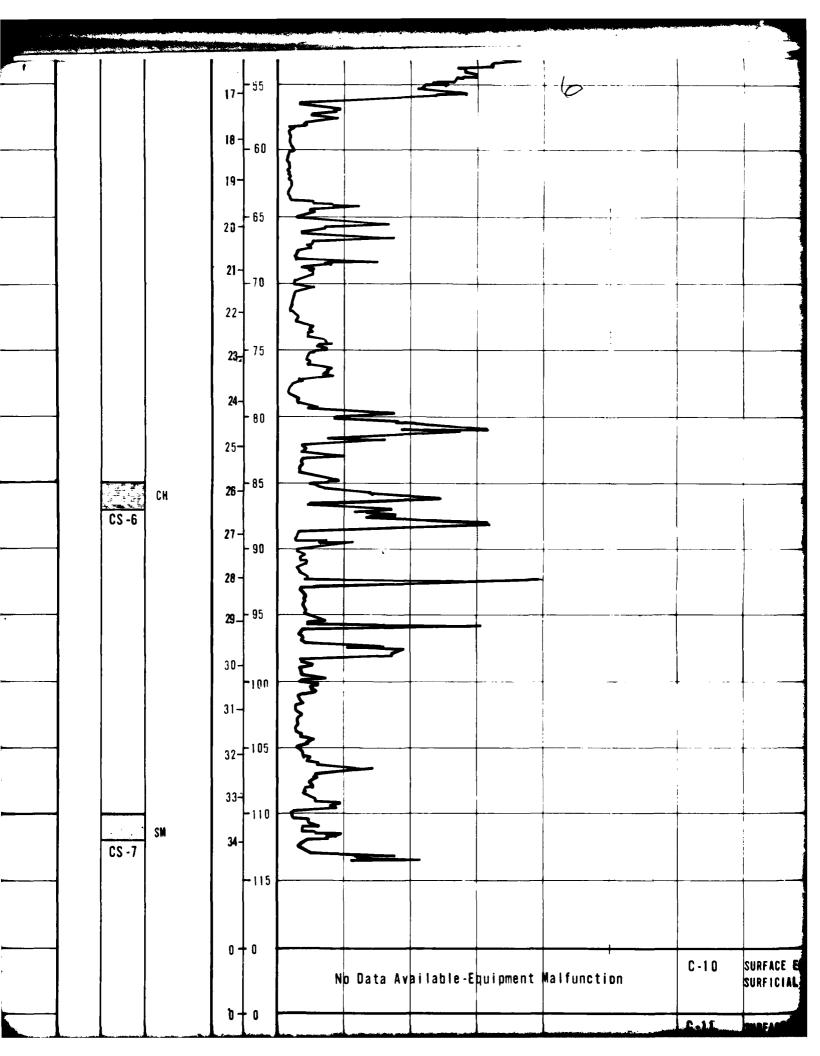
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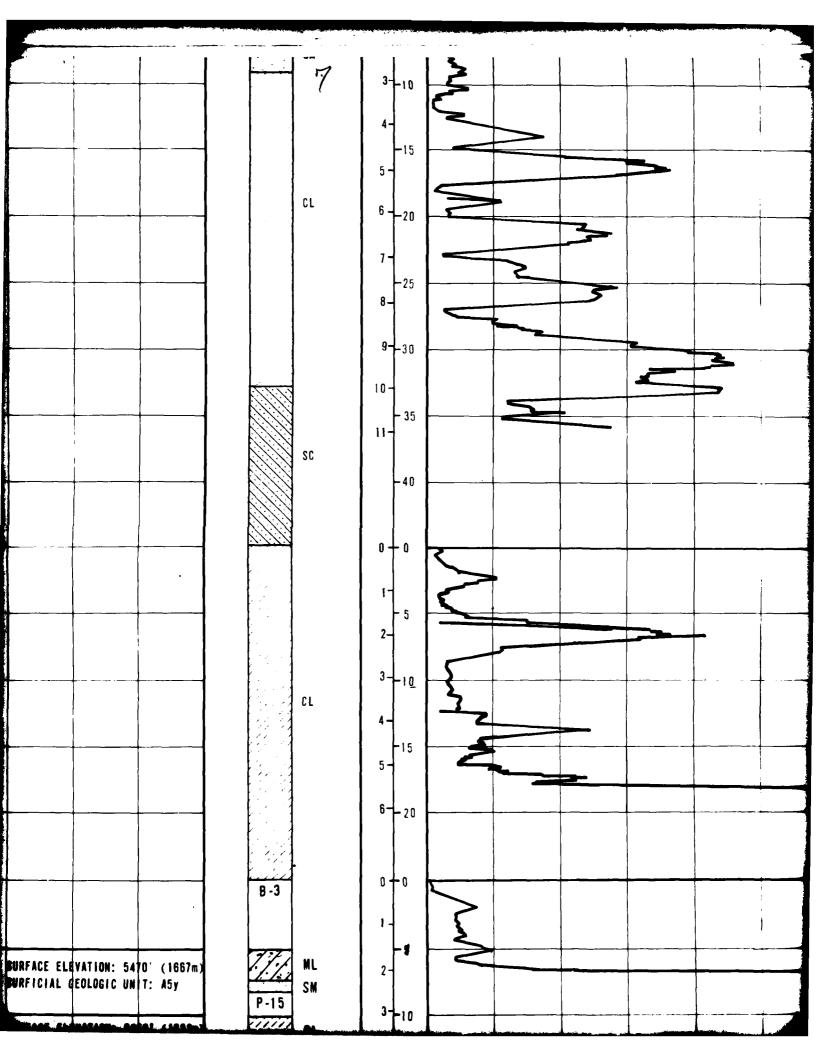




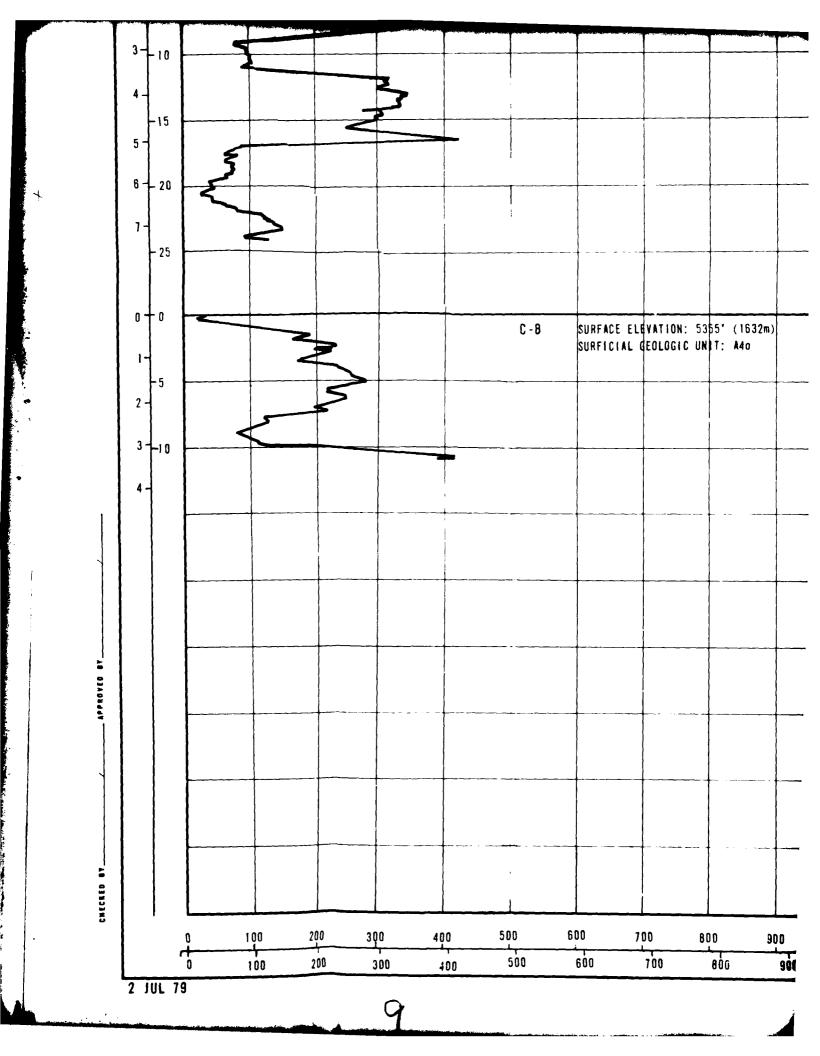


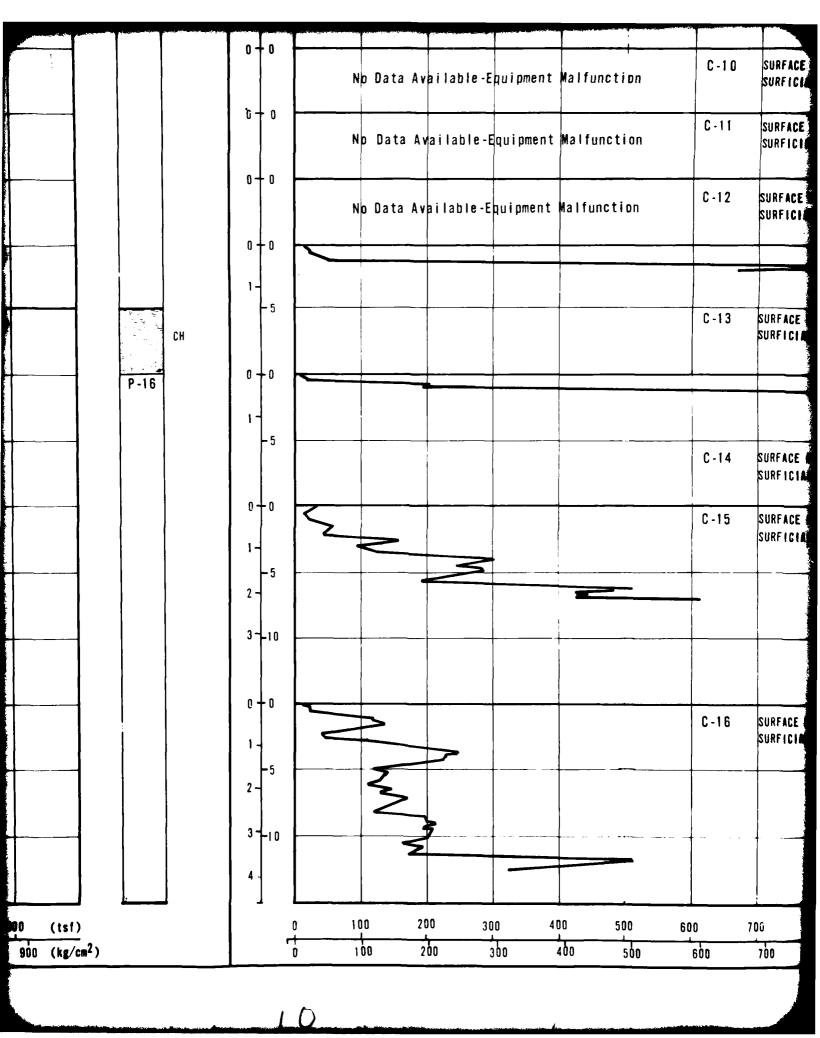


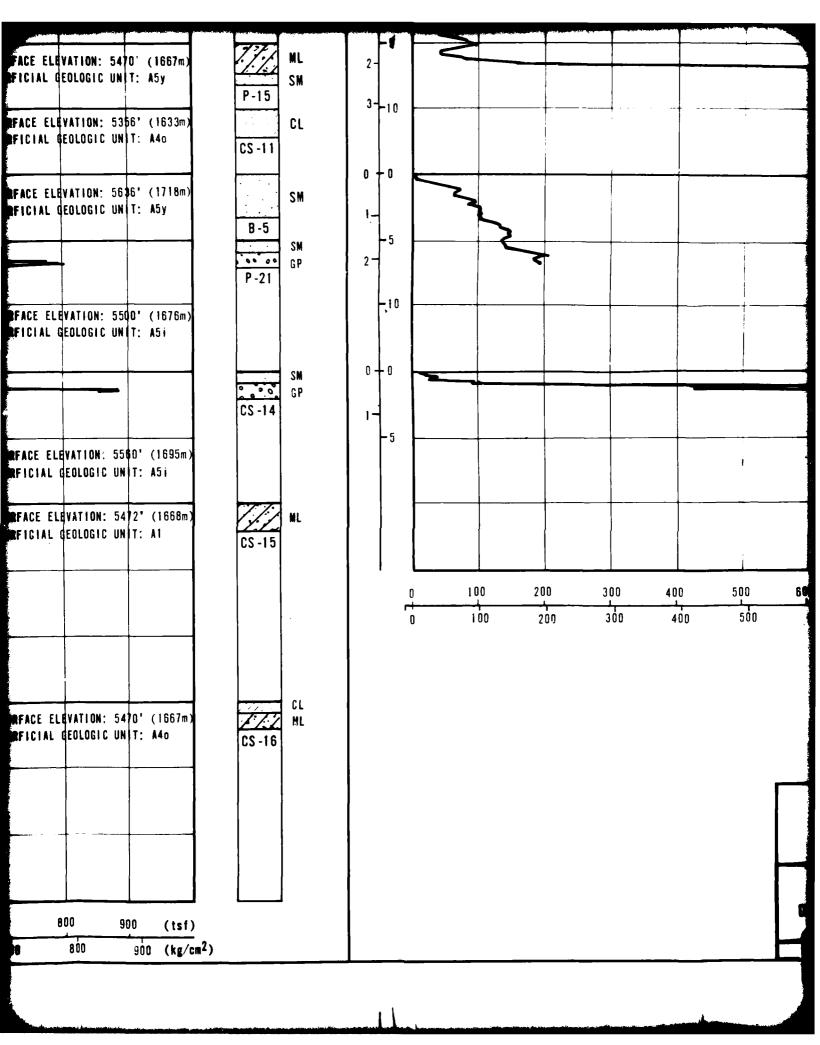


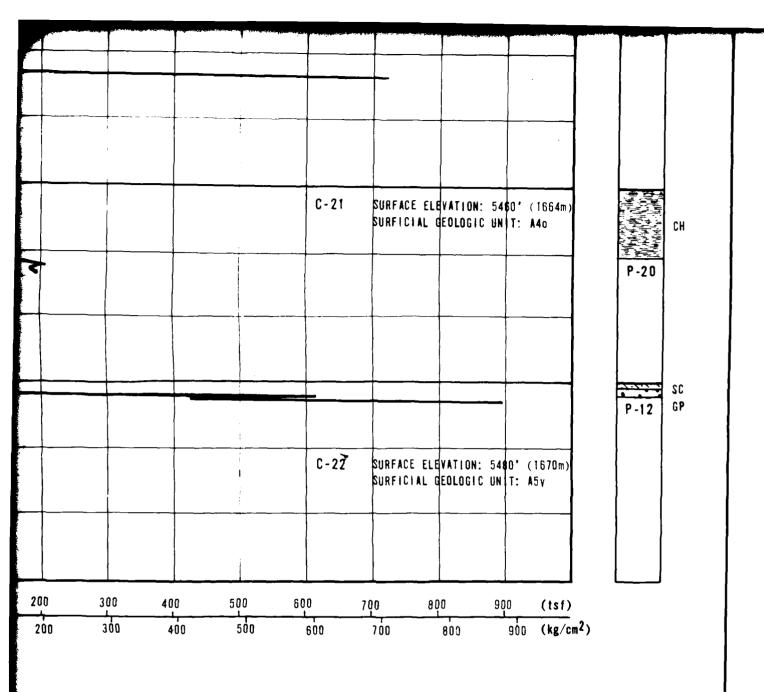


		SM	
		SP	
C-19	SURFACE ELEVATION: 5530' (1686m)	B-4	
0-15	SURFICIAL GEOLOGIC UNIT: A40		
C-20	SURFACE ELEVATION: 5400' (1670m) SURFICIAL GEOLOGIC UN T: A40	CS -20	and the second s









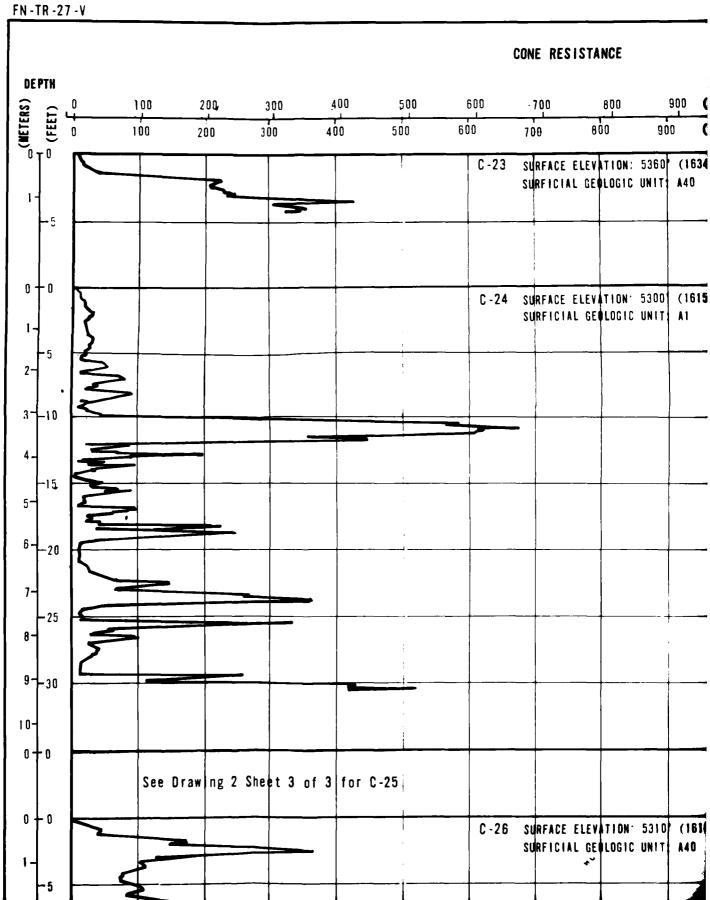
CONE PENETROMETER TEST RESULTS
VERIFICATION SITE
WHITE RIVER CDP. NEVADA

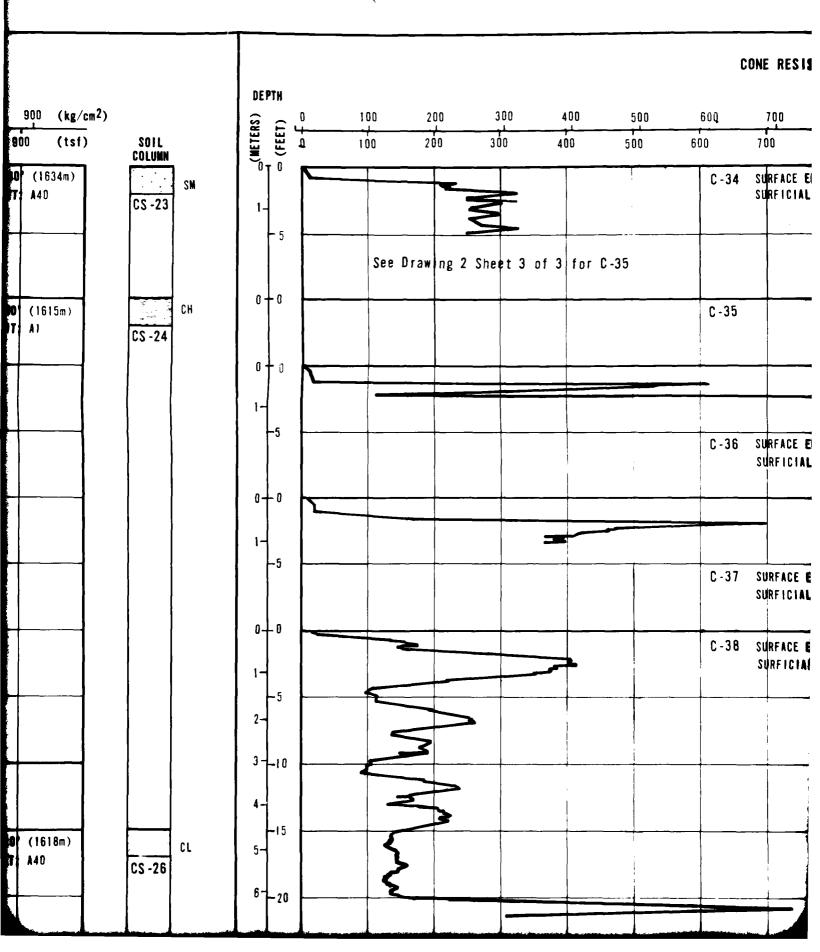
MX SITING INVESTIGATION

DEPARTMENT OF THE AIR FORCE - SAMSO

PRATING 2 1 DF 3

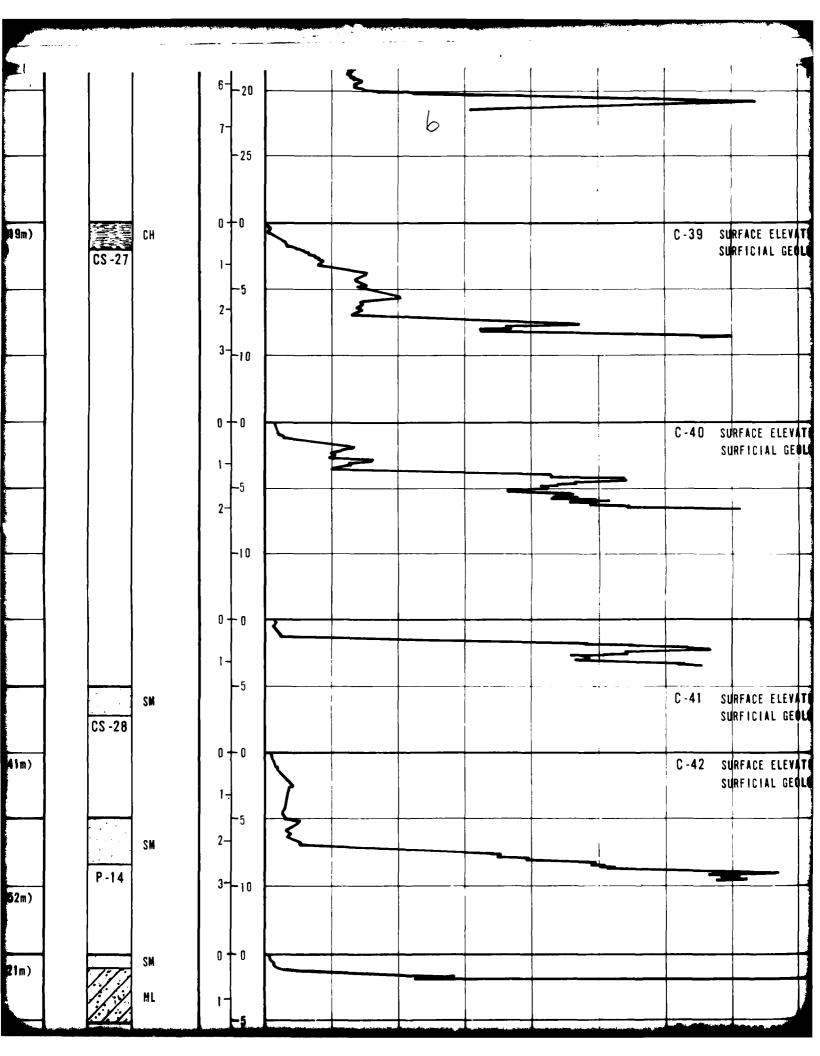
UBRO NATIONAL, INC.





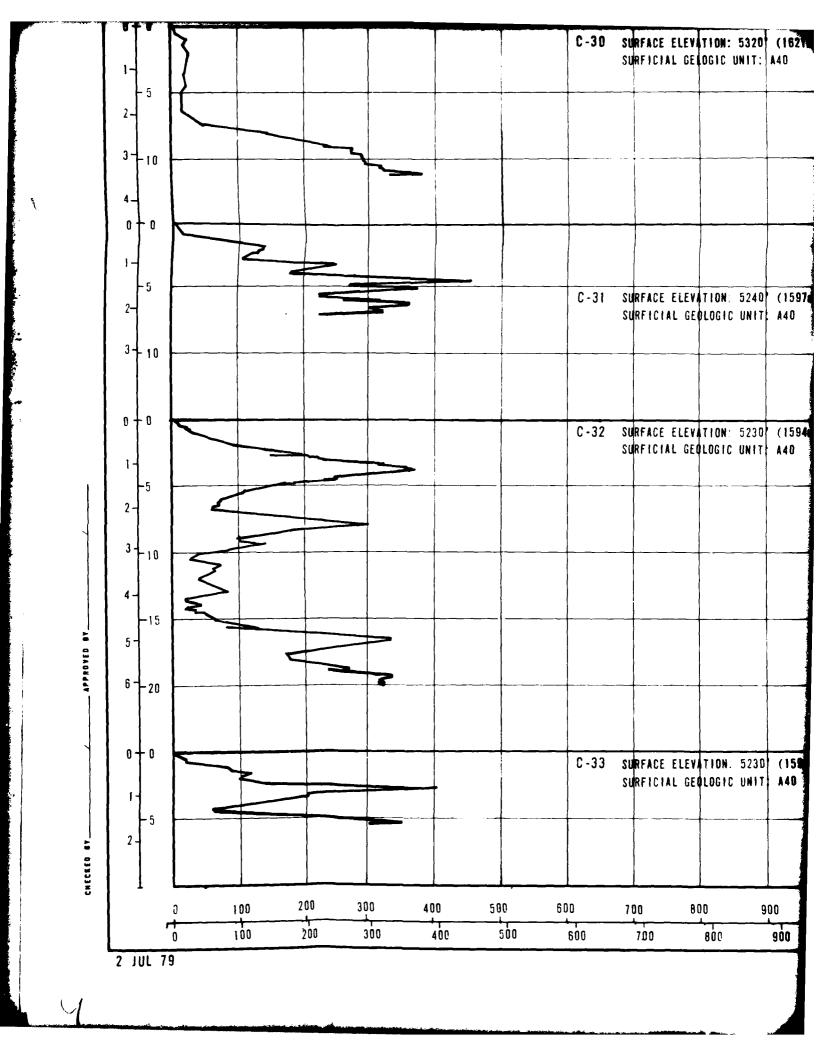
		DERTU				
800 900 (kg/cm²)		DEPTH	100	200	300	400 500
800 900 (tsf)	SOIL	O(METERS)	100			00 500
	COLUMN			200 31	00 4	
CE ELEVATIONS: 5265° (1605m) CIAL GEOLOGIC UNIT: A40	C-34 SM SP-SM		See Dra	wing 2 She	et 3 of 3	for C-49
		0+0	See Dra	ng 2 She	t 3 of 3	for C-50
		0.+0				
	CS -36	0+0				
CE SIEVATINE COLD (1500)		1-		3		
CE ELEVATIONS. 5210° (1588m) CIAL GEOLOGIC UNIT: A40		2-				
	CS 37	4-				3
CE ELEVATION: 5200° (1585m) CIAL GEOLOGIC UNIT: A40		15			5	
		6-20	\$			
CE ELEVATION: 5240 (1597m) CIAL GEOLOGIC UNIT: A5y A40	SM	7- 20 \$,	
	SP	8-25	5			
	ML	9-	2			
		30	2=			
	T-1	0+0				-
			2			
,		5		-		<u> </u>

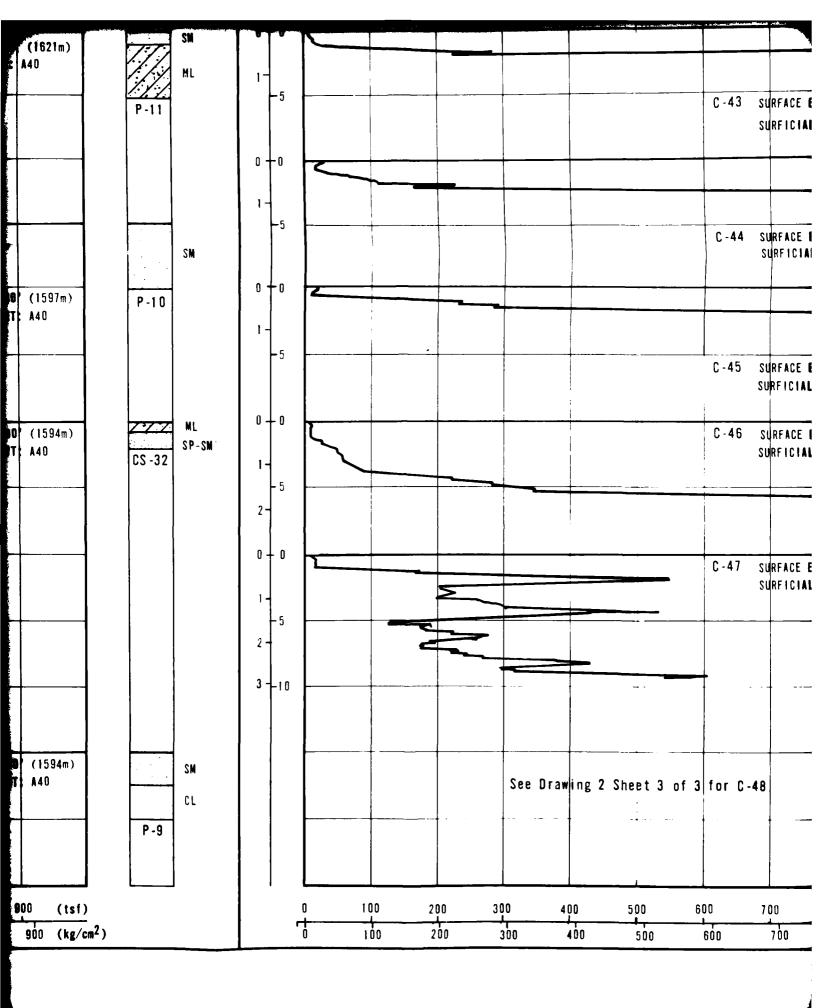
										0	ONE RES	ISTA	NCE					
2	00		300			100		500		600	700		800	9()0 (kg	g/cm²)		
21	0	;	300		41	00		500	6	00	700	8	00	900	(ts	<u>-</u> :f)	SOIL Column	
raw	ing	2 She	et :	3 of	3	for	C -4	9		C-48								
rawl	ng	2 She	et 3	of	3	for	C -5	0		C-49					· · · · · ·			
								<u> </u>		C-50								
	_ _	~						- <u>-</u>		C-51			VATION: Eglogic			m)	CS -51	CI
*	<u></u>	, Z						1										
	Z _					Ş												
-			2													1		
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				 _,														
	-									C -52	SURF AC SURF I C	E EL	EVATION: Geologic	5245 UN T	' (1599 : A4o	Jm)		SI
						-			<u></u>		-					-	B-1	



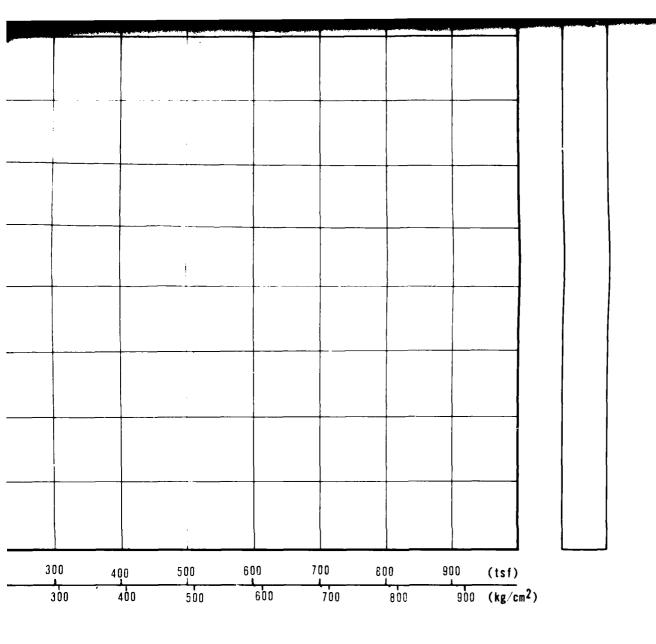
		and the second of the second o				Approximation of the second		
	1 1	-		<u>.</u>			<u> </u>	
		- 5					 	
E ELEVATION: 5270 (1606m) AL GEOLOGIC UNIT: A5y	CS -39 SC							1
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E ELEVATION: 5328 (1624m) IAL GEOLOGIC UNIT: A5y	CS-40							· · · · · · · · · · · · · · · · · · ·
							 	
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E ELEVATION 5397 (1645m)	GP P-1							
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E ELEVATION: 5440 (1658m) IAL GEOLOGIC UNIT: A5y	CS-42							
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ELEVATION: 5485 (1672m)	P-2								
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ELEVATION 5560 (1695m) L GEOLOGIC UNIT: A5:									1
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ELEVATION: 5640 (1719m) L GEOLOGÍC UNIT A5i									
ELEVATION. 5430 (1655m) L GEOLOGIC ELEVATION: A5y		SM						ļ	
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CONE PENETROMETER TEST RESULTS
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DRAWING 2

2 OF 3

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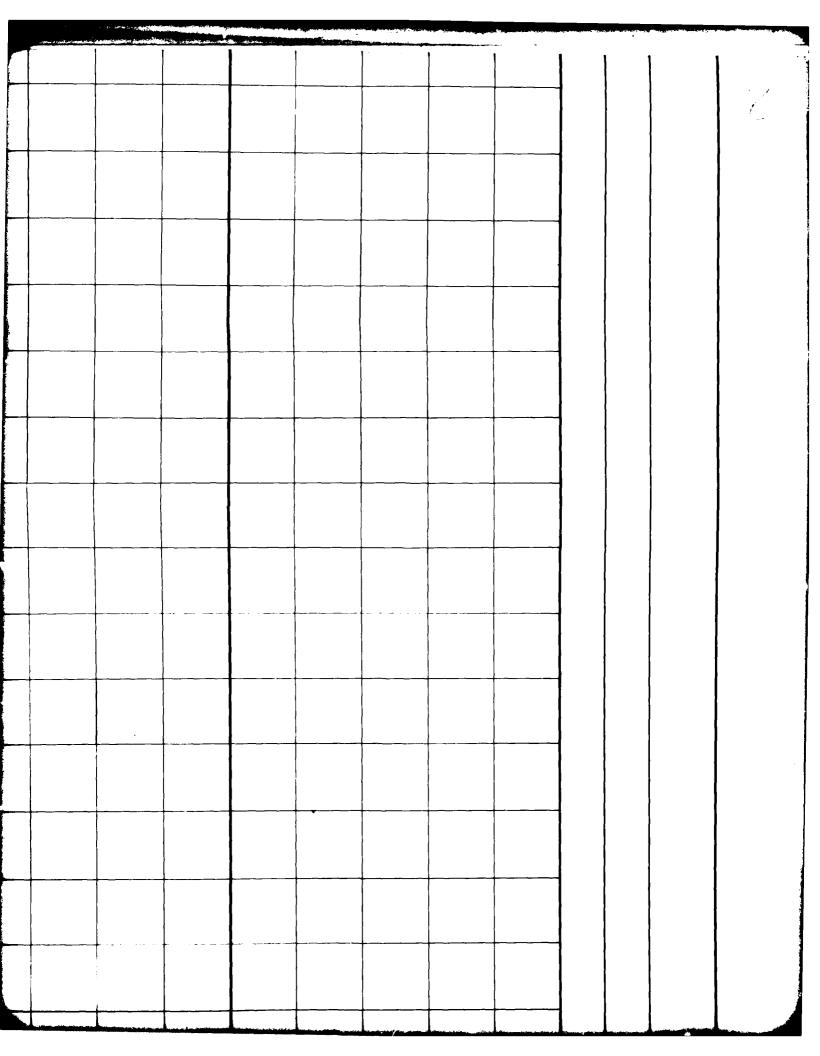
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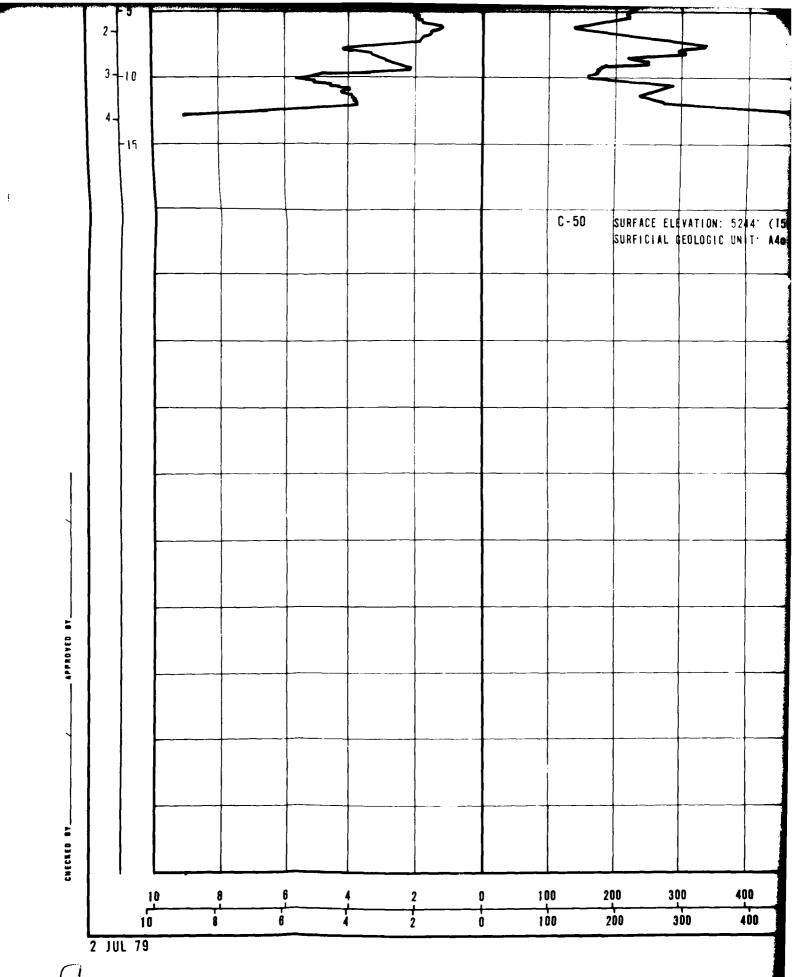
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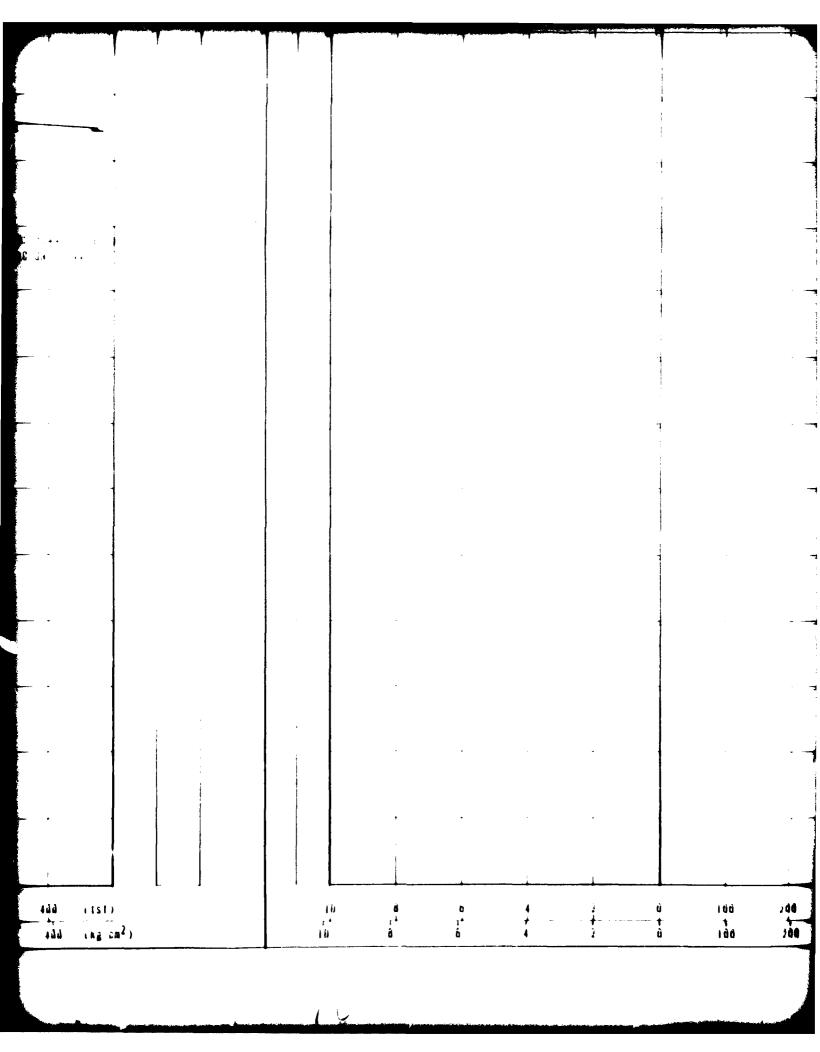
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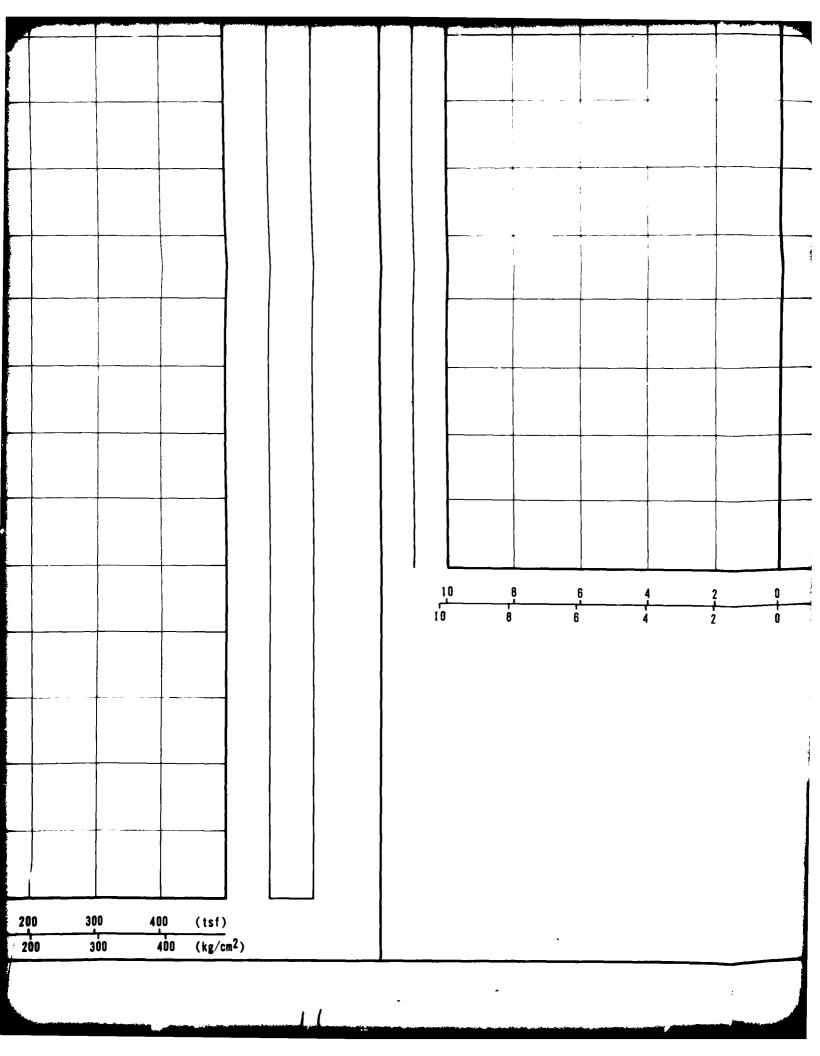
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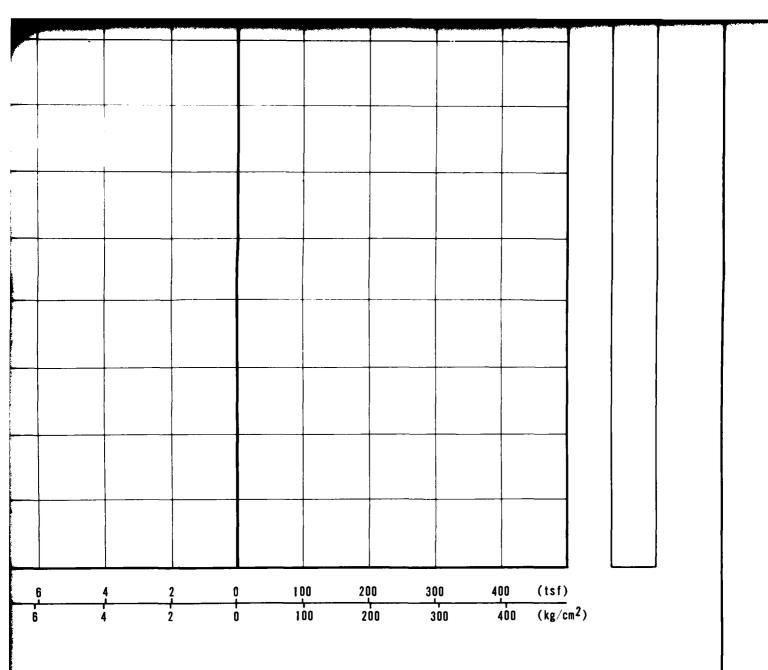




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